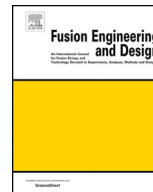




ELSEVIER

Contents lists available at ScienceDirect

Fusion Engineering and Design

journal homepage: www.elsevier.com/locate/fusengdes

Development of EUROFER97 database and material property handbook

 Ermile Gaganidze^{a,*}, Ferenc Gillemot^b, Ildiko Szenthe^b, Michael Gorley^c, Michael Rieth^a,
 Eberhard Diegele^{a,d}
^a Karlsruhe Institute of Technology, Institute for Applied Materials, Hermann-von-Helmholtz-Platz 1, 76344 Eggenstein-Leopoldshafen, Germany^b MTA Centre for Energy Research, H-1525 Budapest 114, P.O. Box. 49, Hungary^c Culham Centre for Fusion Energy, Abingdon, Oxfordshire, OX14 3DB, United Kingdom^d EUROfusion PMU, Boltzmannstrasse 2, 85748 Garching, Germany

ARTICLE INFO

Keywords:

 Material database
 Material property handbook
 Data qualification
 Design allowable

ABSTRACT

The current paper reports the work of the EUROfusion Material Database and Handbook group within the MAT-EDDI (Materials - Engineering Data and Design Integration) subproject of the EUROfusion consortium. A special emphasis is put on the building of the EUROfusion RAFM steel database accounting around 3000 raw materials data records. A data reviewing procedure is discussed for qualification of the data on EUROFER97 for material property handbook summarizing the material database content at a higher level and thus serving as a reference document for the structural design criteria development. Internationally recognized methodologies applied for the calculation of the average and minimum curves as well as for generation of the analysis data is presented and differences between different methodologies is addressed. The content and format of the material property handbook currently counting over 20 DEMO design relevant material properties on baseline steel EUROFER97 is summarized and discussed on the base of selected examples.

1. Introduction

The development of the DEMO Design Criteria (DDC) for in-vessel components of future fusion DEMONstration (DEMO) and power reactors requires building of a sound database on structural, armour and functional materials comprising physical and mechanical properties under various conditions, in particular in unirradiated and irradiated states [1]. Raw material data cannot be directly used in the design due to large dispersion of the data. The reasons underlying the data dispersion might be different and originated in i) variation of the material properties among different products and heats; or ii) a sensitivity of a property to the test and evaluation procedure. Exemplarily, surface finish quality is expected to have different influence e.g. on Low Cycle Fatigue properties of ferritic/martensitic steels while using sub-sized and standard specimens [2]. Qualification of the collated raw data is a mandatory step for the development of Material Property Handbook (MPH) summarizing the material database content at a higher level and thus serving as a reference document for the structural design criteria development [3]. In addition to the quality of the underlying data the conservatism of the calculated design allowables will have direct impact on the reliability and conservatism of the design rules. The examination of different internationally recognized methodologies for

allowable calculation e.g. the ones given in AFCEN RCC-MRx 2012 [4], ASME BPVC 2004 [5], ITER SDC-IC [6] is a mandatory step for identification of the methodologies suited for a given material under targeted operation conditions.

The current work summarizes the results of the EUROfusion Material Database and Handbook group as part of the MAT-EDDI (Materials - Engineering Data and Design Integration) subproject. The activities are currently focused on the Reduced Activation Ferritic/Martensitic (RAFM) steel EUROFER97 which is a European reference steel for ITER Test Blanket Module (TBM) and a potential candidate material for European DEMO. The article is organized as follows. First the status of the development of the EUROfusion RAFM steel database will be reported. In the subsequent sections the procedure for the qualification of the data for inclusion in MPH will be outlined and explained by selected examples. On the base of the tensile properties the application of different internationally recognized methodologies will be discussed aiming at the calculation of the average and minimum curves as well as analysis data. Finally, the format and structure of the MPH will be presented on the base of different examples.

* Corresponding author.

E-mail address: ermile.gaganidze@kit.edu (E. Gaganidze).<https://doi.org/10.1016/j.fusengdes.2018.06.027>

Received 14 February 2018; Received in revised form 29 June 2018; Accepted 29 June 2018

Available online 14 July 2018

0920-3796/ © 2018 Published by Elsevier B.V.

