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Abstract

A physics and engineering analysis of alternative divertor configurations is carried out by examining benefits and problems by comparing the baseline single null solution with a Snowflake, an X- and a Super-X divertor. It is observed that alternative configurations can provide margin and resilience against large power fluctuations, but their engineering has intrinsic difficulties, especially in the balance between structural solidity and accessibility of the components and when the specific poloidal field coil positioning poses further constraints. A hybrid between the X- and Super-X divertor is proposed as a possible solution to the integration challenge.

I. INTRODUCTION AND METHODOLOGY

As fusion enters the delivery era, and the community plans and designs large machines in the reactor class, a greater emphasis is placed on the issues associated with the exhaust of the plasma. These include, but are not limited to, the protection of the surfaces of all the components exposed to the plasma, both in steady state and during transients, the efficient pumping of the helium ashes, which would otherwise choke the fusion reactions, the minimization of the pollution of the core plasma from intrinsic and seeded impurities. While all these essential functions of an exhaust system must be ensured in a reactor, the biggest challenge is to integrate them among each other and especially with the rest of the machine. Indeed, it is crucial that the performance of core physics is not degraded by the exhaust design choices and, equally, that these are compatible with the often severe engineering constraints that a reactor will have.

The problem is exacerbated by the fact that next generation devices will be much more demanding than current machines in terms of both physics and engineering. The power that needs to be handled by the exhaust system scales with the fusion power we want to achieve, and this fact is in the most fundamental laws of fusion physics, as it is connected with the production of α particles. Practically, this means that for a \sim GW reactor the power that needs to be safely absorbed by the walls is in the hundreds of megawatts, at least one order of magnitude larger than what we are experiencing in today's largest tokamaks. Additionally, neutron irradiation with unprecedented high fluence, very large confining fields ($\sim 10T$) and plasma currents ($\sim 15MA$), contributes to the challenge. Finally, the engineering of the reactor poses new limitations on what can be built, as plasma facing material properties, remote maintenance and installation, port dimensioning and acceptable forces and stresses on the structural components all conspire to complicate the design.

Focusing on the exhaust system, one of the biggest concerns is to find an operational space that is sufficiently robust and reliable, even in the presence of unavoidable off-normal events and under uncertainty. In particular, the first line of defence against the exhausted power, the divertor, has to be able to sustain steady state loads that, if unmitigated, would reach hundreds of MW/m^2 , well beyond acceptable structural limits for the plasma facing components. Additionally, once in the operating mitigated state, the divertor needs to be able to dissipate the additional power that unexpected transients could produce (maybe

from failed pellet injection, radiation fluctuations or emergency ramp downs).

The European DEMO design [1] is based on the ITER exhaust solution: a single null divertor (SND) with vertical targets [2, 3]. However, extrapolation is not obvious, as the two machine will operate in different regimes. Core radiation will be much larger in DEMO ($\sim 66\%$ versus $\sim 33\%$ in ITER) but with similar power crossing the separatrix ($\sim 150MW$ for DEMO and $\sim 100MW$ for ITER). This means that DEMO will have a large upstream reservoir of power ($\sim 300MW$ versus $\sim 50MW$) that can endanger a divertor fully detached and under a lot of strain. To give the measure of the problem, a 10% variation in core radiation would unleash an additional $\sim 30MW$ towards a divertor that in its ideal operation point already needs to dissipate 90% of the power it receives (optimistically assuming a wetted area of $3m^2$ and material limits at $5MW/m^2$). The DEMO divertor will therefore need to operate in fully detached conditions (ITER will be semi-detached), which implies that there is a risk the detachment front could reach the X-point and cool off the pedestal or destabilize the discharge. Active detachment control, however, might not be possible in DEMO due to lack of neutron resistant sensors and actuators, thus solutions that provide passive stabilization of the detachment front would be helpful.

These observations motivate research of alternative divertor configurations (ADCs) for the plasma exhaust. EUROfusion has studied these alternatives in a systematic way and initial results were already reported elsewhere [4]. Here we give an updated and comprehensive report of recent and important finding in this area, which mix both physics and engineering considerations. While the potential benefits need to be weighted against the unavoidable cost that the additional complexity entails, the latter must be accepted if the SND cannot provide a solution. In particular, we investigated four ADCs: the double null (DND), the Snowflake (SFD) [5, 6], the X (XD) [7] and Super-X (SXD) [8] divertors. Apart from the first, which will be treated in a separate publication [9], each other one will be discussed independently and from their comparisons we will draw our conclusions.

