

The real-time protection system for MAST-U

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ABSTRACT

The Mega Amp Spherical Tokamak (MAST) is currently being extensively upgraded to provide increased coil system and power supply capability to the extent certain combinations of currents could cause catastrophic damage. To ensure operation of MAST-U within safe engineering limits, the machine protection system was also updated. The protection system is needed to protect against coil faults (such as flashovers) and monitor and calculate, in real-time, quantities such as coil currents, axial coil forces and the stored energy within the coils. The Real-Time Protection System was developed and uses Field Programmable Gate Arrays (FPGAs) which monitors up to 89 different signals collected from 7 different locations around MAST-U at a rate of 0.5MS/s. It filters and calibrates the signals and performs calculations to check if these signals correspond to valid operating ranges for currents, stored energy and coil forces. If thresholds are exceeded, then several actions can be carried out including stops to specific power supplies or a more gradual stop from the plasma control system. Initial testing of the system has shown it meets this challenging specification and the system is able to react within 200µs to breaches in thresholds as well as collecting 400MB/s of calibrated and calculated data.

1. Introduction

The Mega Amp Spherical Tokamak (MAST) (see Fig. 1) is currently being extensively upgraded to provide a system that will be able to add to the knowledge base for ITER as well as testing innovative reactor systems. MAST-U will have [1]:

- Increased toroidal field capabilities - improving confinement
- A new solenoid - increasing plasma current and pulse duration
- 19 new poloidal field coils - improving shaping
- A super-X divertor [2] - testing innovative divertor concepts and improve power handling
- Off axis NBI - modifying q and fast ion pressure profiles

To ensure operation of MAST-U within safe engineering limits, the machine protection system needs to be updated. The protection system needs to protect against coil faults and dangerous coil current combinations. To do this it monitors and calculates, in real-time, quantities such as coil currents, axial coil forces, coil heating and the stored energy within the coils. The aim is to be able to react within hundreds of microseconds if there are any inconsistencies that breach pre-defined thresholds.

The following protection criteria need to be monitored:

- Currents on toroidal, poloidal, and divertor coils are below pre-defined limits
- Coil currents measured by independent sensors (at least two sensors) are consistent within a pre-defined margin
- Toroidal Field voltage measurement across sections of the coil are self-consistent within a pre-defined margin (in order to identify any shorted-turn path fault conditions)
- Current measurements on the central solenoid are self-consistent within a pre-defined margin
- The energy stored in the coils and coil heating (I2t calculation) is kept below set pre-defined thresholds.
- The force exerted on all coils by other coils and the plasma is below pre-defined limits.
- Langmuir probes are used to ensure that plasma does not approach a set point in the divertor region (in order to protect fragile windows).

Once these protection criteria have been compared to the pre-defined thresholds then any breaches are mapped to actions. The actions that can be carried out are:

- controlled stops to the plasma control system which can bring the pulse down slowly
- stops directly to powers supplies
- shifts in the position of the plasma by using the vertical control

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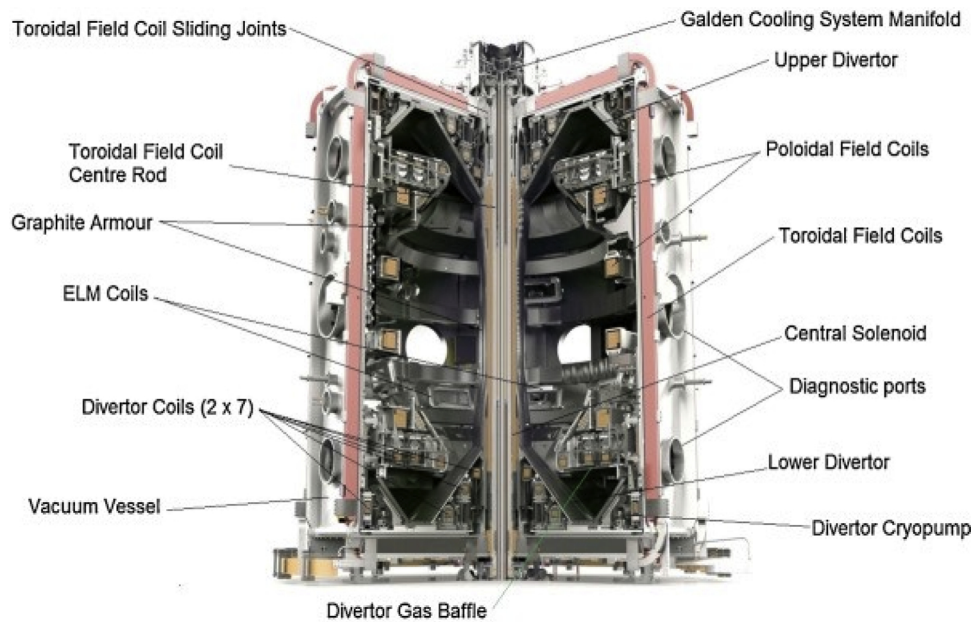


Fig. 1. Annotated cross section of the MAST-U machine [3].

system.

