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Article

Configurational Entropy in Multicomponent Alloys: Matrix formulation from *ab initio* based Hamiltonian and application to FCC Cr-Fe-Mn-Ni system

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Abstract: Configuration entropy is believed to stabilize disordered solid solution phases in multicomponent systems at elevated temperatures over intermetallic compounds by lowering the Gibbs free energy. Traditionally the increment of configuration entropy with temperature was computed by time consuming thermodynamic integration methods. In this work, a new formalism is developed to predict configuration entropy as function of temperature from multi-body cluster probability in a system with arbitrary number of components, K and arbitrary average composition. The formalism uses the principles behind the Cluster Variation Method (CVM) but extends the treatment to arbitrary cluster interaction employed in the Cluster Expansion (CE) technique. The multi-body probabilities are worked out by explicit inversion and direct product of a matrix formulation from point functions in the clusters obtained from symmetry independent correlation functions. The matrix quantities are determined from semi canonical Monte Carlo simulations with Effective Cluster Interactions (ECIs) derived from Density Functional Theory (DFT) calculations. The formalism is applied to analyze the four-body cluster probabilities for the quaternary system Cr-Fe-Mn-Ni. It is shown that for two specific compositions ($\text{Cr}_{25}\text{Fe}_{25}\text{Mn}_{25}\text{Ni}_{25}$ and $\text{Cr}_{18}\text{Fe}_{27}\text{Mn}_{27}\text{Ni}_{28}$) the high value of probabilities of Cr-Fe-Fe-Fe and Mn-Mn-Ni-Ni are strongly correlated with the presence of the ordering phases $\text{L}_{12}\text{-CrFe}_3$ and $\text{L}_{10}\text{-MnNi}$ respectively and that are also in excellent agreement with *ab initio* predictions of these ground state structures. The general formalism is used to investigate configuration entropy as a function of temperature and for 285 different alloy compositions. It is found that our matrix formulation of configuration entropy is in agreement with the result obtained by the thermodynamic integration method. At the high temperature limit, our theoretical prediction for configuration entropy agrees well with random configuration entropy for all compositions of the alloy.

Keywords: Multicomponent; *Ab initio*; Configuration entropy; Matrix Formulation; Cluster Expansion; Cluster Variation Method; Monte Carlo ; Thermodynamic integration

1. Introduction

Multicomponent systems, termed as High Entropy Alloys (HEAs), are crystalline solids that form predominantly in single phase. These systems were brought to wider attention through the work of Cantor et al [1] and Yeh et al [2]. At or near equiatomic ratio of compositions the configuration

29 entropy is maximized and given by the formula $S_{config}/R = \ln K$ where R the ideal gas constant, and
30 K the total number of different components. It has been proposed to define $K = 4$ as the minimum
31 number of components at or near equiatomic composition for these systems to be called HEAs [3–5].

32 There are various sources of entropy in a system in addition to configuration entropy including
33 vibration, electronic and magnetic contributions. The co-existence of multiple phases in the
34 equilibrium state of a chemical system with a given overall composition at a specified temperature
35 is found by minimizing the Gibbs free energy of the whole system. When the system undergoes
36 a phase transition of either order-disorder or spinodal decomposition the relative differences of
37 configurational entropy are dominant in comparison to those contributions from vibration and
38 magnetic terms in FeCoCrNi [6] where the relative difference of configuration entropy dominates
39 or is of similar magnitude to vibration entropy. These multicomponent alloys have transition metals
40 Co, Cr, Fe, and Ni that exhibit magnetic behavior and have magnetic phase transitions characterized
41 by Curie temperatures sensitive to concentrations [7].

42 In general, the formulation of configuration entropy given by the expression $S_{config}/R =$
43 $\ln K$ only holds for disordered alloys with equiatomic composition at temperatures near their
44 melting point. On the other hand at low temperature the lowest free energy structures can be
45 ordered intermetallic phases or partially ordered structures. In the intermediate temperature range
46 there exists short range order, which is related to the nature of the chemical environment of
47 each atomic species containing ordering or segregation preferences specially at low temperatures,
48 because random disordering is favored at the high temperatures. The importance of short-range
49 order was manifested in diffuse X-ray scattering measurements of alloys contained ordered
50 superstructure domains that were seen to significantly affect electrical resistivity properties [8,9],
51 and also influence on the strengthening by hindering dislocation motion [10] in concentrated
52 alloys. Recently, it has been demonstrated how short-range order can be predicted from ab
53 initio based Hamiltonians in combination with Monte Carlo simulations [11] in multicomponent
54 Mo-Nb-Ta-V-W system. The study predicted that strong SRO parameter may lead to the formation
55 of Mo-Ta ordering in the B2 structure after quenching down from temperatures as high as 3,000K.
56 HEAs such as $Al_{1.3}CoCrCuFeNi$ have been reported to be susceptible to complex phase transitions
57 including segregation, precipitation, chemical ordering and spinodal decomposition into a complex
58 microstructure containing regions of BCC, FCC and B2 phases [12]. Physical models have been
59 successfully applied to predict the formation of these phases on the basis of the average number
60 of valence electrons [13].

61 The prediction of equilibrium thermodynamic properties (free energies, and phase diagrams) is
62 one of the goals of computational materials science. Lattice statistical models involving an Ising-like
63 Hamiltonian developed from ab initio enthalpies of mixing have become an important tool in the
64 computation of the thermodynamic properties of alloy systems. In particular, the cluster expansion
65 (CE) method [14] expands the Hamiltonian into contributions from an optimized set of clusters, each
66 term weighted by Effective Cluster Interactions (ECI). The thermodynamic properties at temperature
67 are obtained from the ECI by computing the free energies from either Monte Carlo methods or the
68 Cluster Variation Method (CVM).

69 The CVM expresses the free energy in terms of enthalpies of mixing and configuration entropies
70 as a functional of the temperature dependent correlation functions; the free energy value is found
71 at any given temperature by minimizing the free energy from variational principles. The correlation
72 function parameters in terms of which configuration entropy and enthalpy of mixing are expressed
73 grow exponentially with component number K and size of the maximal cluster ω . Due to this, the
74 CVM has been commonly applied to clusters consisting of four sites in a regular tetrahedron or the
75 so-called tetrahedron-octahedron in the FCC lattice [15,16], or the four sites in an irregular tetrahedron
76 in the BCC lattice [17]. It is generally accepted that the Monte Carlo method is more accurate, but
77 the calculations are time consuming due to the need of many passes to obtain free energies at any
78 given temperature from the disordered high temperature configuration. A hybrid approach taking

79 the Monte Carlo calculated correlation functions at temperature and computing the configuration
 80 entropy value from analytic CVM expression has been used to improve the accuracy of the CVM to
 81 that of time-consuming thermodynamic integration. This method has been applied to FCC systems
 82 in the 13 sites cluster, which consist of a lattice point and its twelve first nearest neighbors, and the 14
 83 sites cluster approximation [18]. However, the analytic expressions for the configuration entropy
 84 reported in the literature do not often match those clusters used for the CVM. In this work we
 85 close this gap by providing a methodology to develop analytic expressions for configuration entropy
 86 matching the clusters from the CE Hamiltonian. We apply our method to CrFeMnNi HEA to arbitrary
 87 alloy composition. In particular, the composition $\text{Cr}_{18}\text{Fe}_{27}\text{Mn}_{27}\text{Ni}_{28}$ has been used recently to design
 88 radiation tolerant materials for advanced nuclear reactor systems. This HEA has been studied for
 89 advanced nuclear applications in preference to Cantor's alloy [1] due to the removal of Co, which can
 90 cause activation by transmutation of ^{60}Co isotope in nuclear reactors [19].