It is in the nature of our analysis to be comparative. Indeed, given the large uncertainties on exhaust physics and technology, and the unprecedented level of complexity of the problem, the only wise approach is to dismiss predictions that aim at absolute values and rather focus on similarities, differences and trends observed between the configurations investigated. This, however, requires a rigorous methodology in which analyses are carried out in a standardized way, with the same tools and with agreed procedures, so that the

comparison is fair. Despite the triviality of this argument, its practical application is far from easy.

The second important methodological aspect is that the work presented was deeply integrated, with cross-fertilization and continuous exchanges between the physics and engineering aspects, so to form a consistent picture where each configuration analysed can be represented as a single entity. This is the way we choose to present our results, with one section for each solution, despite the fact that the actual work was carried out across configurations.

Finally, the results presented here must be interpreted as a step in the right direction rather than a conclusive assessment of the properties of the ADCs, or a recommendation for how to build an exhaust system for a reactor. Indeed, we started from ADCs for DEMO that included the features that were originally predicted to be beneficial, but that are not yet optimized. This initial attempt cannot lead to the 'right' solution straight away, as this must be the result of iterations based on the lessons learned.

II. CONFIGURATIONS AND REFERENCE

Our analysis started with equilibria previously elaborated and discussed in [4], see Fig.4 in that paper. For each configuration, it is possible to find a solution that is sustained only by external coils (i.e. external to the toroidal coils cage) and in which forces and macroscopic engineering constraints are satisfied (see [4] for further details, including the machine characteristics). More refined structural calculation, which show issues for the mechanical stresses in the toroidal field coils, will be discussed later on. While the analysis on this paper will be based on the '2018' configurations discussed in [4], new and updated 2D poloidal sections have been further elaborated and modified to include ports compatible with remote handling and are shown in Fig.1, where also the vacuum vessel (VV), the breeding blankets (BB), the toroidal (TF) and poloidal (PF) coils are depicted. The position of the PF coils and the shape of the TF coils is optimized as far as the constraints discussed above are concerned. However, the configurations are not yet designed to achieve optimal structural conditions in the TF coils or for the maximization of the physical benefits.

The SND design is the baseline DEMO divertor and will be used as a reference against all the other designs. This configuration is more optimized on the engineering side, and

already incorporates refined considerations on divertor, remote handling [1] and breeding blanket integration. We therefore had to simplify some of its features so that it could be at the same level of maturity of the ADCs in order to have a fair comparison (especially for structural calculations).

Multifluid simulations were carried out with SOLPS-ITER in order to identify the operating space of the machine, defined as the parameter set when the maximum heat flux on the divertor is below $10\text{MW}/\text{m}^2$, the target temperature is below 5eV (due to limits on the erosion), and the separatrix Greenwald fraction is below 0.6. The simulations evolved Deuterium, Helium and Argon (used as a seeded impurity and bundled), assumed fluid neutrals, no drifts and a fusion power of 2GW . This implies that, with a core radiation fraction of 66%, the power crossing the separatrix accounts for 150MW . Also, given the fusion power, also the core Helium production rate is fixed at $7 \cdot 10^{20}$ particles per second. A core Deuterium puffing rate of $3.5 \cdot 10^{22}$ particles per second simulates pellet injection, while gas puff is used as a scanning parameter, Γ_D , as well as the Ar seeding rate, Γ_{Ar} . All equi-