2. Detailed requirements

The Real Time Protection (RTP) System must be able to react to the protection criteria within 200 μ s (mainly determined by the signal filtering latency) of thresholds being exceeded. To achieve this, it needs to measure up to 89 signals from 7 different areas of plant and send this data to a central unit for real-time data analysis. The central unit will need to digitally filter the signals to allow a highly configurable filter setup. In addition, it will also need to be able to perform real-time calibrations and calculations. The system also needs to be highly configurable to allow changes to filter, calibration and calculation coefficients, fault thresholds and mappings of events to plant. Changes to the configuration should be possible on a per pulse basis.

To achieve these challenging requirements, it was decided to use a network of interconnected FPGAs, controlled with a central FPGA and ARM processor control unit. FPGAs were chosen, as determinism and low latency are inherent to this technology. CCFE has built up a significant experience and expertise in FPGA development [3]. The FPGA can handle the real-time aspects of the system while the ARM processor is able to deal with the communication with other plant systems on a slower time-scale.

The system architecture is shown in Fig. 2. The FPGA based acquisition units: ADCs, integrator and protection Langmuir probe units, located around MAST-U, collect signals and send them to a central FPGA on digital optical links using the aurora protocol [5]. This central FPGA performs the real-time processing on the data and sends requests to the plasma position controller or the FPGA based digital output modules which send optical outputs to the Plasma Control System (PCS) and to power supplies. Data is also streamed to an archive via 2 FPGA boards in a data collection PC. The ARM processor handles the communications to:

- The Machine Control System which sequences RTP states throughout a MAST-U pulse
- The parameters database which stores all the thresholds and coefficients required by RTP
- The data acquisition management system which records any actions that occur during a pulse.

Note that a hardwired system (HW) based on analogue and digital electronics also protects some critical components of MAST-U (TF coils, Solenoid). The HW protection system, provides overcurrent I2T and basic coils protections and together with RTP forms a hierarchy of protection with redundancy for MAST-U.

3. Protection design

The ADC units can each collect up to 32 channels and consist of 16-bit 0.5MS/s ADC PCBs produced by CCFE and connected via a backplane to an FPGA board: the Simple PCIe FMC Carrier (SPEC) board [4] (see Fig. 3) The SPEC board sends control signals to the ADCs, decodes the ADC data and multiplexes this data over a fiber link to the central FPGA unit using the Xilinx aurora protocol [5] through an SFP port. There are 6 of these ADC units and an ADC coupled with integrator units at the front end. The data from the ADCs and integrators is decoded in the central FPGA processing unit.

The digital input unit includes optical (ON/OFF) receivers used to trigger and synchronize the RTP system, input the Langmuir probes faults status in the RTP system, and input the status of various parts of the plants involved in MAST-U protection (hardwired protection tripped status for example).

The central processing unit hardware is the White Rabbit Switch (WRS [4]) (see Fig. 3), which consists of a Virtex-6 FPGA connected to an ARM processor. The WRS was originally designed as an ethernet switch, however in this application, the FPGA is completely re-programmed to perform the MAST-U RTP specific function. The real-time aspects of the system are streamlined on the FPGA and the updating of remotely configurable coefficients, thresholds and mappings are handled by the processor as they can occur on a much slower timescale. The filtering and calibration occur on the decoded ADC and integrator data. The output of this is streamed to the calculation modules to perform the protection criteria mentioned previously.