91 This paper is organized as follows: In the section 2, a new matrix formulation within the cluster
 92 expansion method is introduced that links cluster correlation functions obtained from Monte Carlo
 93 calculations to multi-body probabilities. Notation is developed to treat as general as possible arbitrary
 94 cluster sizes, ω , number of components, K , and temperature. In section 3, our general method
 95 is illustrated to calculate four-body cluster probabilities as a function of temperature for the two
 96 specific compositions of equiatomic $\text{Cr}_{25}\text{Fe}_{25}\text{Mn}_{25}\text{Ni}_{25}$ and also the composition $\text{Cr}_{18}\text{Fe}_{27}\text{Mn}_{27}\text{Ni}_{28}$
 97 from [19]. In section 4, the general expression for configuration entropy is discussed for an arbitrary
 98 alloy composition at two temperatures 1000 and 3000 K. The changes in configuration entropy are
 99 attributed to the lowering of the probabilities of the phases that are most stable at low temperatures
 100 and the complementary tendency towards disordered random solution of the alloy at the average
 101 composition given. The main conclusions of this work are given in section 5.

102 2. Methods

103 2.1. Matrix formulation of cluster expansion

104 Let us consider an alloy system with arbitrary number, K , of components and crystalline lattice
 105 symmetry, in which the disordered phase is described by space group, G . The CE Hamiltonian at $T =$
 106 0 K of the alloy can be found from enthalpies of mixing, $\Delta H_{DFT}^{Mixing}[\vec{\sigma}]$, of derivative alloy structures
 107 [14,20] denoted by varying length arrays of spin-like variables $\vec{\sigma}_i$ taking values from 0 to $K - 1$. In
 108 general a derivative structure of the alloy has non-zero atomic concentrations for each of $p = 1, \dots, K$
 109 different chemical elements forming it i.e. $x[\vec{\sigma}]_p \neq 0$. For each member structures the reference
 110 energy in the calculation of the enthalpy of mixing is the pure element total energy, $E_{total}[p]$, in the
 111 same crystallographic symmetry. The alloy enthalpy of mixing is defined as follows:

$$\Delta H_{DFT}^{Mixing}[\vec{\sigma} \equiv \{\sigma_1, \sigma_2, \dots\}] = E_{total}[\vec{\sigma} \equiv \{\sigma_1, \sigma_2, \dots\}] - \sum_{p=1, \dots, K} x_p[\vec{\sigma} \equiv \{\sigma_1, \sigma_2, \dots\}] E_{total}[p] \quad (1)$$

112 The enthalpies of mixing are calculated from the total energies $E_{total}[\vec{\sigma}]$ and $E_{total}[p]$ of alloy and
 113 pure element, respectively, by density functional theory (DFT) for the underlying lattice. In the CE
 114 the $\Delta H_{DFT}^{mixing}[\vec{\sigma}]$ of an arbitrary structure $\vec{\sigma}$ is expanded into a sum of reference clusters, $\Delta H_{CE}^{Mixing}[\vec{\sigma}]$.

$$\Delta H_{CE}^{Mixing}[\vec{\sigma} \equiv \{\sigma_1, \sigma_2, \dots\}] = \sum_{\omega, n, (s)} m_{\omega, n}^{(s)} I_{\omega, n}^{(s)} \langle \Gamma_{\omega', n'}^{(s')}[\vec{\sigma} \equiv \{\sigma_1, \sigma_2, \dots\}] \rangle_{\omega, n, (s)} \quad (2)$$

115 In Eq. 2 each reference cluster is characterized by three labels ω, n and (s) . The label ω denotes
 116 the total number sites; n is an auxiliary label that refers to highest order coordination shell contained
 117 in the reference cluster and finally the label $(s) = (j_1, j_2, \dots, j_\omega)$, denotes decoration of cluster by
 118 point functions with dimension equal to ω and j_i taking values $0, \dots, K - 1$. For each reference cluster,

119 an effective cluster interaction (ECI) $J_{\omega,n}^{(s)}$ and the multiplicity per lattice site, $m_{\omega,n}^{(s)}$ are associated.
 120 The term $\langle \Gamma_{\omega',n'}^{(s')}[\vec{\sigma}] \rangle_{\omega,n,(s)}$ used in the definition of enthalpy of mixing in Eq. 2 is the thermally
 121 averaged cluster correlation function over all clusters $\omega', n', (s')$ which are equivalent to a space group
 122 symmetry element of the disordered phase within the reference decorated cluster defined by $\omega, n, (s)$.
 123 Overall the triple product of multiplicity, ECI and correlation function, $m_{\omega,n}^{(s)} J_{\omega,n}^{(s)} \langle \Gamma_{\omega',n'}^{(s')}[\vec{\sigma}] \rangle_{\omega,n,(s)}$ gives
 124 the energetic contribution per lattice site of the reference cluster ω, n and (s) to the enthalpy of mixing
 125 of the particular structure configuration given by $\vec{\sigma}$.

126 The correlation function is defined as the product of point functions evaluated over the system,
 127 and its average is given by the following formula:

$$\begin{aligned} \langle \Gamma_{\omega',n'}^{(s')}[\vec{\sigma}] \rangle_{\omega,n,(s)} &= \langle \gamma_{j_1,K}[\sigma_1] \gamma_{j_2,K}[\sigma_2] \cdots \gamma_{j_{\omega},K}[\sigma_{\omega}] \rangle \\ &= \frac{1}{\Omega[\omega,n]} \sum_{u=1}^{\Omega[\omega,n]} \gamma_{j_1,K}[\sigma_{\overrightarrow{(\omega,n)}_{u_1}}] \gamma_{j_2,K}[\sigma_{\overrightarrow{(\omega,n)}_{u_2}}] \cdots \gamma_{j_{\omega},K}[\sigma_{\overrightarrow{(\omega,n)}_{u_{\omega}}}] \end{aligned} \quad (3)$$

128 where the point function can be determined following [14] as:

$$\gamma_{j,K}[\sigma_i] = \begin{cases} 1 & \text{if } j = 0, \\ -\cos\left(2\pi\left[\frac{j}{2}\right]\frac{\sigma_i}{K}\right) & \text{if } j > 0 \text{ and odd,} \\ -\sin\left(2\pi\left[\frac{j}{2}\right]\frac{\sigma_i}{K}\right) & \text{if } j > 0 \text{ and even,} \end{cases} \quad (4)$$

129 In Eq. 3 the correlation function of the system is averaged over the arbitrary crystal structure of
 130 the alloy system with configuration $\vec{\sigma}$ over all the set of $\Omega[\omega,n]$ clusters, $\{\overrightarrow{(\omega,n)}_u\}_{u=1,2,\dots,\Omega[\omega,n]}$ where
 131 each cluster labeled by u contains ω sites, each site denoted by the vector, $\overrightarrow{(\omega,n)}_{u_i}$. The i -union of
 132 the ω vectors, $\overrightarrow{(\omega,n)}_{u_i}$, composes the cluster of vectors, $(\overrightarrow{(\omega,n)}_{u_1}, \overrightarrow{(\omega,n)}_{u_2}, \cdots, \overrightarrow{(\omega,n)}_{u_{\omega}}) \equiv \overrightarrow{(\omega,n)}_u$.
 133 The $u_1, u_2, \cdots, u_{\omega}$ are numeric labels referring to the values taken by variable u in Eq. 3 that serve
 134 to enumerate the vectors making up the u cluster of vectors $\{\overrightarrow{(\omega,n)}_u\}$. The clusters $\overrightarrow{(\omega,n)}_u$ are
 135 symmetrically equivalent to the reference cluster (ω,n) sites by a symmetry operation and that are
 136 enumerated by an index taking values $1, 2, \cdots, \Omega[\omega,n]$. $\Omega[\omega,n]$ is defined as the number of times the
 137 reference cluster (ω,n) is contained in a structural configuration which can be obtained from Monte
 138 Carlo simulation. The sites in the cluster $\{\overrightarrow{(\omega,n)}_u\}$ can allocate all of the possible decoration values
 139 $\in (s)$ which we express as $(s) = (j_1, j_2, \cdots, j_{\omega})$. These integer indexes corresponding to the decorated
 140 cluster are parameters for the point functions in Eq. 4.