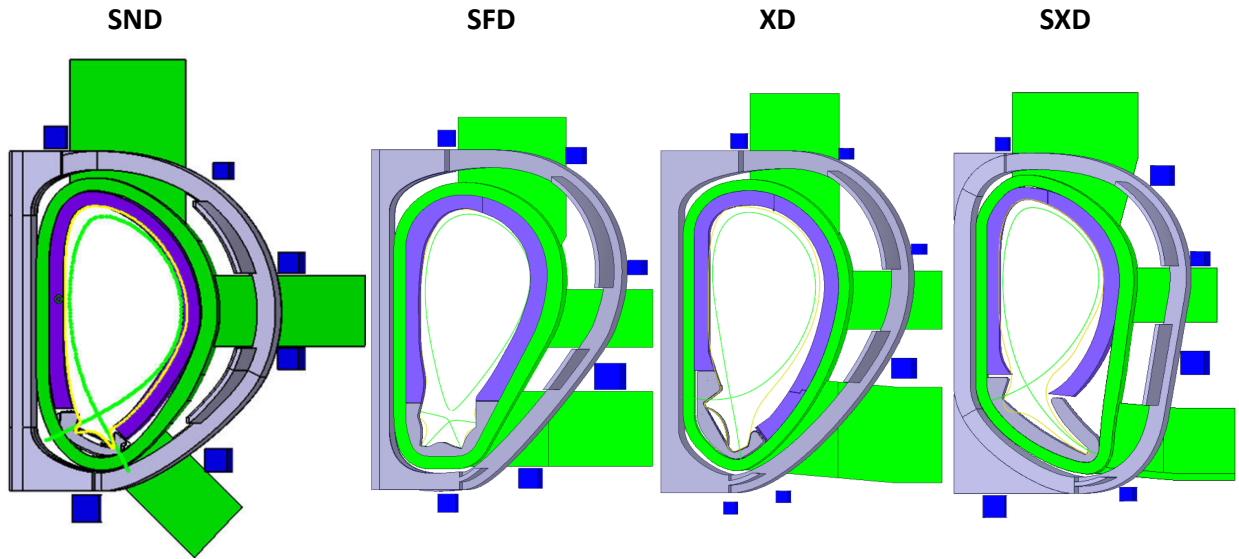


FIG. 1. Cross sections for the different configurations. TF coils and intercoil structures and divertor cassette in grey, PF coils in blue, BB in purple, VV and ports in green. The plots are not in scale, as the plasma volume is constant in all cases (2350m^3).

libria had a the same target angle of 1.5° to ensure a fair comparison. Large uncertainties afflict the predictions of the transport coefficients, which are therefore fixed by rescaling the values used for ITER simulations [3] in such a way that the midplane heat flux decay length is 3mm. Therefore, $D = 0.1m^2/s$ and $\chi_i = \chi_e = 0.3m^2/s$ in the SOL, with the heat transport coefficients reduced to $0.17m^2/s$ in the transition region spanning 5mm inside the separatrix and to $0.1m^2/s$ in the core (i.e. deeper than 5mm from the separatrix). This roughly simulates a temperature pedestal with a weaker density pedestal, representative of generic no-ELM regimes. Additional information on the simulation set-up can be found in [9, 10]. The results of the simulations for the reference case are shown in Fig.2, where He concentration at the separatrix density is plotted as a function of the seeding and fuelling levels. Additional curves bound the acceptable operating regime, as given by the physics constraints discussed in the previous paragraph plus the separatrix Ar concentration. The acceptable operating space lies in the region internal to these curves. A potential concern, is the Tritium throughput in a 50%-50% mix, which is very large for all the configurations ($\sim 3-5kg/h$). However, our performance could be maintained by decreasing the throughput and reducing the pumping efficiency, as done for the ITER simulations [3].

Simulations carried out with state-of-the-art European 3D SOL turbulence codes (GBS, GRILLIX, STORM/BOUT++, TOKAM3X) show filamentary transport in the Scrape Off layer both above and below the divertor, confirming experimental observations and previous numerical results. These 3D simulations are too computationally intensive for realistic DEMO parameters and hence they had to be rescaled to medium size tokamak dimensions. While this will surely affect the physics, it should still allow comparison between different designs and especially provide a first indication of the poloidal variations of the transport coefficients.