The actions, that can occur when the calculations breach pre-defined limits, are directed to outputs of the central FPGA. The communication to PCS and power supplies are done by connecting to digital output modules using the Xilinx aurora protocol. The digital output modules contain a SPEC board like the ADCs and integrators but are used to decode the aurora stream and send out digital outputs to on/off optical transmitters. Some of these optical transmitters connect to different power supplies and others encode different stop types to PCS. In

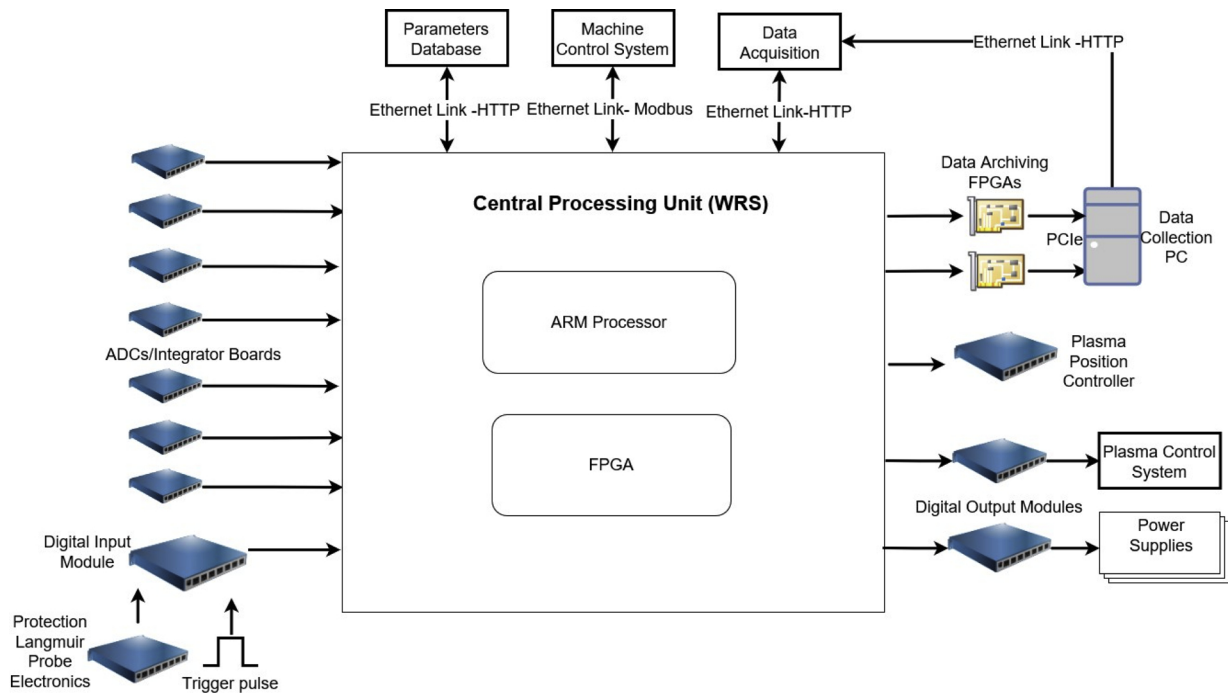


Fig. 2. The real-time protection system layout.

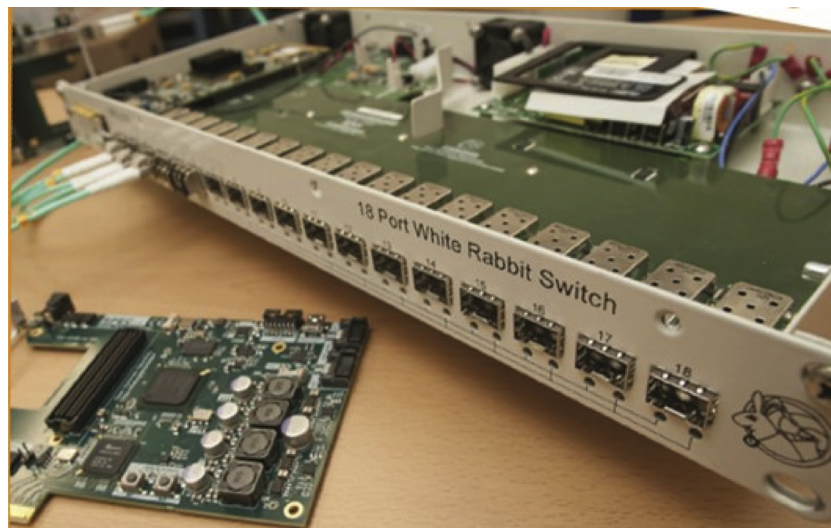


Fig. 3. SPEC board and White Rabbit Switch Hardware.