Nomenclature		Components	
AFCEN RCC-MRx	French Design and Construction Rules for Mechanical Components of nuclear installations : high-temperature, research and fusion reactors	LCF	Low Cycle Fatigue
ASME BPVC	The American Society of Mechanical Engineering - Boiler and Pressure Vessel Code	LM	Larson-Miller parameter
DEMO	DEMOstration power reactor	MPH	Material Property Handbook
DDC	DEMO Design Criteria	PWHT	Post Weld Heat Treatment
MAT	EUROfusion Materials Project	RAFM	Reduced Activation Ferritic/Martensitic
EDDI	Engineering Data and Design Integration	R _{p0.2}	0.2% offset proof stress
EFDA	European Fusion Development Agreement	RT	Room Temperature
EN	European Standard	RU	Research Unit
EUROfusion	The European Consortium for Development of Fusion Energy	S	Allowable stress intensity as defined in RCC-MRx
ITER	A world's largest tokamak under construction	SD	Standard Deviation
ITER SDC-IC	ITER Structural Design Criteria for In-vessel	S _m	Allowable stress intensity as defined in RCC-MRx
		S _{mB}	Allowable stress intensity as defined in RCC-MRx
		SSTT	Small Specimen Testing Technology
		S _t	Time dependent allowable stress intensity as defined in RCC-MRx
		TBM	Test Blanket Module

2. EUROFER97 database

The European RAFM steel EUROFER97 has been developed in the course of the systematic optimization of 9%CrWTA alloys [7]. The current study is limited to the 1st and 2nd industrial batches of 3.5 and 7.5 tonnes with 10 different heats and 18 different semi-finished product forms produced by EU steel manufacturers Böhler Austria GmbH and Saarschmiede GmbH [8]. The last heat treatments applied by producer included normalization at 980 °C for 15–30 min and tempering at 760 °C for 90 min for plates and normalization at 960–980 °C for 110–120 min and tempering at 750 °C for 220–240 min for rods. The impact of different tempering and annealing conditions on the microstructure and mechanical properties has been thoroughly studied at laboratory scale, for the results on selected product forms from the 1st batch of EUROFER97 the reader is referred to [9]. Specified concentrations of main alloying elements and radiologically undesired elements of EUROFER97 are summarized in Table 1.

Extensive examination and characterization campaigns have been carried out by several European Research Units (RUs) in the framework of the course of implementing the Contract of Association under EFDA (2001–2013) and within EUROfusion grants (since 2014). The raw materials data generated by RUs were made available either as scientific reports and open publications or in form of private communications kindly provided by responsible investigators. The majority of the mechanical properties used for the development of the EUROFER97 database are compiled from the following data sources [9,11–39].

Dedicated data acquisition templates developed at CEA [40] and further standardized by the EDDI group have been utilized for the collection of tensile, low cycle fatigue, impact, fracture toughness and creep data. In addition, new templates have been developed for specific testing needs, e.g. for collection of the physical and mechanical properties data. All relevant information on the heat, product form, heat treatment, irradiation condition, specimen geometry, test and

evaluation procedure as well as the testing results can be stored in the template thus allowing full traceability of the data from the results down to initial product. The EUROfusion EDDI RAFM steel database currently accounts around 3000 raw materials data records. Selected data have been reassessed aiming at completion of the required information or at judgment of the validity of the collected results according to the international testing standards.

3. Data qualification

A data reviewing procedure and quality thresholds have been elaborated for the exclusion and inclusion the data in the MPH. In the first step the integrity of the compiled data has been checked focusing on identification of i) material (manufacturer, heat/product, thermo-mechanical treatment ...); ii) specimen (geometry, extraction direction, ...); iii) irradiation condition; and iv) testing and evaluation procedure (testing standard, parameter, temperature, environment, results, validity ...). The calculation of the design allowables for MPH has been performed with the data passing the quality thresholds. In the following the data qualification procedure will be exemplarily shown for selected properties obtained on base metal EUROFER97. Aged data and irradiated data have been excluded for the calculation of the design allowables in the reference unirradiated state.

Fig. 1 summarizes the results of 0.2% offset proof stress, R_{p0.2}, on the 1st and 2nd batches of EUROFER97. Totally six different product forms (plates of different thicknesses, bars) are considered in the current plot. With respect to the yield strength, the differences between different batches and product forms turned out to be within the scatter band of the data measured on single product forms. Based on this observation no differentiation of tensile data has been done between different products for the MPH.

For the case when the collated information was in-complete the influence of the missing parameter on the property under consideration

Table 1

Specified chemical composition of EUROFER97 in weight % (wt%), Fe is balanced [10]. ALAP = as low as possible. Table is divided in main alloying elements and radiologically undesired elements.