Moving to engineering, Finite Element Method structural calculations of the TF coils were performed using ANSYS, focusing on the effect of the electromagnetic (EM) loads. These can be divided into hoop forces, describing the expansion of a closed current carrying conductor, and out-of-plane forces, generated by the interaction between the TF coil current and the poloidal magnetic field induced by the PF coils. The hoop forces can be minimized by producing a constant tension design known as Princeton D-shape [11]. Clearly, the ADCs cannot be designed with this optimal bending-free solution in mind, and we will see that this creates issues. However, also the current version of the SND design is not optimized in

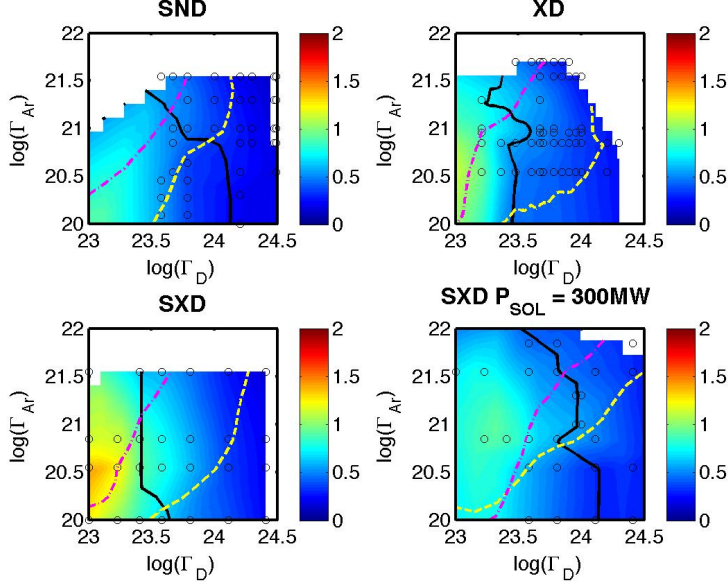


FIG. 2. Comparison between operating spaces in different configurations. The colour plot represents the He concentration at the outer midplane separatrix (in %) as a function of the base 10 logarithm of the imposed Deuterium, Γ_D and Argon Γ_{Ar} fluxes, measured in s^{-1} . The lines represents the isocontour for $T = 5eV$ at the inner or outer divertor (solid), the a Greenwald fraction of 0.6 at the separatrix (dashed), and an Ar concentration of 1% at the outer midplane separatrix (dot-dashed). The constraint on the target heat load is not shown because it is always less stringent that the temperature one.

this respect and the shape of the TF coils will probably need to be modified to be capable to withstand the EM forces. This will either require the increase of their height or their number. In terms of limits, stress linearization was used to assess the designs where the peak static stress intensity appears to be problematic [12]. The allowable stress value, S_m , is set to 2/3 of the material's yield strength at a temperature of 4K, which is 1000 MPa for the EC1 strengthened austenitic steel we consider. According to the RCC-MRx rules, the primary membrane stress, P_m , must be such that $P_m < \alpha S_m$, the primary membrane plus bending stress, P_{mb} , such that $P_{mb} < 1.3\alpha S_m$ and the primary membrane plus bending plus peak stress P_{mbp} , such that $P_{mbp} < 1.5\alpha S_m$. High and low field side parts of the TF coil have different limits, so that for the former $\alpha = 1$ and for the latter $\alpha = 3/4$, reflecting the fact that the inner section is forged and the outer cast.

The analysis was performed using a simplified winding pack geometry composed by six

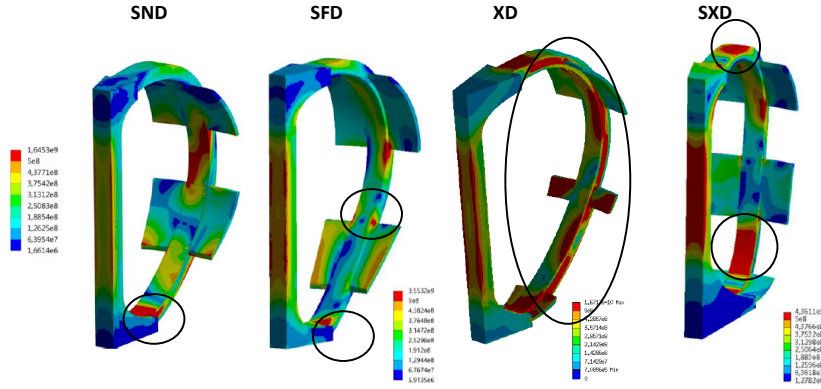


FIG. 3. Stress map for the different configurations (in Pa). Note that the maximum of the colormap is based on the outer limb peak threshold of 500MPa, which is the most conservative limit. Hence several areas present acceptable stresses despite being red. The black ellipses identify areas where stresses are unacceptably high.