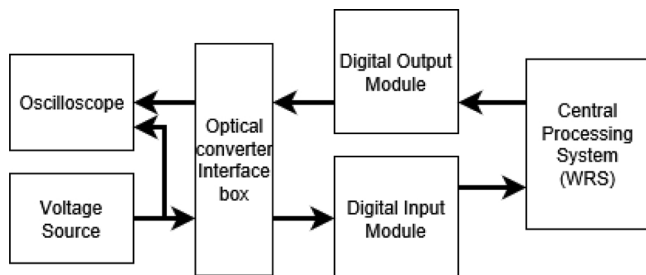


Fig. 4. Loopback experiment setup.

In addition to these actions the central FPGA can also communicate to the plasma position controller directly using the Xilinx aurora protocol and can request a plasma kick for a set period. Hardware faults can also be mapped to actions, e.g. if an aurora link goes down.

The central FPGA (the WRS hardware) embeds the real-time logic of the system, whereas the ARM processor is there to facilitate communications to the machine control system to enable the system and perform data acquisition to collect events and actions after the pulse. The FPGA also requires access to many coefficients for filters, calibration, offsets and calculations as well as thresholds and event/action mappings which are stored in a database. This is also handled by the ARM processor.

To facilitate post processing of events and actions and checking of signal integrity it is necessary to collect both the calibrated and calculated data that is acted on during the pulse. The throughput of calibrated and calculated data is 400MB/s and will need to be collected over a 7 s period. This data is not able to be stored locally as there is not enough space on the central FPGA unit, therefore this data is streamed over two optical links to two AC701 FPGAs [6] using the aurora protocol. Once the data is on the AC701 FPGAs it can be streamed over PCIe to a data collection PC using the Xillybus FPGA IP which allows

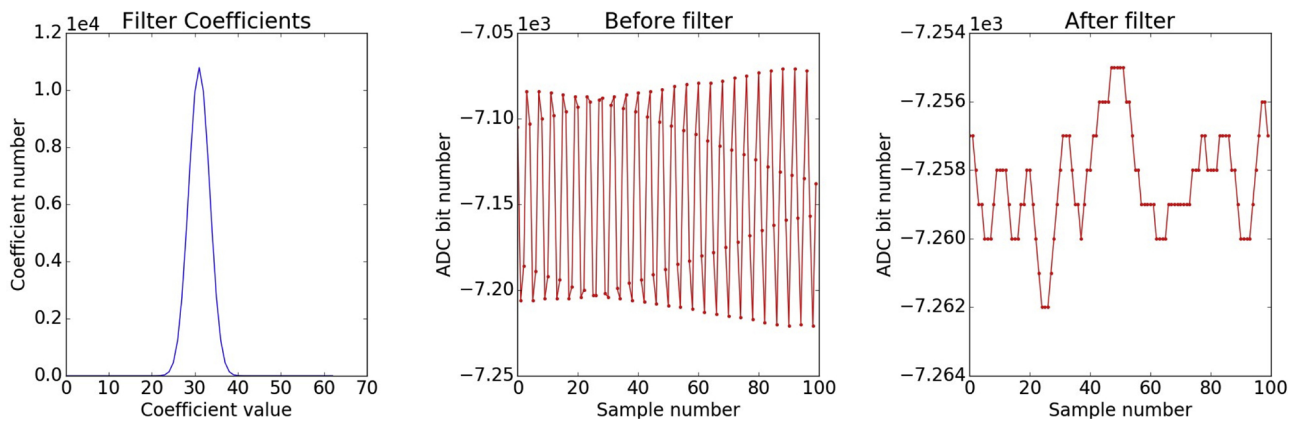


Fig. 5. The filter coefficients applied in real-time to a 125 kHz modulated signal which attenuated the signal.