141 For an arbitrary ω -sites cluster and K components, the number of ω -tuples formed with integer
 142 entries running from $0 \cdots K-1$ can be calculated. For $\omega = 2$, the formula calculates the number
 143 of symmetrically unique decorations (s) for a two-point cluster $\langle \Gamma_{\omega',n'}^{(s')}[\vec{\sigma}] \rangle_{\omega=2,n,(s)}$ and K component
 144 alloy system reduces to $(K+1)K/2$ [11], where K is the number of components. For higher order
 145 cluster, the total number of decorations depend on the cluster coordinates and the space group
 146 symmetry G of the high temperature disordered phase i.e. FCC or BCC and can not be simply
 147 expressed in terms of K (in general there could be less than $\binom{\omega+K-1}{K-1} = \frac{(\omega+K-1)!}{(K-1)!(\omega)!}$ number of
 148 symmetrically unique correlation functions). ATAT [14] numerically works out all the number of
 149 symmetrically unique decorated clusters $\omega', n', (s')$ equivalent to $\omega, n, (s)$ and uses one correlation
 150 function per set of equivalent decorated clusters $\langle \Gamma_{\omega',n'}^{(s')}[\vec{\sigma}] \rangle_{\omega,n,(s)}$. For convenience in notation, from
 151 now on we will use $\langle \Gamma_{\omega,n}^{(s)}[\vec{\sigma}] \rangle = \langle \Gamma_{\omega',n'}^{(s')}[\vec{\sigma}] \rangle_{\omega,n,(s)}$. In general, two decorations (s) and (s') are
 152 symmetrically equivalent if there is at least one element in the space group symmetry $g \in G$ that

153 transforms the sites $\{\vec{\tau}_1, \vec{\tau}_2, \dots, \vec{\tau}_\omega\} \subset (\omega, n)$ into $\{\vec{\tau}_{g[1]}, \vec{\tau}_{g[2]}, \dots, \vec{\tau}_{g[\omega]}\} \subset (\omega, n)$ as the permutation
 154 connecting the decorations $(s) = (1, 2, \dots, \omega) \subset \{(s)_{(\omega, n)}\}$ and $(s') = (g[1], g[2], \dots, g[\omega]) \subset$
 155 $\{(s)_{(\omega, n)}\}$. This is given by following equation:

$$g\{\vec{\tau}_1, \vec{\tau}_2, \dots, \vec{\tau}_\omega\} = \{\vec{\tau}_{g[1]}, \vec{\tau}_{g[2]}, \dots, \vec{\tau}_{g[\omega]}\} \quad (5)$$

156 With the symmetry relations between decorations (s) and (s') in any given cluster, we are
 157 able to retrieve all K^ω possible ω tuples from the set of unique symmetries corresponding to an ω
 158 cluster in ATAT [14]. The point functions $\gamma_{j,K}[\sigma_i]$ used to define the general correlation functions are
 159 related to the multi-body cluster probabilities (see below in Eq. 9) by direct products of a linear [21]
 160 transformation τ_K

$$(\tau_K)_{ji} \equiv \gamma_{j,K}[\sigma_i] \quad (6)$$

161 where the new matrix τ is constructed from these point functions, $\gamma_{j,K}[\sigma_i]$. It can be trivially
 162 shown that the inverse of Van der Monde matrices with complex entries equal to roots of unity, is
 163 its complex conjugate one. The inverse of the τ_K matrix can be obtained from the complex conjugate
 164 matrix of τ_K by taking the real and imaginary part and riffing their rows. Fom Eq. 4, the following
 165 expression results for a system with K components:

$$(\tau_K^{-1})_{ij} = \begin{cases} \frac{1}{K} & \text{if } j = 0, \\ -\frac{2}{K} \cos\left(2\pi\left[\frac{j}{2}\right]\frac{\sigma_i}{K}\right) & \text{if } j > 0 \text{ and } j-1 < K \text{ and } j \text{ odd,} \\ -\frac{2}{K} \sin\left(2\pi\left[\frac{j}{2}\right]\frac{\sigma_i}{K}\right) & \text{if } j > 0 \text{ and } j \text{ even,} \\ -\frac{1}{K} \cos\left(2\pi\left[\frac{j}{2}\right]\frac{\sigma_i}{K}\right) & \text{if } j-1 = K \text{ and } j \text{ odd,} \end{cases} \quad (7)$$

166 The size of τ_K matrix is $K \times K$, where K is the number of components. It is convenient to perform
 167 the matrix multiplications with all K^ω decorations formed from ω -tuples with integer elements
 168 running from 0 to $K-1$. In particular for the case of four component $K = 4$ these matrices τ become by
 169 applying Eqs. 4 and 7 for the inverse τ_K^{-1} :

$$\tau_4 = \begin{pmatrix} 1 & 1 & 1 & 1 \\ -1 & 0 & 1 & 0 \\ 0 & -1 & 0 & 1 \\ -1 & 1 & -1 & 1 \end{pmatrix} \quad \tau_4^{-1} = \frac{1}{4} \begin{pmatrix} 1 & -2 & 0 & -1 \\ 1 & 0 & -2 & 1 \\ 1 & 2 & 0 & -1 \\ 1 & 0 & 2 & 1 \end{pmatrix} \quad (8)$$

170 We duplicate the symmetrically unique decorations (s) whenever two decorations are connected
 171 by symmetry of the disordered structure. For relating two equivalent decorations we find it
 172 convenient to use a permutation representation of the space group operator as permutations of ω -site
 173 tuples. We use the property of invariance of the cluster expansion to obtain probability distributions
 174 from correlation functions [22]. As a consequence of the compact formalism and by using Eqs. 4 and
 175 7, the expression of correlation functions can be rewritten into a matrix form:

$$\langle \Gamma_{\omega, n}^{(ij \dots)}[\vec{\sigma}] \rangle = \sum_{\forall [(pq \dots)]}^{K^\omega} \gamma_{i,K}[\vec{\sigma}_p] \gamma_{j,K}[\vec{\sigma}_q] \dots y_{\omega, n}^{(pq \dots)}[\vec{\sigma}] \equiv \overbrace{(\tau_K \otimes \dots \otimes \tau_K)}^\omega_{ij \dots, pq \dots} y_{\omega, n}^{(pq \dots)}[\vec{\sigma}] \quad (9)$$