layers with smeared material properties meshed with hexahedral elements, while the case and the filler use tetrahedral elements to improve the contact behaviour (a friction coefficient of 0.3 has been chosen between the casing and the filler, which can slide). The boundary conditions simulate the periodic behaviour between individual TF elements. In reality, the inner leg of the TF coils can slide with respect to each other and we carried out a series of stress analyses allowing for the possibility of separation. However, our preliminary results show that the differences between the two approaches are small as far as equivalent stresses are concerned, thus giving us confidence in our simplified approach. Finally, the stress state is converged with respect to mesh refinements.

For the sake of comparison, we have simplified the refined SND DEMO engineering design to the level of our ADC configurations. With this in mind, our structural calculations, show stresses against cooldown (from ambient temperature to 4 K) and EM forces several tens of percent above threshold at the connection between inner and outer limb of the lower part of the TF coil (see Fig.3). While this number is given to compare with our current ADCs designs, these stresses are likely to be significantly reduced by more detailed engineering, and thus are not cause for concern.

In addition to the integrity of the structures surrounding the plasma, we have also examined the response of the equilibrium to perturbations representing unwanted, but sometimes

unavoidable, changes in pressure or current profiles. In particular, we have assumed fluctuations during the flat top phase that change by roughly 10% the plasma induction, l_i , and in the ratio between kinetic and poloidal magnetic pressure, β_p . In our baseline case, $I_p = 19MA$, $l_i = 0.8$ and $\beta_p = 1.14$. In addition, the growth rate of the vertical instability was assessed at flat top and at the start of ramp down, when conditions are more challenging due to the fact that the current is peaked and β_{pol} is low. The SND configuration, which has already been optimized, does not cause concerns, as the growth rates are $\gamma_{FT} \approx 2.3s^{-1}$, $\gamma_{SRD} \approx 6.3s^{-1}$ and the vertical displacement once the plasma equilibrium is perturbed induce a vertical displacement of around 2cm, well within safety limits. Another important parameter to assess is the capability of the system to recover from a vertical displacement event of a certain magnitude in terms of the power required by the stabilizing coils. A 5cm displacement in SND can be stabilized with only ex-vessel coils with less than 350MW in all the regimes considered.

Finally, all configurations have been analysed to assess their accessibility for remote maintenance and component installation. The SND has been extensively analysed in this respect and information on its challenges and solutions can be found in [1].

III. SNOWFLAKE DIVERTOR

The potential advantages of the SFD configuration are threefold, one is to distribute the power and particle fluxes on multiple legs, the second is to provide an increase of the connection length at its hexapole null and the third is to allow a stable radiation region between the two nulls and hence outside the main plasma.

Obtaining SOLPS results for this configuration is challenging, as only recently the code has acquired the capability to perform SFD simulations [13]. The magnetic equilibrium we examined is a SFD- (secondary X-point in the low field side SOL) with a gap between the separatrices at the midplane of 1mm. Unfortunately, the simulations converged only in a region of the parameter space with low Ar and D levels and are hence not shown (one order of magnitude lower than the SND). Comparing the data with the SND, it is thus no surprise that one of the divertor legs (the outermost) is still in attached regime and is exposed to very large heat fluxes and target temperatures. Due to these technical difficulties, it is therefore not yet possible to reliably assess the potential benefits of this configuration.

On the other hand, some conceptual progress was achieved on the basic mechanisms underlying the physics of the SFD. In particular, 3D turbulent simulations were performed with the GBS code [14], albeit for analytic equilibria and plasma parameters much more forgiving than DEMO's. What was observed was that a convective cell forms in the proximity of the X-point, which contributes to redistribute the plasma among the four strike points. The mechanism associated with the convective cell is novel and does not appear to be the electromagnetic churning mode described in [16], as the simulations discussed here are electrostatic. More details on these simulations and their results can be found in [14] and some connected investigation in SND geometry in [15].