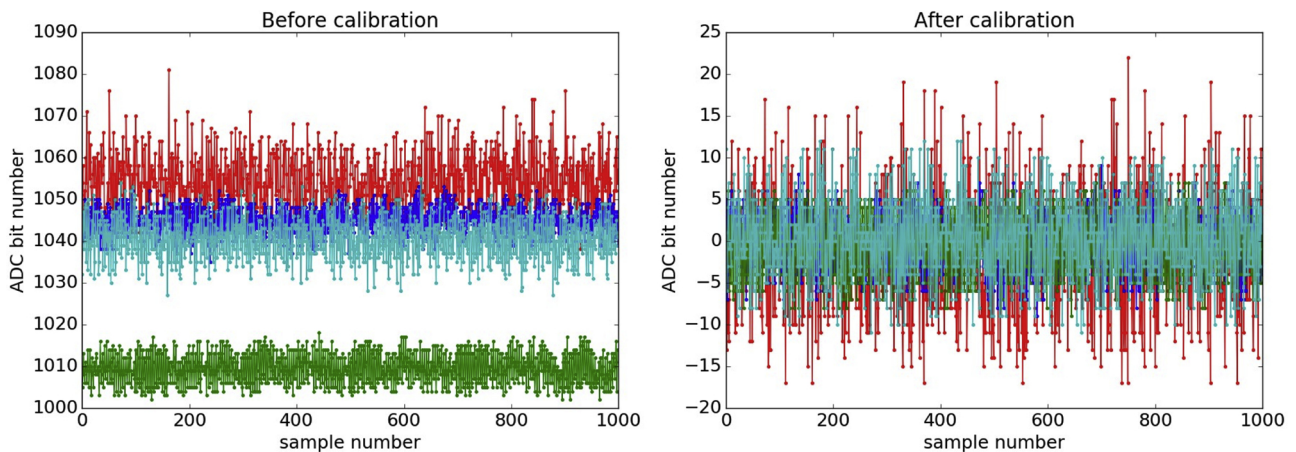


Fig. 6. The collected data calibrated in real-time to zero.

direct memory access to the PC using a linux driver [7].

4. Testing

To ensure the high level of reliability needed for the real-time protection system, a through testing strategy was developed. This testing strategy also needed to be able to be as streamlined as possible to reduce delays in functional testing and commissioning. The strategy developed involves application of virtual signals for testing that enables unit tests to be run on the FPGA but controlled from the RTP data collection PC. In addition, manual testing will also be carried out using an off the shelf 32 channel DAC unit that can be controlled remotely. This will produce predefined waveforms as inputs to mimic waveforms seen during a normal pulse. In implementing the virtual signal tests, external signal tests and automating them both, testing can be completed quickly. This facilitates any changes needed during testing as well as easily automating tests over a representative number of pulses of the expected RTP lifetime. This testing is carried out in addition to interface tests with all systems shown in Fig. 2. Integrated commissioning with power supplies will then be carried out and will be focused on running shots with reduced thresholds to ensure full protection functionality at levels that will not harm the machine.

5. Results

The setup in Fig. 4 was used to test the latency given by a loopback of a signal. A signal from a generator (ON/OFF) is input into the optical receiver modules and looped back via the WRS (with no filtering or calculations), to the optical transmitter modules, the latency is

measured on an oscilloscope. The transfer and decoding of the data using the aurora protocol without any processing is $2\mu\text{s}$ with this setup.

Filtering (see Fig. 5) has also been tested by applying the filter with coefficients shown in Fig. 5. This was calculated by convoluting a low pass filter and a notch filter at 125 kHz to attenuate a systematic noise contribution from the ADCs. The noise was reduced from 150 to 7 bits as shown from the comparison of graphs in Fig. 5. The 64-coefficient symmetric filter setup in the WRS will add an additional $60\mu\text{s}$ to the $2\mu\text{s}$ measured on the loopback test. The calibrations, calculations and mapping add a further $\sim 2\mu\text{s}$. These latencies match the overall latency requirements needed for MAST-U.

In addition, the analog signal calibration carried-out in RTP allows precise correction for the ADC offsets as shown when comparing graphs in Fig. 6. Initial testing of the calculation modules has also been carried out and shown that the functionality of these modules works as expected with minimal latency in comparison to the necessary latency added by the filter module. Furthermore, the system has shown reliable streaming of 400MB/s from the central FPGA to data storage PC without any loss of data and has routinely been used during testing. The WRS with all ADCs/integrators has also been tested and has been able to collect all signals simultaneously from all the different ADC/integrator modules for data processing in the FPGA.

The status of the system is nearing the end of the virtual signal testing stage, interface and testing involving external input of signals is expected to start in January 2019 ready for MAST-U power supplies off-coil commissioning.

6. Future plans

There are plans for development of a wider real-time network, which could be employed to perform divertor detachment control on fusion devices. This system would use the same technologies and firmware as the real-time protection system and would integrate with it. This would allow real-time control of the detachment front to ensure that divertor heat loads can be kept within reasonable operating limits

7. Conclusion

To ensure MAST-U operates within a safe operating range a protection system is needed that is able to react in real-time: within hundreds of microseconds of the machine moving towards a non-safe operating range. The Real-Time Protection system was developed, which was able to meet the challenging criteria set. Current results have met the specification and the system is currently undergoing a period of testing to validate the system ready for off coil commissioning.

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