176 With the aid of the matrix formulation from Eq. 9 and the generalized form of the inverse matrix
 177 τ_K^{-1} in Eq. 7, one can express the ω -cluster probabilities into a matrix form:

$$y_{\omega, n}^{(pq \dots)}[\vec{\sigma}] = \overbrace{(\tau_K^{-1} \otimes \dots \otimes \tau_K^{-1})}^\omega_{pq \dots, ij \dots} \langle \Gamma_{\omega, n}^{(ij \dots)}[\vec{\sigma}] \rangle \quad (10)$$

178 where we have used of the notation for direct product of matrices $\overbrace{(\tau_K^{-1} \otimes \dots \otimes \tau_K^{-1})}^{\omega}_{pq\dots,ij\dots} =$
 179 $(\tau_K)_{p,i}(\tau_K)_{q,j} \dots$. And we also implied summation over repeated indexes on the right hand side of
 180 Eq. 10. Note that the size of these matrices increases exponentially with cluster size ω , $K^\omega \times K^\omega$; in
 181 particular for $\omega = 4$ the matrices have 256x256 entries. The cluster probabilities are normalized as
 182 expressed in Eq. 11

$$\sum_{\forall[(pq\dots)]}^{K^\omega} y_{\omega,n}^{(pq\dots)}[\vec{\sigma}] = 1 \quad (11)$$

183 As a consequence of the normalization of the cluster probabilities, it is possible to separate
 184 probabilities of the decorated sub-clusters from the probabilities of the maximal cluster by partial
 185 summations over all possible decorations for the sites that belong to the maximal cluster ω, n but not
 186 the i -th sub-cluster ω_i, n_i .

$$\sum_{(pq\dots) \in \{[(pq\dots)_{\omega_i, n_i}]\}} y_{\omega_i, n_i}^{(pq\dots)}[\vec{\sigma}] = y_{\omega, n}^{(pq\dots)}[\vec{\sigma}] \quad (12)$$

187 From Eq. 10 and for the case with $\omega=2$, it follows the generalized expression for SRO of species p
 188 and q at the n th shell, $\alpha_{2,n}^{(pq)}[\vec{\sigma}]$ ($p \neq q$), can be interpreted as the tendency to order or segregate species
 189 p and q with respect the disordered random probability given by the product of their elemental, p ,
 190 bulk concentration $x_p[\vec{\sigma}]$. For the four component Cr-Fe-Mn-Ni system, there are 6 chemically distinct
 191 SRO parameters: $\alpha_{2,n}^{(01)}[\vec{\sigma}]$ for Cr-Fe, $\alpha_{2,n}^{(02)}[\vec{\sigma}]$ for Cr-Mn, $\alpha_{2,n}^{(03)}[\vec{\sigma}]$ for Cr-Ni, $\alpha_{2,n}^{(12)}[\vec{\sigma}]$ for Fe-Mn, $\alpha_{2,n}^{(13)}[\vec{\sigma}]$
 192 for Fe-Ni, and $\alpha_{2,n}^{(23)}[\vec{\sigma}]$ for Mn-Ni. The SRO allows a quantitative description of the interactions
 193 between atoms as a function of temperature to predict order-disorder transition temperatures [11,23].
 194 In particular the matrix formalism from Eqs. 7 and 10 allows one to generalize the SRO treatment for
 195 an arbitrary number of components, K :

$$y_{2,n}^{(pq)}[\vec{\sigma}] = x_p[\vec{\sigma}]x_q[\vec{\sigma}](1 - \alpha_{2,n}^{(pq)}[\vec{\sigma}]) \quad (13)$$

196 2.2. Configuration entropy in the matrix formulation

197 In general, a thermodynamical system in state $\vec{\sigma}$ and with enthalpy of mixing given by the CE
 198 Hamiltonian $\Delta H_{CE}^{Mixing}[\vec{\sigma}]$ is described by a set of symmetry unique probability distributions $y_{\omega,n}^{(pq\dots)}[\vec{\sigma}]$
 199 characterized by decorations of a chosen maximal ω, n cluster. In practice the chosen maximal cluster
 200 ω, n contains few points (for the tetrahedron approximation, four nearest neighbour cluster within the
 201 CVM [15]). As a mean field approximation [21], the CVM can be rationalized as a factorization of the
 202 probability distributions of the ω, n maximal cluster into integer powers $\eta_{\omega_1, n_1}, \eta_{\omega_2, n_2} \dots, \eta_{\omega_s[\omega, n], n_s[\omega, n]}$
 203 of the probability distributions of the sub-clusters $(\omega_i, n_i) \subseteq (\omega, n); i = 1, \dots, [\omega, n]$ [24] with
 204 decorations $(pq\dots)_{\omega_i, n_i}$ corresponding to the components $(pq\dots)_{\omega_i, n_i}$ of all decorations $(pq\dots)$
 205 $\in \{(pq\dots)_{(\omega, n)}\}$ occupied by sites of the ω_i, n_i sub-cluster

$$y_{\omega,n}^{(pq\dots)}[\vec{\sigma}] = (y_{\omega_1, n_1}^{(pq\dots)}[\vec{\sigma}])^{\eta_{\omega_1, n_1}} (y_{\omega_2, n_2}^{(pq\dots)}[\vec{\sigma}])^{\eta_{\omega_2, n_2}} \dots (y_{\omega_{[\omega, n]}, n_{[\omega, n]}}^{(pq\dots)}[\vec{\sigma}])^{\eta_{\omega_{[\omega, n]}, n_{[\omega, n]}}} \quad (14)$$

206 The following expression, a consequence of the CVM factorization scheme, can be derived from
 207 [24] and is the reason why the disordered configuration at high temperature is reproduced from
 208 multi-body probabilities $\sum_{i=1}^{[\omega, n]} \omega_i \eta_{\omega_i, n_i} = -1$. This occurs because at the high temperature limit the
 209 CVM probabilities tend to products of composition of the species involved in the decorations of the
 210 cluster:

$$y_{\omega_i, n_i}^{(pq\cdots)_{\omega_i, n_i} [\vec{\sigma}]} \xrightarrow{T \rightarrow \infty} \prod_{j=1}^{\omega_i} y_{1,1}^{((pq\cdots)_j)_{\omega_i, n_i} [\vec{\sigma}]} = \prod_{j=1}^{\omega_i} x_{((pq\cdots)_j)_{\omega_i, n_i} [\vec{\sigma}]} \quad (15)$$

211 where $y_{1,1}^{((pq\cdots)_j)_{\omega_i, n_i} [\vec{\sigma}]} = x_{(pq\cdots)_j)_{\omega_i, n_i} [\vec{\sigma}]}$ is the concentration of the $(pq\cdots)_j$ equal to one of the
 212 integers $0, 1, \dots, K-1$ in the disordered state of the alloy. A natural consequence of the factorization
 213 scheme chosen for the CVM multi-body probabilities is that the configuration entropy assumes the
 214 formulation

$$S_{\omega, n} [\vec{\sigma}] \equiv \sum_{i=1}^{[\omega, n]} \eta_{\omega_i, n_i} \tilde{S}_{\omega_i, n_i} [\vec{\sigma}] = \sum_{i=1}^{[\omega, n]} \eta_{\omega_i, n_i} \sum_{\forall [(pq\cdots)_{\omega_i, n_i}]}^{K^{\omega_i}} k_B y_{\omega_i, n_i}^{(pq\cdots)_{\omega_i, n_i} [\vec{\sigma}]} \ln(y_{\omega_i, n_i}^{(pq\cdots)_{\omega_i, n_i} [\vec{\sigma}]}) \quad (16)$$