Alloying elements	C	Cr	W	Mn	V	Ta	N ₂	P	S	B	O ₂
min value (wt%)	0.09	8.5	1.0	0.20	0.15	0.10	0.015			ALAP	
max value (wt%)	0.12	9.5	1.2	0.60	0.25	0.14	0.045	0.005	0.005	0.002	0.01
target value (wt%)	0.11	9.0	1.1	0.40		0.12	0.030				
Undesired elements	Nb	Mo	Ni	Cu	Al	Ti	Si	Co	As + Sn + Sb + Zr		
min value (wt%)	ALAP	ALAP	ALAP	ALAP	ALAP			ALAP			
max value (wt%)	0.005	0.005	0.01	0.01	0.01	0.02	0.05	0.01	0.05		

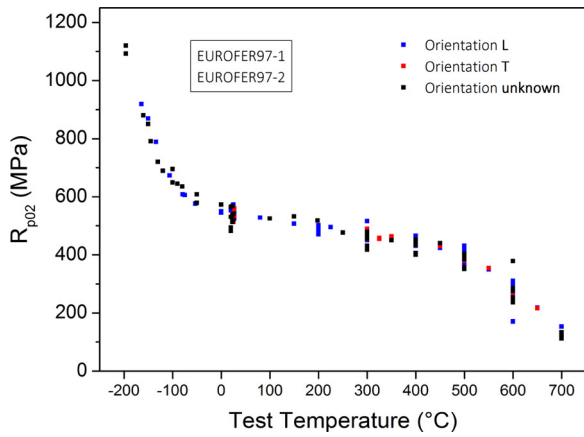


Fig. 1. R_{p02} proof stress of EUROFER97-1 and EUROFER97-2 for six different product forms [9], [11], [12], [19], [13], [14], [24], [20], [15], [17], [21]. The specimen orientations are indicated in the figure legend. (For identification of specimen orientations, the reader is referred to the web version of this article).

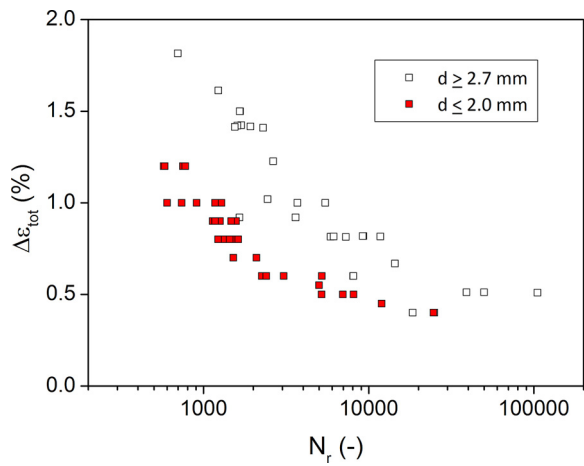


Fig. 2. Low cycle fatigue properties for EUROFER97 obtained by using SSTT type specimens ($d \leq 2\text{ mm}$) and large ($d \geq 2.7\text{ mm}$) specimens at test temperatures of $T_{\text{test}} \leq 350\text{ }^\circ\text{C}$ [33], [34], [23], [24].

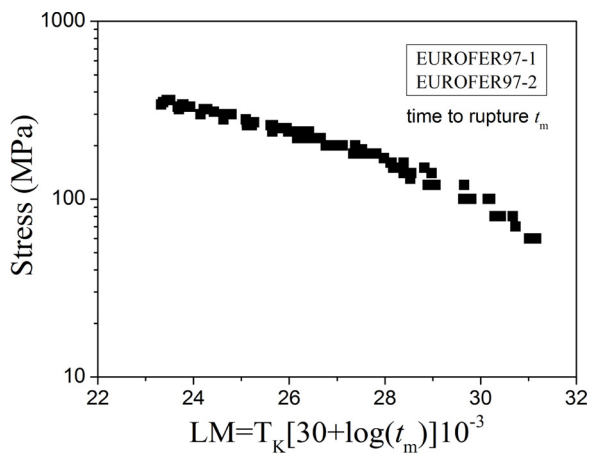


Fig. 3. Larson-Miller plot regarding the creep rupture time for four product forms from the 1st and 2nd batches of EUROFER97.

has been examined. The influence of the specimen orientation is exemplarily studied in Fig. 1. In additions to the results obtained in longitudinal and transverse orientations, the results available on specimens with unknown orientations are also included in the diagram.

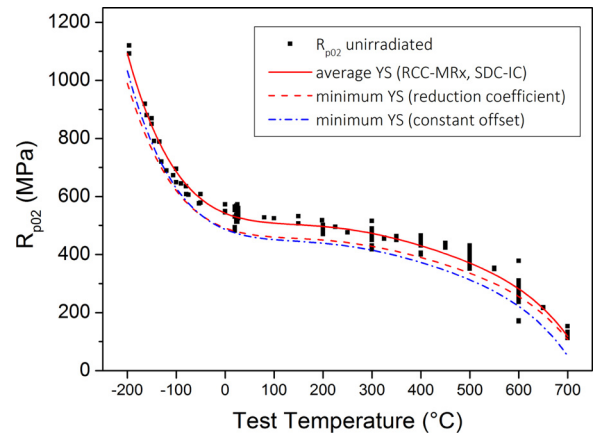


Fig. 4. R_{p02} yield strength along average and minimum curves calculated by means of different internationally accepted methodologies. The red solid line: an average yield strength curve determined by 5th order polynomial fitting to the data; the red dashed line: a minimum yield strength curve calculated on the base of Eq. (1) by using the minimum yield strength value determined by means of statistical methods; the blue dashed-dotted line: a minimum yield strength curve calculated following Eq. (2) (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article).