In terms of the structural calculations of the TF coils, we have identified two issues where inner and outer segments meet and at the connection between the intercoil structures and the casing just below the equatorial port. In both cases, the stresses exceed one of the thresholds, but these conditions were less severe than for the SND, with the equatorial port failing only by a couple of percent, see Fig.3. These peaks appear at sharp corners, which could be smoothed with fillets in more refined designs, and thus only cause moderate concern.

On the other hand, the current design is probably underestimating the stresses in the TF coil, since the intercoil structures used have an unacceptable poloidal extension. Indeed, a major issue for the SFD is the accessibility of the divertor region for installation and remote handling operations. A remote maintenance assessment carried out *a posteriori* showed that the calculations presented here are not yet compatible with the divertor cassette removal as the intercoil structures encroach into the lower port and the inner blanket removal would not be possible. This has the unfortunate consequence that the structure's rigidity will be lowered in future designs due to the removal of the excess material. In general, a fundamental complexity and weakness of the SFD is the need to bring PF5 and PF6 close to the bottom low field side part of the TF coil while remaining sufficiently separated to efficiently generate the hexapole null (here we count PF coils clockwise starting from the top). This creates problems of space for the lower port and therefore of accessibility of the divertor.

Another worrying and intrinsic feature of the SFD is its susceptibility to perturbations. While its vertical stability is acceptable, with $\gamma_{FT} \approx 1.73s^{-1}$ and $\gamma_{SRD} \approx 5.36s^{-1}$, the position of its magnetic axis shows displacements of up to 30cm when l_i or β_{pol} are changed. Furthermore, it is concerning that the shape variations of the separatrix bring the plasma

closer to the wall and that the strike point positions have large excursions that could take them outside of the armoured region. Power requirements for the ex-vessel control system appear to be unmanageable in our current designs, with more than 100MW required to stabilize a 5cm vertical displacement during the flattop and above 1GW in the ramp down phase.

IV. X-DIVERTOR

The X-divertor is associated with a large poloidal flux expansion in the vicinity of the target and a consequent increase of connection length and particle residence time in the divertor. Also, the fanning of the flux surfaces close to the plate is considered to be useful to stabilize the motion of the detachment front towards the X-point.

We find that this configuration has indeed beneficial effects in terms of allowing a much wider operational space than the SND in terms of seeding and fuelling levels (see Fig.2). It is interesting to observe that, differently from the SND, the XD enters the acceptable operating space by increasing the deuterium flux, which seems to be sufficient to induce detached conditions. The role of the Ar impurities is to keep the separatrix density low by absorbing the power that would otherwise go into deuterium ionization and by doing that providing additional radiation.

The preliminary structural calculations for this configuration, however, were performed considering a minimal poloidal extension for outer intercoil structures. The results suggest that a significant redesign is needed, as at the moment they show several difficulties. As shown in Fig.3, stresses in the outer limb of the TF coils exceed thresholds systematically, and can sometimes be significantly above acceptable limits. This is largely due to the fact that port size was maximised in this configuration, leading to relatively short intercoil structures and a lack of support and rigidity (see also Section VI). While the equatorial and lower port could be reduced to increase the strength of this design, the upper port cannot be further shrunk because it already presents challenges in terms of safe extraction of the inner blanket structures, which would require complex kinematics. In addition to the fact that the upper port should not be enlarged to avoid weakening of the structure, there is no physical space due to the proximity of PF1 and PF2, so that blanket handling is difficult. These, however, seem to be issues connected with the current design rather than intrinsic

to the XD configuration.

Finally, in terms of controllability, the XD shows growth rates comparable to the SND's ($\gamma_{FT} \approx 1.66s^{-1}$, $\gamma_{SRD} \approx 6.73s^{-1}$) but larger vertical displacement in the case of equilibrium modifications (between 10cm and 15cm for our usual variations of l_i and β_{pol}). The power required for the vertical stabilization is roughly twice as large than for the SND, thus implying that the start of ramp down phase cannot be handled even for a 5cm shift. Similarly to the SFD, the strike points of the XD display a significant sweeping during variations of the equilibrium (25cm for the inner leg and 40cm for the outer), although they remain on the target plate, thus implying acceptable conditions. The shape of the plasma under perturbations remains significant and larger than the SND's, although less concerning than the SFD and potentially possible to handle.