215 where $\tilde{S}_{\omega_i, n_i}$ is the entropy contribution to cluster (ω, n) from the sub-cluster (ω_i, n_i) :

$$\tilde{S}_{\omega_i, n_i} [\vec{\sigma}] = \sum_{\forall [(pq\cdots)_{\omega_i, n_i}]}^{K^{\omega_i}} k_B y_{\omega_i, n_i}^{(pq\cdots)_{\omega_i, n_i} [\vec{\sigma}]} \ln(y_{\omega_i, n_i}^{(pq\cdots)_{\omega_i, n_i} [\vec{\sigma}]}) \quad (17)$$

216 The set of integers $\eta_{\omega_1, n_1}, \eta_{\omega_2, n_2}, \dots, \eta_{\omega_s[\omega, n], n_s[\omega, n]}$ are the mean field integer coefficients associated
 217 with the partition function of the alloy system. In the theory of regular mixtures, the coefficients
 218 can be found from the recursive heuristic expression after Kikuchi, [25], Barker [26] and whose
 219 formulation was explicitly derived by using group theoretic methods by Gratias et al. [27]. It requires
 220 the determination of two quantities: the site multiplicity N_{ω_i, n_i} and the sub-cluster multiplicity N_{ω_i, n_i}^β .
 221 The site multiplicity can be determined by calculating the number of symmetry operators, $\mathcal{N}_{\omega_i, n_i}$,
 222 that stabilize the ω_i, n_i cluster i.e. $g \in G$ such that the application of g into the set of cluster positions
 223 $\{\vec{\tau}_1, \vec{\tau}_2, \dots, \vec{\tau}_\omega\}$ results in a permutation of the set; then $N_{\omega_i, n_i} = \frac{|G|}{|\mathcal{N}_{\omega_i, n_i}|}$ where $|G|$ is the order of
 224 the point group associated to the space group G and $|\mathcal{N}_{\omega_i, n_i}|$ is the order of the group $\mathcal{N}_{\omega_i, n_i}$. The
 225 sub-cluster multiplicity N_{ω_i, n_i}^β is just the frequency of the cluster β that is contained in the cluster
 226 ω_i, n_i

$$\eta_{\omega_i, n_i} = -N_{\omega_i, n_i} - \sum_{(\omega_i, n_i) \subset \beta \subseteq (\omega, n)} N_{\omega_i, n_i}^\beta \eta_\beta \quad (18)$$

227 In particular the formulation applied to point cluster retrieves the Bragg-Williams approximation
 228 for maximal cluster ($\omega = 1, n = 1$), i.e a site cluster, giving the entropy weight of $\eta_{\omega_1=1, n_1=1} = -1$
 229 and for a two body cluster ($\omega = 2, n$) in the n^{th} coordination shell, we get $\eta_{\omega_2, n_2} = -N_{2, n}$ and
 230 $\eta_{\omega_1, n_1} = 2N_{2, n} - 1$, where $N_{2, n}$ is site multiplicity of the cluster $(2, n)$ calculated from the sites in this
 231 cluster and the space group G .

232 This formulation is valid for the CVM method or for the hybrid CE-Monte Carlo method; in
 233 the hybrid CE-Monte Carlo technique, the free energy minimization is performed by Monte Carlo
 234 technique, and in the process, the Monte Carlo produces the correlation functions for the equilibrium
 235 configurations found at each of the temperatures investigated [28]. The hybrid approach uses these
 236 correlation functions in the analytic expressions for configuration entropy.

237 There is an alternative to the hybrid approach for the entropy calculation where the
 238 thermodynamic integration method can be used. Here entropy is calculated from the contribution
 239 to the specific heat at constant volume, C_{conf} derived from the fluctuations of enthalpy of mixing at
 240 temperature values in a fine grid of temperature values:

$$S_{conf}[T] = \int_0^T \frac{C_{conf}}{T'} dT' = \int_0^T \frac{\langle \Delta H_{CE}^{Mixing} \rangle^2 - \langle \Delta H_{CE}^{Mixing} \rangle^2}{T'^3} dT' \quad (19)$$

241 where $\langle \Delta H_{CE}^{Mixing} \rangle^2$ and $\langle \Delta H_{CE}^{Mixing^2} \rangle$ are the square of the mean and mean square enthalpies of
 242 mixing, respectively, calculated by averaging over all the MC steps at the accumulation stage for a
 243 given temperature. The accuracy of evaluation of configurational entropy depends on the size of
 244 temperature integration step and the number of MC steps performed at the accumulation stage [29].

245 2.3. Computational details

246 The DFT enthalpies of mixing given by Eq. 1 were calculated from DFT total energies performed
 247 using the projector augmented wave (PAW) method [30] implemented in VASP [31–35]. Exchange
 248 and correlation were treated in the generalized gradient approximation GGA-PBE [36]. The core
 249 configurations of Fe, Cr, Mn and Ni in PAW potentials are [Ar]3d⁷4s¹, [Ar]3d⁵4s¹, [Ar]3d⁶4s¹
 250 and [Ar]3d⁹4s¹, respectively. Total energies were calculated using the Monkhorst-Pack [37] mesh
 251 of 12x12x12 k-point for a four-atom FCC cubic cell. The plane wave cut-off energy used in the
 252 calculations was 400 eV. The total energy convergence criterion was set to 10⁻⁶ eV/cell, and force
 253 components were relaxed to 10⁻³ eV/nm. The DFT enthalpies of mixing were fitted into the cluster
 254 expansion given by Eq. 2 of the FCC CrFeMnNi system resulting in a minimal cross-validation
 255 criterion of 12.95 meV/atom, which is an indicator for the average difference $\Delta H_{DFT}^{Mixing}[\vec{\sigma}] -$
 256 $\Delta H_{CE}^{Mixing}[\vec{\sigma}]$ for all structures $\vec{\sigma}$ of the database employed to perform the cluster expansion. The
 257 database of structures for the cluster expansion consisted on 835 structures categorized by the
 258 difference of local environments in binaries (structures with two chemical elements: 58 CrFe, 55
 259 CrMn, 77 CrNi, 58 FeMn, 54 FeNi and 52 MnNi), ternaries (structures with three chemical elements:
 260 89 CrFeMn, 85 CrFeNi, 46 FeMnNi, and 66 CrMnNi); and 191 quaternaries CrFeMnNi.

261 In the semi canonical Monte Carlo calculations performed the temperature range and
 262 temperature steps are important. The accuracy of the thermodynamic integration method to calculate
 263 configuration entropy generally requires a lower temperature integration step, $\Delta T = 10$ K and also
 264 depends on the number of Monte Carlo passes [29]. In particular, we use a cell containing 2048
 265 atoms distributed into a 8x8x8 primitive unit cell, and average compositions for the ensemble given
 266 by Cr₁₈Fe₂₇Mn₂₇Ni₂₈ and equiatomic Cr₂₅Fe₂₅Mn₂₅Ni₂₅. The simulations start at high temperature
 267 3,000 K where the semi canonical potential at the high-temperature limit is given by $k_B T \ln(4)$ for
 268 equiatomic and $-k_B T \{0.18 * \ln(0.18) + 2 * 0.27 * \ln(0.27) + 0.28 * \ln(0.28)\}$ for Cr₁₈Fe₂₇Mn₂₇Ni₂₈
 269 [28], and then we integrated numerically the canonical potential in temperature steps of $\Delta T = 10$ K
 270 to reach $T = 100$ K for equiatomic and $T = 180$ K for the system with composition Cr₁₈Fe₂₇Mn₂₇Ni₂₈,
 271 respectively. For thermodynamic integration calculation of configuration entropy, we use theoretical
 272 formula 19.