Table 2

Table of content of EUROFER MPH, release 2017 [41].

1.	SHORT INTRODUCTION AND OBJECTIVES OF WORK, CHANGES FROM THE LAST ISSUE	6
2.	GENERAL INFORMATION ON EUROFER97	8
3.	CHEMICAL COMPOSITION	11
4.	DENSITY	12
5.	YIELD STRENGTH	14
6.	TENSILE STRENGTH	22
7.	ELONGATION	28
8.	REDUCTION OF AREA	33
9.	YOUNG'S MODULUS	35
10.	POISSON'S RATIO	38
11.	CHARPY IMPACT ENERGY	39
12.	FRACTURE TOUGHNESS	45
13.	FATIGUE-CRACK-GROWTH RATE	50
14.	FATIGUE	53
15.	CREEP	58
16.	SWELLING	62
17.	RATCHETTING	63
18.	LINEAR THERMAL EXPANSION	64
19.	THERMAL CONDUCTIVITY	67
20.	THERMAL DIFFUSIVITY	70
21.	SPECIFIC HEAT	73
22.	MELTING TEMPERATURE	75
23.	ELECTRICAL RESISTIVITY	76
24.	MAGNETIC SATURATION	78
25.	REMNANT MAGNETIZATION	80
26.	COERCIVE FIELD	82

Specimen orientation is shown to have no measurable influence on the yield strength and consequently no differentiation has been done between different orientations for MPH.

The influence of the specimen geometry on the Low Cycle Fatigue (LCF) properties of EUROFER97 is shown in Fig. 2 for test temperatures below 350 °C. The use of SSTT type specimens with a diameter in the gauge section of 2 mm are found to strongly underestimate the lifetime of the material in comparison with the results obtained by using larger specimens. More pronounced influence of the surface imperfections (e.g. grooves introduced during the turning of the specimens in the workshop) on the lifetime for the SSTT specimens were attributed to the higher ratio of imperfection size to the specimen diameter in comparison with the larger specimens [2]. On the base of the assessment of the results in Fig. 2 the results obtained on the SSTT specimens have been excluded for the MPH allowable calculations. Similar to the tensile

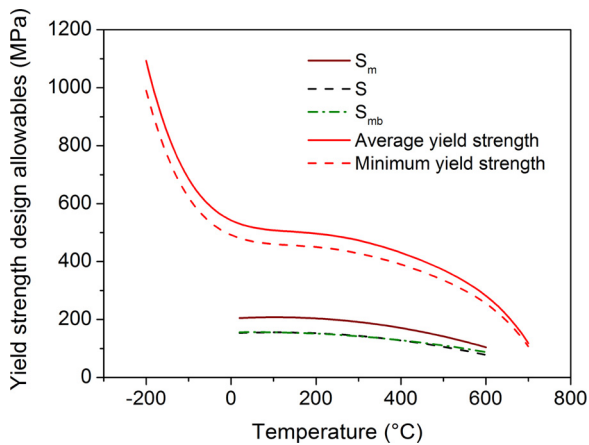


Fig. 5. The averaged and minimum values of the yield strength together with the S_m , S and S_{mb} allowables calculated according to the RCC-MRx methodology [41].

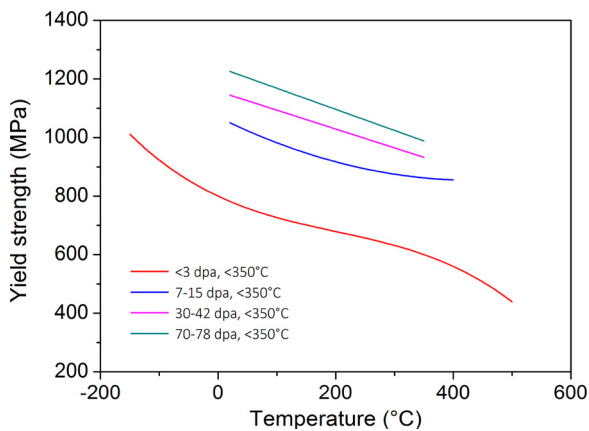


Fig. 6. The effects of irradiation on yield strength of EUROFER97, below 350 °C [41].