V. SUPER-X DIVERTOR

The final configuration we discuss is the Super-X divertor, which has a longer outer divertor leg to maximize the toroidal flux expansion (basically, it increases the wetted area by depositing the power on an annulus of larger major radius), increase the connection length, improve neutral trapping and provide passive stabilization of the detachment front as the latter has to move against the magnetic field gradient [17].

According to the multifluid simulations, similarly to the XD, the SXD has a wider operating space than the SND and detaches thanks to an increase in fuelling levels, see Fig.2. Most importantly, the SXD has an operating window even with 300MW crossing the separatrix, corresponding to zero line radiation in the core. This means for a well designed operating point, reattachment should not occur even during the largest power fluctuations that can be achieved in the device. Preliminary analysis, discussed in a companion paper [10], suggest that this might be due to the fact that, at the higher power, Ar supplements the required additional radiation as it becomes more efficient at dissipating energy at higher SOL temperatures. The SND cannot achieve that because its operating space at 150MW already relies on Ar radiation. Although simulations are not mature enough for the XD configuration, we suspect that a mechanism similar to the SXD's might be at play also in that case.

Finally, it is worth remarking that concerns were raised in the past with respect to the

asymmetry between in/out power fluxes in the SXD divertor. This is due to simple extended two-point estimates of the power redistribution based on the connection length. The power flows preferentially through the shortest path, leading to a higher load at the outer target in the SND and more balanced load in the SXD (and XD) when the in/out connection lengths are comparable. However, the wetted area at the high field side is smaller, and the energy fluxes are therefore higher, even becoming problematic if the outer connection length becomes excessive. On the other hand, these estimates are based on simplified models that do not include radiation physics and detachment. We find that *both* inner and outer target have acceptable loads and temperatures and the asymmetry is reduced in the SXD and XD in the operating space where the divertor is detached, and hence this does not raise concerns[10]. This is compatible with ITER's results at high divertor neutral pressure [3].

We also find that the SXD configuration generates a different pattern of turbulence with respect to the SND. In particular, simulations at a reduced scale show significant turbulent activity in the outer divertor leg, potentially able to increase the perpendicular transport in the divertor region. Also, core filaments shear before reaching the target, thus effectively disconnecting the regions above and below the X-point. While more analysis is required, and especially on the extrapolation to larger devices, these are potentially beneficial effects as far as load spreading is concerned.

While the physics of this configuration seems attractive, it comes with an engineering cost. In particular, the need to extend the outer divertor leg to major radii poses a challenge to coil design, as it implies a significant deviation from the TF D-shape (if one wants to use space efficiently and keep cost contained). Regions of sharp curvature in the lower part of the TF coil are problematic, with stresses just exceeding the threshold by a few percent. In the upper part of the coil, where the inner and outer limb connect, stresses are above the allowed value, but comparable to those found in the SND, see Fig.3. As this is a preliminary design, we expect that more sophisticated engineering of the TF coil could improve the situation, although care must be taken on the intrinsic difficulties associated with the SXD. In terms of remote maintenance, all ports provide adequate access to both the blankets and the divertor, as long as the divertor cassettes are properly shaped. As a matter of fact, the upper port could be slightly reduced on its high field side to reduce the structural issues discussed above with consequences that can probably be handled on blanket handling extraction.

In terms of plasma control, even in this case vertical stability is comparable to the SND as far as growth rates are concerned ($\gamma_{FT} \approx 2.11s^{-1}$, $\gamma_{SRD} \approx 7.3s^{-1}$). On the other hand the SXD displays shape changes under variations of the equilibrium which are particularly concerning as they might lead to enhanced interactions with the upper wall. Indeed, while the displacement of the magnetic axis is comparable to the XD, the top of the plasma can shift up to 25cm upwards. Inner and outer strike points can move up to 40cm along the targets, but the particular design of the SXD implies that they remain on armoured structures. Power requirements for the ex-vessel vertical control system appear very demanding in the ramp down phase.