273 3. Four-body probability functions in fcc Cr-Fe-Mn-Ni alloys

274 We apply the methods to the FCC CrFeMnNi system to calculate the temperature and
 275 composition dependent cluster probability distribution functions and the configuration entropy.

276 3.1. Cluster Expansion Hamiltonian for FCC CrFeMnNi

277 The cluster expansion Hamiltonian for the quaternary system CrFeMnNi consists in total of
 278 83 different decorated clusters distributed among 10 different non-decorated clusters: 4 decorated
 279 clusters for the point cluster, $\omega = 1, n = 1$; 6 decorated clusters for each pair cluster $\omega = 2, n =$
 280 $1, \dots, 6$; 10 decorated clusters for the non-decorated cluster $\omega = 3, n = 1$; 18 decorated clusters
 281 for the non-decorated cluster $\omega = 3, n = 2$; and 15 decorated clusters for the non-decorated cluster
 282 $\omega = 4, n = 1$. The decoration labels, (*s*) required to specify the clusters, are listed in Tab. 1. Each
 283 non-decorated cluster is defined by the coordinates (specified with respect to the standard Cartesian
 284 coordinate system in units of lattice spacing) of the lattice sites that it includes. The decorations define
 285 the chemical species allocated to each site in strictly the same order i.e. for $\omega = 2, n = 1$ cluster the

286 decoration (2,3) means that species 2 is allocated for site with coordinates (1,1,1) and species 3 is
 287 allocated for site with coordinates (1/3,3/2,3/2).

Table 1. ω , highest coordination shell n , decoration (s) and coordinates of points in the relevant clusters on FCC lattice. The coordinates are referred to the simple cubic Bravais lattice. Index (s) is the same as the sequence of points in the relevant cluster. The canonical order for decoration indexes, (s) _{i} , is 0,1,2 and 3 is Cr, Fe, Mn and Ni.

ω	n	(s)	Coordinates	ω	n	(s)	Coordinates
1	1	(0)	(1,1,1)	3	1	(1,1,1)	((1,1,1),(3/2,1,1/2),(1,3/2,1/2))
		(1)				(2,1,1)	
		(2)				(3,1,1)	
		(3)				(2,2,1)	
2	1	(1,1)	((1,1,1),(1,3/2,3/2))			(3,2,1)	
		(2,1)				(3,3,1)	
		(3,1)				(2,2,2)	
		(2,2)				(3,2,2)	
		(3,2)				(3,3,2)	
		(3,3)				(3,3,3)	
2	2	(1,1)	((1,1,1),(1,1,0))	3	2	(1,1,1)	((1,1,1),(1,3/2,1/2),(1,1,0))
		(2,1)				(2,1,1)	
		(3,1)				(3,1,1)	
		(2,2)				(1,2,1)	
		(3,2)				(2,2,1)	
		(3,3)				(3,2,1)	
2	3	(1,1)	((1,1,1),(2,3/2,3/2))			(1,3,1)	
		(2,1)				(2,3,1)	
		(3,1)				(3,3,1)	
		(2,2)				(2,1,2)	
		(3,2)				(3,1,2)	
		(3,3)				(2,2,2)	
2	4	(1,1)	((1,1,1),(2,1,2))			(3,2,2)	
		(2,1)				(2,3,2)	
		(3,1)				(3,3,2)	
		(2,2)				(3,1,3)	
		(3,2)				(3,2,3)	
		(3,3)				(3,3,3)	
2	5	(1,1)	((1,1,1),(1,3/2,-1/2))	4	1	(1,1,1,1)	((1,1,1),(3/2,3/2,1),(3/2,1,1/2),(1,3/2,1/2))
		(2,1)				(2,1,1,1)	
		(3,1)				(3,1,1,1)	
		(2,2)				(2,2,1,1)	
		(3,2)				(3,2,1,1)	
		(3,3)				(3,3,1,1)	
2	6	(1,1)	((1,1,1),(2,2,0))			(2,2,2,1)	
		(2,1)				(3,2,2,1)	
		(3,1)				(3,3,2,1)	
		(2,2)				(3,3,3,1)	
		(3,2)				(2,2,2,2)	
		(3,3)				(3,2,2,2)	
						(3,3,2,2)	
						(3,3,3,2)	
						(3,3,3,3)	

288 3.2. Semi canonical Monte Carlo simulations

289 After performing the Monte Carlo simulations for alloy compositions $\text{Cr}_{18}\text{Fe}_{27}\text{Mn}_{27}\text{Ni}_{28}$ and
 290 equiatomic $\text{Cr}_{25}\text{Fe}_{25}\text{Mn}_{25}\text{Ni}_{25}$, we use the correlation functions calculated at each of the temperatures
 291 to study the temperature dependent probabilities of decorated clusters corresponding to the
 292 equilibrium configuration $[\vec{\sigma}]$ of the Monte Carlo supercell following the formalisms described in

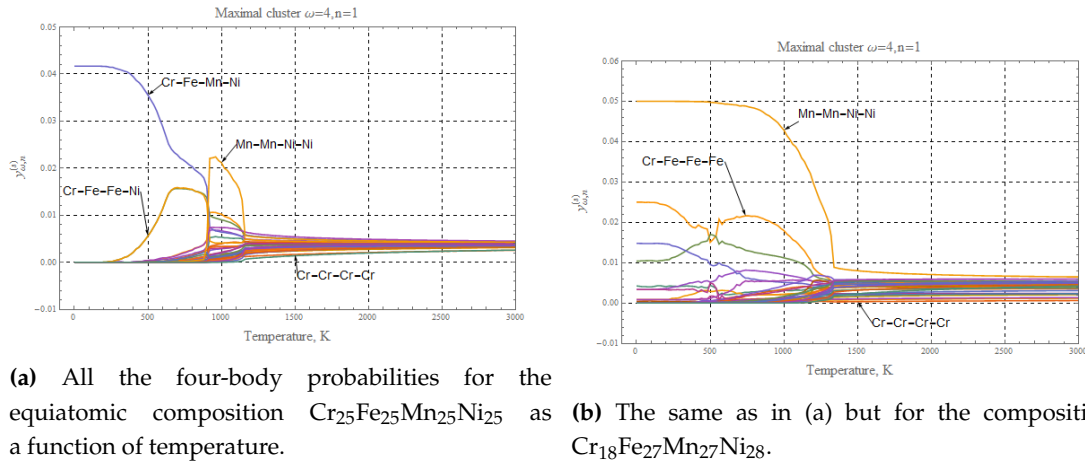


Figure 1. Four-body probabilities obtained from the hybrid CE-Monte Carlo calculations.