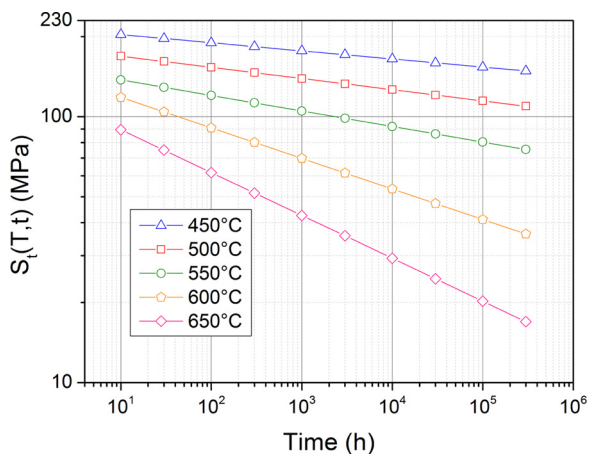


Fig. 7. Creep allowable stress [41].

properties no differentiation has been done between different product forms and between different orientations.

Approximately 140 original creep curves have been analysed with respect to the design relevant parameters e.g. onset of the tertiary creep, time to reach 1% total strain, time to reach 0.05% creep strain, etc. A Larson-Miller plot of creep properties constructed for the rupture time t_m is shown in Fig. 3 for the 1st and 2nd batches of EUROFER97. The results were found to follow common trend curve without

substantial differences for the two batches and consequently no differentiation has been done between different heats for MPH.

4. Procedures for allowable calculation

Internationally recognized methodologies AFCEN RCC-MRx [4], ASME BPVC [5] and ITER SDC-IC [6] have been applied to the qualified data for calculation of the average and minimum curves as well as for the generation of analysis data. Independently from the design codes the average values of the properties are determined by a statistical method on the basis of the sufficient number of data on the representative samples. Fitting of the data with a polynomial function was found to describe fairly well the temperature evolution of most of the time independent mechanical properties. Exemplarily, the average curve obtained by 5th order polynomial fitting to the yield strength data is shown by red solid line in Fig. 4.

Within different design and construction codes different approaches are used for calculation of minimum mechanical properties at elevated temperatures [4–6]. One possible way is the application of constant reduction coefficient to the average curve $R_{p02,av}(T)$ according with the following equation:

$$R_{p02,min}(T) = \frac{R_{p02,min}(RT)}{R_{p02,av}(RT)} R_{p02,av}(T) \quad (1)$$

Here $R_{p02,min}(RT)$ is a minimum yield strength at RT which can either be specified within the material technical specification or calculated on the base of statistical analysis by $R_{p02,min}(RT) = R_{p02,av}(RT) - 1.96 \cdot SD_{RT}$, with SD_{RT} being the standard deviation at RT.

Alternatively, minimum curve can be calculated on the base of the statistical analysis of the whole dataset according with the following equation

$$R_{p02,min}(T) = R_{p02,av}(T) - 1.96 \cdot SD \quad (2)$$

Here SD denotes the standard deviation obtained for the whole dataset in the procedure for the determination of $R_{p02,av}(T)$ curve. By definition Eq. (2) gives the 97.5% probability of sample exceeding the minimum.

Eq. (1) is conventionally used by ASME BPVC for determination of minimum yield strength at elevated temperatures by applying specified value of the minimum yield strength at RT, whereas Eq. (2) is typically used in ITER SDC-IC. As for AFCEN RCC-MRx code the minimum values of mechanical properties are given either by EN standards for the corresponding grades or determined by means of the statistical analysis or determined on the base of minimum values specified at RT. The example of minimum yield strength calculated by using Eq. (1) with RT minimum yield strength calculated by means of statistical methods is given by the red dashed line in Fig. 4. On the other hand blue dashed-dotted line in Fig. 4 shows the minimum value calculated on the base of the statistical analysis of the whole dataset following Eq. (2). It can be seen that minimum curve according with Eq. (2) yields more conservative results at elevated temperatures in comparison with the curve calculated according with Eq. (1). It has to be noted that application of Eq. (2) would require sufficiently large number of test results in the whole temperature range and consequently case by case study will be required in order to check whether Eq. (2) can be applied to the a given property for a given material. To determine the minimum values of yield strength and ultimate tensile strength for MPH we made use of Eq. (1) by using the minimum value of the RT yield strength calculated on the base of statistical methods, $R_{p02,min}(RT) = R_{p02,av}(RT) - 1.96 \cdot SD_{RT}$. This procedure can be however revised in the future taking into account the needs of the European DEMO Design Criteria being currently under development. Variation of the confidence levels as well as subdivision of the temperature domains shall be investigated to determine reliable minimum curves and to avoid unnecessary conservatism.

5. EUROFER97 material property handbook

The EUROFER chapter of the MPH has been developed as the “pilot project” by the EDDI group. The format of the MPH is largely based on the format of ITER MPH. In contrast to the ITER MPH, however, the raw data points are not shown in the MPH in order not to violate intellectual property rights of data owner RUs. The data points are instead stored in the EUROfusion EDDI database and the procedures for the allowable calculations are justified in separate EUROfusion task reports. Table 2 shows the content of the EUROFER MPH. For the case when the material data were missing, e.g. for ratcheting behaviour, place holders have been introduced in the MPH. Currently, MPH summarizes over 20 DEMO design relevant material properties on base metal EUROFER97.