VI. DISCUSSION

The comparative analysis of the different configurations allows a deeper understanding of the problem of divertor optimization. On the physics, one of the conclusions is that increasing the outer connection length does show an increase in asymmetries, but they become completely irrelevant when the divertor detaches, since both targets remain within acceptable constraints. On the other hand, the outer divertor leg should not be too long and the ratio of the in/out connection length should not be much larger than one to ensure safe power handling in the inner leg and accessible operating spaces (all our configurations satisfy this criterion). Crucially, we found at least one configuration (SXD) that can allow operations without imposing performance reducing radiation from the core, and we suspect that a second one might lead to similar results. With the caveat that more sophisticated models will have to confirm these results, this means that even in the event of large power transients, the divertor should be able to cope with the additional power flux. In general, it is interesting to see that Ar seeding is less crucial for the ADCs than for the SND, as this could give some extra margin to access higher power conditions. However, Ar injection is efficient at reducing the separatrix density and thus potentially improve performance (this was observed also in ITER simulations [3]). Of course, our multifluid results must be taken with caution as kinetic simulations should confirm these benefits, although we believe the trends identified can provide valuable information, especially in the high fuelling phase of interest (e.g. ITER's simulations were kinetic but show trends similar to ours).

The engineering studies carried out showed that designing ADCs requires a delicate bal-

ance between ports and intercoil structures. The latter have to be sufficiently resistant to provide rigidity against out of plane forces and extended to ensure passive stabilization against vertical displacement events. On the other hand, ports have to allow for efficient removal of blanket modules and divertor cassettes, and, in the case of the lower port, give a clear path for pumping purposes. Alternative configurations require PF coils in certain positions to maximize their benefits and this poses additional constraints on the overall design. The bottom part of the machine is the most affected by this issue, although some effects can be seen also in other areas (e.g. the SXD problem near PF1). While certain difficulties can be designed out in more elaborated engineering studies (such as those already carried out for the SND), others are intrinsic to the ADCs and these are the ones that should receive more attention going forward (e.g. the PF coil positioning in the XD and SFD and the TF coil shape for the SXD). Finally, control poses a serious concern, especially for the sensitivity of the plasma shape to current profile variations. In particular, secondary X-points are very susceptible to this and have large excursions in all ADCs, which can be problematic for the configurations that are based on this concept (especially the SFD since its secondary null is in the plasma). The possibility to improve the stability performance of the configurations with appropriate reshaping and with the addition of an in-vessel vertical stabilization system is under analysis.

VII. CONCLUSIONS AND PERSPECTIVES

The overall analysis of the ADCs presented in this paper has shown a truth that we already suspected: their physics is appealing but their engineering is difficult. However, in many cases we can now identify where improvements are likely, possible or difficult. In particular, it is clear that the challenge of the ADCs is the integration of often conflicting requirements. In this respect, this work would be incomplete without a recommendation on how to optimize an ADC for DEMO.

Based on the physics results obtained, it is clear that large flux expansion (poloidal and toroidal) and longer outer connection lengths should be sought (especially the latter seemed relevant for our SXD configuration). Extreme solutions, however, clash with engineering constraints, in particular the controllability, the PF coil positioning and the level of stresses in TF coils that diverge from the D-shape. We hence think that a divertor with comparable

in/out connection length, outer strike point radius and target poloidal flux expansion as large as possible and good closure (potentially just given by the size of the machine) could capture the physics benefits of both the SXD and XD. The hope is that it would inherit their capability to operate with Ar margin so that low core radiation can be sustained, at low separatrix density and good impurity segregation. The requirement to have small impinging angles, but still above a certain threshold (1.5-2 degrees), implies that, to maximize flux expansion, the outer divertor leg must form a 90 degree angle with the divertor plate in the poloidal plane. In addition, its poloidal length should be shorter than the one we have analysed here, so that less extreme TF coil designs could be considered and the PF coils could remain closer to the plasma and improve control. In order to strengthen the coil cage, especially to out of plane deformations, we also suggest to implement box intercoil structures, as considered in the current I-DTT design. These consist of structures with larger effective poloidal cross section but hollow in the center to keep them light.

Future work should develop the new configuration described above, but also include more refined multifluid and turbulent simulations, including kinetic neutral physics and an assessment of the poloidal variations of the diffusion coefficients. Also, neutronics studies will assess the amount of irradiation of the components as well as determine (comparatively) tritium breeding capabilities. Pumping studies have also been carried out and will be improved to ensure that fuel, ashes and impurities can be efficiently removed.

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