293 the Methods. For each non-decorated cluster ω, n and temperature we generate the corresponding
 294 τ^{-1} matrices with dimension $K^\omega \times K^\omega$ and a vector formed by all the decorated correlation cluster
 295 functions, $\langle \Gamma_{\omega,n}^{(ij\dots)}[\vec{\sigma}] \rangle$ with dimension K^ω . The Monte Carlo simulations output only the symmetry
 296 unique correlation functions (see Tab. 1), which are less than the K^ω required for matrix operation.
 297 In order to generate the full set of K^ω from the symmetrically unique correlation functions we devise
 298 a set of permutation operators g_i (see Tab. 2) that indicate how an arbitrary decoration ω -tuple of
 299 integers is obtained from the symmetrically unique decorations belonging to the non-decorated
 300 cluster or one of its sub-clusters (see the third column of Tab. 2 for identifying the cluster-sub-cluster
 301 relation). Tab. 2 contains all the operators necessary to generate cluster probabilities, $y_{\omega,n}^{(s)}$ for any
 302 possible decoration, (s) , of 9 non-decorated clusters employed in the cluster expansion Hamiltonian.
 303 We use the maximal cluster given by $\omega = 4, n = 1$ for obtaining the four-body
 304 temperature dependent configuration probabilities. In particular in Figs. 1 a-b, we plot the 35
 305 symmetrically unique probabilities for the four body maximal cluster defined by the set of lattice
 306 sites $((1, 1, 1), (3/2, 3/2, 1), (3/2, 1, 1/2), (1, 3/2, 1/2))$.

307 The most probable four-body bonding configurations in the temperature range from 0 to 3000 K
 308 for the two alloy systems (the equiatomic $\text{Cr}_{25}\text{Fe}_{25}\text{Mn}_{25}\text{Ni}_{25}$ and $\text{Cr}_{18}\text{Fe}_{27}\text{Mn}_{27}\text{Ni}_{28}$) are highlighted
 309 in Figs. 1 a-b. It should be noted that for both compositions the cluster configuration referred as
 310 Cr-Cr-Cr-Cr appears as the least probable of all the cluster configurations.

311 For the equiatomic composition Cr-Fe-Mn-Ni appears particularly probable at temperatures
 312 between 0-900 K, followed by Mn-Mn-Ni-Ni at temperatures between 900-1200 K. Furthermore, in the
 313 temperature range 0-900 K, the cluster configuration Cr-Fe-Fe-Ni shows as the second most probable
 314 configuration after the Cr-Fe-Mn-Ni configuration. Beyond 1200 K, all of the cluster configuration
 315 probabilities tend to the solid solution or random configuration.

316 For the system with average composition $\text{Cr}_{18}\text{Fe}_{27}\text{Mn}_{27}\text{Ni}_{28}$, the cluster probability of
 317 decorations given by Mn-Mn-Ni-Ni appears to dominate until 1300 K, where the solid solution or
 318 random configuration begins. Furthermore, the second most probable cluster configuration in the
 319 temperature range 500-1200 K appears to be Cr-Fe-Fe-Fe.

320 For each temperature value in the range 0-3000 K the configuration probabilities corresponding
 321 to cluster $\omega = 4, n = 1$ are used in Eq. 17 to obtain the quantities $\tilde{S}_{\omega_i, n_i}[\vec{\sigma}]$. There is one quantity
 322 $\tilde{S}_{\omega_i, n_i}[\vec{\sigma}]$ and a corresponding weight η_{ω_i, n_i} for each of the ω_i, n_i sub-clusters: $\omega = 1, n = 1$, $\omega =$
 323 $2, n = 1$; $\omega = 3, n = 1$; and $\omega = 4, n = 1$ included in the maximal cluster $\omega = 4, n = 1$. The total
 324 configuration entropy, $S_{\omega,n}[\vec{\sigma}]$, is calculated by adding the η_{ω_i, n_i} weighted quantities $\tilde{S}_{\omega_i, n_i}[\vec{\sigma}]$. By
 325 applying the same arguments developed for the cluster $\omega = 4, n = 1$, the total configuration entropy

326 for each of the 10 different maximal clusters can be calculated. The subclusters and the permutation
 327 operators contained in each of the 10 maximal clusters appearing in the cluster expansion are detailed
 328 in Tab. 2.

Table 2. Permutation tables for generating the full set of decorations K^ω from the set of 83 symmetry unique ones indicated in Tab. 1. The space group of the disordered FCC structure is O_h^5 and the decorations of clusters on which the operators permute sites are indicated in Tab. 1

Maximal cluster	Permutation operators $\{g_1, g_2, \dots\}$	Subcluster $\{\omega_i, n_i\}$	N_{ω_i, n_i}	$N_{\omega, n}^{\omega_i, n_i}$	η_{ω_i, n_i}
$\omega = 1, n = 1$	$\{(1)\}$	$\omega_1 = 1, n_1 = 1$	1	1	-1
$\omega = 2, n = 1$	$\{(1, X), (X, 1)\}$	$\omega_1 = 1, n_1 = 1$	1	2	11
$\omega = 2, n = 2$	$\{(1, 2), (2, 1)\}$	$\omega_2 = 2, n_2 = 1$	6	1	-6
	$\{(1, X), (X, 1)\}$	$\omega_1 = 1, n_1 = 1$	1	2	5
$\omega = 2, n = 3$	$\{(1, 2), (2, 1)\}$	$\omega_2 = 2, n_2 = 2$	3	1	-3
	$\{(1, X), (X, 1)\}$	$\omega_1 = 1, n_1 = 1$	1	2	23
$\omega = 2, n = 4$	$\{(1, 2), (2, 1)\}$	$\omega_2 = 2, n_2 = 3$	12	1	-12
	$\{(1, X), (X, 1)\}$	$\omega_1 = 1, n_1 = 1$	1	2	11
$\omega = 2, n = 5$	$\{(1, 2), (2, 1)\}$	$\omega_2 = 2, n_2 = 4$	6	1	-6
	$\{(1, X), (X, 1)\}$	$\omega_1 = 1, n_1 = 1$	1	2	23
$\omega = 2, n = 6$	$\{(1, 2), (2, 1)\}$	$\omega_2 = 2, n_2 = 5$	12	1	-12
	$\{(1, X), (X, 1)\}$	$\omega_1 = 1, n_1 = 1$	1	2	7
$\omega = 3, n = 1$	$\{(1, 2), (2, 1)\}$	$\omega_2 = 2, n_2 = 6$	4	1	-4
	$\{(1, X, X), (X, X, 1), (X, 1, X)\}$	$\omega_1 = 1, n_1 = 1$	1	3	-13
$\omega = 3, n = 2$	$\{(1, 2, X), (2, 1, X), (2, X, 1), (1, X, 2), (X, 1, 2), (X, 2, 1)\}$	$\omega_2 = 2, n_2 = 1$	6	3	18
	$\{(1, 3, 2), (3, 2, 1), (2, 1, 3), (3, 1, 2), (2, 3, 1), (1, 2, 3)\}$	$\omega_3 = 3, n_3 = 1$	8	1	-8
	$\{(1, X, X), (X, X, 1), (X, 1, X)\}$	$\omega_1 = 1, n_1 = 1$	1	3	-19
	$\{(2, 1, X), (1, 2, X)\}$	$\omega_2 = 2, n_2 = 2$	1	1	9
$\omega = 4, n = 1$	$\{(1, X, 2), (2, X, 1), (X, 1, 2), (X, 2, 1)\}$	$\omega_3 = 2, n_3 = 1$	6	2	18
	$\{(3, 1, 2), (1, 3, 2), (1, 2, 3)\}$	$\omega_4 = 3, n_4 = 2$	12	1	-12
	$\{(1, X, X, X), (X, X, X, 1), (X, X, 1, X), (X, 1, X, X)\}$	$\omega_1 = 1, n_1 = 1$	1	4	-5
	$\{(X, X, 1, 2), (X, X, 2, 1), (1, 2, X, X), (2, 1, X, X), (X, 1, X, 2), (X, 2, X, 1), (2, X, 1, X), (1, X, 2, X), (1, X, X, 2), (2, X, X, 1), (X, 1, 2, X), (X, 2, 1, X)\}$	$\omega_2 = 2, n_2 = 1$ $\omega_2 = 2, n_2 = 1$ $\omega_2 = 2, n_2 = 1$	6 6 6	6	6
$\{(1, 3, 2, X), (3, 1, X, 2), (2, X, 1, 3), (X, 2, 3, 1), (3, 2, 1, X), (1, X, 3, 2), (X, 1, 2, 3), (2, 3, X, 1), (2, 1, 3, X), (X, 3, 1, 2), (1, 2, X, 3), (3, X, 2, 1), (2, X, 3, 1), (X, 2, 1, 3), (1, 3, X, 2), (3, 1, 2, X), (1, X, 2, 3), (3, 2, X, 1), (2, 3, 1, X), (X, 1, 3, 2), (3, X, 1, 2), (1, 2, 3, X), (X, 3, 2, 1), (2, 1, X, 3)\}$	$\omega_3 = 3, n_3 = 1$ $\omega_3 = 3, n_3 = 1$ $\omega_3 = 3, n_3 = 1$ $\omega_3 = 3, n_3 = 1$ $\omega_3 = 3, n_3 = 1$ $\omega_3 = 3, n_3 = 1$	8 8 8 8 8	4	0	
$\{(1, 4, 3, 2), (4, 1, 2, 3), (3, 2, 1, 4), (2, 3, 4, 1), (4, 3, 1, 2), (1, 2, 4, 3), (2, 1, 3, 4), (3, 4, 2, 1), (3, 1, 4, 2), (2, 4, 1, 3), (1, 3, 2, 4), (4, 2, 3, 1), (3, 2, 4, 1), (2, 3, 1, 4), (1, 4, 2, 3), (4, 1, 3, 2), (1, 2, 3, 4), (4, 3, 2, 1), (3, 4, 1, 2), (2, 1, 4, 3), (4, 2, 1, 3), (1, 3, 4, 2), (2, 4, 3, 1), (3, 1, 2, 4)\}$	$\omega_4 = 4, n_4 = 1$ $\omega_4 = 4, n_4 = 1$ $\omega_4 = 4, n_4 = 1$ $\omega_4 = 4, n_4 = 1$ $\omega_4 = 4, n_4 = 1$ $\omega_4 = 4, n_4 = 1$	2 2 2 2 2	1	-2	