Each property section provides identification of material, brief description of the property under consideration followed by relevant plots and tables. The influence of the irradiation is given in the *aged values* subsection of the property. Furthermore, in addition to the average and minimum curves selected allowables (e.g. S_m , S , S_{mb}) have been calculated by applying the RCC-MRx methodology [4]. Finally, at the end of each property paragraph a list of the references used for the calculation of the design allowables is given. This paper has no intention to report on the whole design allowables determined for MPH, instead aiming at giving the first insight into MPH selected examples will be briefly discussed below.

Fig. 5 is a reproduction of the yield strengths design allowables from MPH [41]. As already mentioned above in contrast to Fig. 4 the underlying data is removed from the MPH. This improves a readability of the document. Furthermore the tabulated values of the allowables together with the corresponding formulas given in MPH make the handling of the allowables straightforward for the designers.

Fig. 6 shows the effects of the neutron irradiation on the yield strength for low irradiation temperatures. Due to limited statistics of the irradiated data, only trend curves are provided for the data grouped according to their irradiation conditions. An adequate trend curve is also provided for high irradiation temperatures where the influence of the neutron irradiation is substantially suppressed.

According to the RCC-MRx code [4] the $S_r(T,t)$ stress allowables are defined as the least of the following quantities: i) 2/3 of the minimum stress inducing fracture at a given temperature T and time t ; ii) 80% of the minimum stress leading to the appearance of the tertiary creep and iii) the stress inducing total strain (elastic + plastic + creep) of 1%. Due to lack of the statistics 80% of the rupture stresses have been used as the estimate of the minimum values of the rupture stresses in the same conditions. The stresses leading to the onset of the tertiary creep stage have been evaluated from the original creep curves by using the 0.2% offset of the secondary creep stage. Also the stresses inducing total strain (elastic + plastic + creep) of 1% have been derived on the base of the analysis of the original creep curves and by taking into account initial elastic plus plastic strains. The determined values of $S_r(T,t)$ are summarized in Fig. 7. $S_r(T,t)$ values were found to be governed by 2/3 of minimum stress to rupture.

Concluding this section we would like to emphasize that actual release of MPH [41] is developed within a pilot project. This means that the current document will be further evolved in order to address the need of the DEMO Design Criteria as well as to close the known gaps in the design allowables. Dedicated experimental campaigns will be required for closing the database gaps particularly in fracture toughness, creep-fatigue, ratcheting, fatigue crack growth, etc. properties both in the unirradiated and irradiated states. Full qualification of the weldments exposed to the suitable Post Weld Heat Treatments (PWHT) compatible with the DEMO design will be required in addition for development and validation of the design rules with respect to the joints. Complete identification of the missing data and elaboration of the detailed testing matrices requires close collaboration between the experts from database, testing, design and technology areas from relevant EUROfusion projects and is currently under progress.

6. Summary

In the current work we reported on the development of EUROfusion material database and material property handbook on European reference RAFM steel EUROFER97. The EUROfusion EDDI RAFM steel database currently accounts around 3000 raw materials data records. The quality thresholds for the assessment of the data integrity have been introduced and the reviewing procedure for qualification of the data on EUROFER97 for material property handbook has been discussed. The application of different internationally recognized methodologies has been examined for calculation of the average and minimum curves as well as analysis data. The content and format of the MPH currently covering over 20 DEMO design relevant properties have been explained on the base of selected examples. The needs for the further optimization of the methodologies for calculation of the design allowables as well as the needs for the closing the gaps in the material database have been addressed.

Acknowledgments

This work has been carried out within the framework of the EUROfusion Consortium and has received funding from the Euratom research and training programme 2014–2018 under grant agreement no. 633053. The views and opinions expressed herein do not necessarily reflect those of the European Commission.

References

- [1] A.-A.F. Tavassoli, A. Alamo, L. Bedel, L. Forest, J.-M. Gentzbittel, J.-W. Rensman, et al., Materials design data for reduced activation martensitic steel type EUROFER, *J. Nucl. Mater.* 329–333 (2004) 257–262.
- [2] M. Walter, Eurofer 97—size effects under cyclic loading, The 15th International Conference on Fusion Reactor Materials, Charleston, USA, 2011.
- [3] M. Porton, J. Aktaa, C. Bachmann, P. Fernandez, M. Kalsey, T. Lebarbe, C. Petesch, W. Timmis, Structural design criteria development needs for a European DEMO, *Fusion Sci. Technol.* 66 (2014) 18–27.
- [4] AFCEN, RCC-MRx, Design and Construction Rules for Mechanical Components of Nuclear Installations, (2012).
- [5] THE AMERICAN SOCIETY OF MECHANICAL ENGINEERS, ASME Boiler and Pressure Vessel Code—Rules for Construction of Nuclear Facility Components, New York (2004).
- [6] ITER Organization, ITER Structural Design Criteria for In-Vessel Components (SDC-IC), ITER, 2004.
- [7] A. Moeslang, E. Diegele, M. Klimiankou, R. Laesser, R. Lindau, E. Lucon, et al., Towards reduced activation structural materials data for fusion DEMO reactors, *Nucl. Fusion* 45 (2005) 649–655.
- [8] R. Lindau, A. Moeslang, M. Rieth, M. Klimiankov, E. Materna-Morris, A. Alamo, et al., Present Development Status of EUROFER and ODS-EUROFER for Application in Blanket Concepts 75–79 (2005), pp. 989–996.
- [9] M. Rieth, M. Schirra, A. Falkenstein, P. Graf, S. Heger, H. Kempe, R. Lindau, H. Zimmermann, EUROFER97 Tensile, Charpy, Creep and Structural Tests, Forschungszentrum Karlsruhe, Wissenschaftliche Berichte, FZKA 6911, 2003.
- [10] European Fusion Development Agreement, „Procurement of reduced activation ferritic-martensitic steel type 9CrWtV (EUROFER) for the TBM fabrication technology trials and mock-ups, Annex A, Technical Specification to contract No EFDA 06/1903, 27 September 2006“.
- [11] E. Lucon, Mechanical properties of the European reference RAFM steel (Eurofer97) before and after irradiation at 300°C (0,3–2 dpa), Irfuma I-III, EFDA TW2, Materials Development - TTMS-001, SCK-CEN Mol, BLG-962, (2003).
- [12] P. Fernández, A.M. Lancha, J. Lapeña, M. Serrano, M. Hernández-Mayoral, Reduced activation ferritic/martensitic steel Eurofer97 as possible structural material for fusion devices, metallurgical characterization on as-received condition and after simulated service conditions. Technical Report CIEMAT. Number 1048. December, 2004. ISSN: 1135-9420.
- [13] J. Rensman, NRG irradiation testing: report on 300°C and 60°C irradiated RAFM, EFDA TW2-TTMS-001a D6 and TW2-TTMS-001b D12, Nuclear Research and Consultancy Group (NRG), 20023/05.68497/P, 2005.
- [14] E. Materna-Morris, Ch. Adelhelm, S. Baumgärtner, B. Dafferner, A. Falkenstein, S. Heger, R. Lindau, P. Graf, C. Petersen, M. Rieth, R. Ziegler, H. Zimmermann, "Structural Material EUROFER97-2, Characterization of 100 mm Rod Material: Structural, Tensile, Charpy, and Creep Properties," EFDA TW4-TTMS-005 D2, Forschungszentrum Karlsruhe, 2006.
- [15] E. Lucon, W. Vandermeulen, Overview and critical assessment of the tensile properties of unirradiated and irradiated EUROFER97, EFDA TW5-TTMS-001 D6, Open Report SCK-CEN-BLG-1042 REV(1), (2007).
- [16] P. Spaetig, P.F. Mueller, T. Kruml, Assessment of irradiations performed on EUROFER97. Comparison and critical review of the fracture properties and

- microstructures of RAFM steels, TW5-TTMS-001 D7, Ecole Polytechnique Federale de Lausanne (CRPP-EPFL), (2008).
- [17] P. Spätig, „Effects of proton irradiations on the mechanical properties of the Eurofer97 steel, Final Report TASK TW1-TTMS-001 del. 3 Period 01/2002 – 12/2006, “CRPP-EPFL, 2007.
- [18] E. Gaganidze, B. Dafferner, H. Ries, R. Rolli, H.-C. Schneider, J. Aktaa, "Irradiation Programme HFR Phase IIb (SPICE), Impact testing on up to 16.3 dpa irradiated RAFM steels," EFDA TW2-TTMS 001b-D05, Forschungszentrum Karlsruhe, FZKA 7371, 2008.
- [19] A. Alamo, P. Wident, Y. Tournier, S. Urvoy, Mechanical properties of Eurofer 97 steel in the as-received condition, CEA Report NT SRMA 01-2419, (2001).
- [20] A. Alamo, J.L. Bertin, V.K. Shamardin, P. Wident, Mechanical properties of 9Cr martensitic steels and ODS-FeCr alloys after neutron irradiation at 325 °C up to 42 dpa, *J. Nucl. Mater.* 367–370 (2007) 54–59.
- [21] J. Henry, X. Averty, A. Alamo, Tensile and impact properties of 9Cr tempered martensitic steels and ODS-FeCr alloys irradiated in a fast reactor at 325 °C up to 78 dpa, *J. Nucl. Mater.* 417 (2011) 99–103.
- [22] C. Petersen, Post irradiation examination of RAF/M steels after fast reactor irradiation up to 33 dpa and < 340°C (ARBOR 1), EFDA TW2-TTMS-001b D9, Karlsruher Institut für Technologie, FZKA 7517, 2010.
- [23] E. Gaganidze, C. Petersen, Post irradiation examination of RAFM steels after fast reactor irradiation up to 71 dpa and < 340 °C (ARBOR 2)," EFDA TW5-TTMS-001 D10, Karlsruhe Institute of Technology, KIT Scientific Report 7596, 2011..
- [24] E. Materna-Morris, A. Möslang, H.-C. Schneider, Tensile and low cycle fatigue properties of EUROFER97-steel after 16.3 dpa neutron irradiation at 523, 623 and 723 K, *J. Nucl. Mater.* 442 (2013) 62–66.
- [25] E. Materna-Morris, A. Möslang, S. Baumgärtner, B. Dafferner, J. Ehrmann, E. Gaganidze, M. Holzer, S. Lautensack, H. Ries, R. Rolli, H.-C. Schneider, H. Zimmermann, Irradiation Programme HFR IIb (SPICE-T), Post-irradiation examinations after 16.3 dpa, tensile properties, fatigue properties, fractography and structure analysis after Charpy and tensile tests, EFDA TW2-TTMS 001b-D05, Forschungszentrum Karlsruhe, (2008).
- [26] H.-C. Schneider, Entwicklung einer miniaturisierten bruchmechanischen Probe für Nachbestrahlungsuntersuchungen, Doktorarbeit, Universität Karlsruhe (TH), 2005, Forschungszentrum Karlsruhe, Wissenschaftliche Berichte, FZKA 7066, Germany (2005).
- [27] N. Ilchuk, P. Spätig, G.R. Odette, Fracture toughness characterization in the lower transition of neutron irradiated Eurofer97 steel, *J. Nucl. Mater.* 442 (2013) 58–61.
- [28] M. Kytka, M. Brumovsky, M. Falcnik, Irradiation embrittlement characterization of the EUROFER 97 material, *J. Nucl. Mater.* 409 (2011) 147–152.
- [29] R. Chaouadi, Effect of irradiation-induced plastic flow localization on ductile crack resistance behavior of a 9%Cr tempered martensitic steel, *J. Nucl. Mater.* 372 (2006) 379–390.
- [30] E. Gaganidze, Assessment of Fracture Mechanical Experiments on Irradiated EUROFER97 and F82H Specimens, EFDA TW5-TTMS 001 D14, Forschungszentrum Karlsruhe, Wissenschaftliche Berichte, FZKA 7310, 2007.
- [31] R.A. Bonade, Constitutive behavior and fracture properties of tempered martensitic STEELS for nuclear applications: experiments and modeling, ÉCOLE POLYTECHNIQUE FÉDÉRALE DE LAUSANNE, PhD Thesis, (2006).
- [32] P. Mueller, P. Spätig, R. Bonadé, G.R. Odette, D. Gragg, Fracture toughness master-curve analysis of the tempered martensitic steel Eurofer97, *J. Nucl. Mater.* 386–388 (2009) 323–327.
- [33] R. Schmitt, C. Petersen, "Isothermal Low Cycle Fatigue Of Reduced Activation Ferritic/Martensite (RAF/M) Materials," EFDA TTMS-002 D19, FZKA 6942, Forschungszentrum Karlsruhe, 2004.
- [34] P. Marmy, "Low cycle fatigue and creep-fatigue of Eurofer97," EFDA TW3-TTMS-005 D1, Ecole Polytechnique fédérale de Lausanne, LRP 826/06, Switzerland, 2006.
- [35] P. Fernandez, LCF Properties of EUROFER, CIEMAT, 2014 Private communication.
- [36] N.V. Luzginova, J.-W. Rensman, Assessment of Eurofer97 LCF, FCP, Hold Time Effects, and Irradiation Stress Relaxation, EFDA TW5 TTMS-001 D12, D13, Nuclear Research and Consultancy Group (NRG), 2009.
- [37] J.-W. Rensman, M. Jong, P. ten Pierick, T. Bakker, "Fatigue of (un)irradiated Eurofer97 between 450°C and 550°C," EFDA TW2-TTMS-001b-D1, Nuclear Research and Consultancy Group, NRG-20903/10.105274, 2010.
- [38] M. Rieth, S. Hegger, Creep Properties of EUROFER97," KIT, private communication, 2015.
- [39] F. Tavassoli, Comparison of 316L(N) -IG and Eurofer for Early DEMO, EFDA-WP13-MAT-02-01, CEA, 2013.
- [40] F. Tavassoli, Eurofer Steel, Development to Full Code Qualification, *Procedia Eng.* 55 (2013) 300–308.
- [41] EUROfusion Consortium, MAT-Project, „Materials Property Handbook, 2nd formal release, Grant Deliverable MAT D25.15, “ 2017.