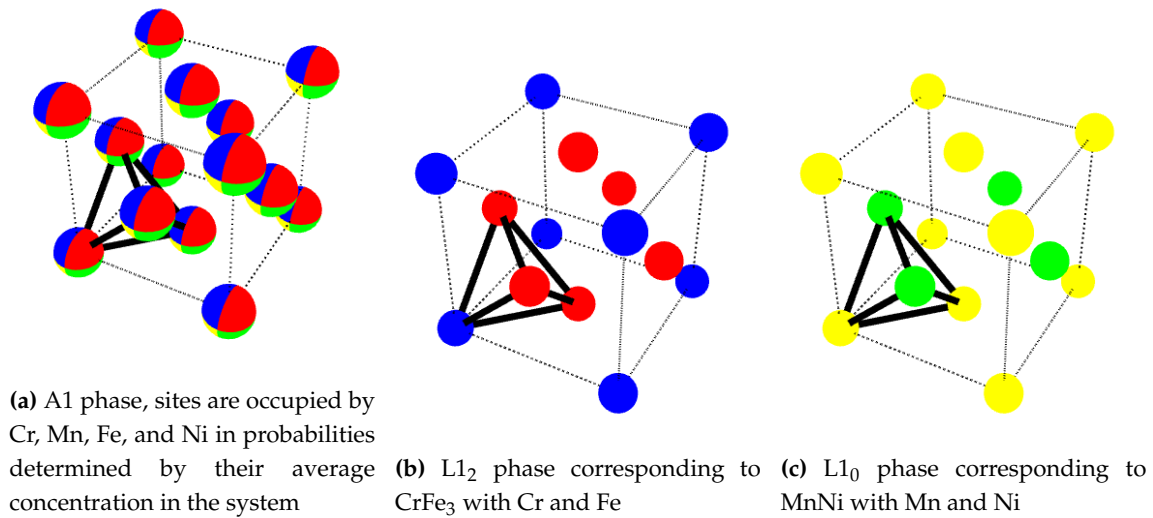


Figure 2. (a) Most probable phase at high temperature (disordered structure); (b) and (c): two most probable ordered phases at low temperature in the equiatomic Cr₂₅Fe₂₅Mn₂₅Ni₂₅ and Cr₁₈Fe₂₇Mn₂₇Ni₂₈ HEAs compositions. Cr, Fe, Mn and Ni are illustrated in blue, red, yellow and green respectively.

3.3. Origin of the high correlation functions Mn-Mn-Ni-Ni and Cr-Fe-Fe-Fe in the low temperature region

The symmetry unique decorations, (s) , are generated by studying all of the decorations $(s)_{\omega_i, n_i}$ from the sub-clusters ω_i, n_i in ω, n that have decorations with empty cluster, i.e. at least one integer entry in $0 \subseteq (s)_{\omega_i, n_i}$. For example, in the case of a two-body cluster consisting of sites $\{(1, 1, 1), (1, 3/2, 3/2)\}$, see Tab. 1, we have $4^2 = 16$ 2-tuples of decorations. It can be noted that the cluster $\{(1, 1, 1), (1, 3/2, 3/2)\}$ contains two sub-clusters: the point cluster $\{(1, 1, 1)\}$ that has decorations $\{(0), (1), (2), (3)\}$ and the cluster itself which has decorations $\{(1, 1), (2, 1), (3, 1), (2, 2), (2, 3), (3, 3)\}$. In general any given sub-cluster ω_i, n_i can be contained several times inside the cluster ω, n . For example in this case the the point cluster is contained twice: one time in $(1, 1, 1) \subset \{(1, 1, 1), (1, 3/2, 3/2)\}$ and also in $(1, 3/2, 3/2)\{(1, 1, 1), (1, 3/2, 3/2)\}$; similarly the cluster itself $\{(1, 1, 1), (1, 3/2, 3/2)\}$ is contained just once. To transfer the sub-cluster decorations in notation ω_i tuples to ω tuples notation we make use of the empty cluster X . Thus a point cluster decorated by $(s) = (3)$ is transferred to ω tuples notation in the maximal cluster as $(3, 0)$ or $(0, 3)$; this can be captured by the permutation operators $\{(1, X), (X, 1)\}$ (see Tab. 2) where X stands for empty cluster where a 0 should be placed. Similarly the ω tuples $(1, 2)$ in the ω cluster notation are equivalent to $(1, 2)$ and $(2, 1)$, this can again be captured by permutation operators $\{(1, 2), (2, 1)\}$, where X no longer appears, since the ω_i tuples have the same order as the ω tuples.

The analysis outlined above for the two body cluster $\{(1, 1, 1), (1, 3/2, 3/2)\}$ with $K = 4$ components can be extended to larger clusters. The permutation operators that carry the appropriate decorations $(s)_{\omega_i, n_i}$ of sub-clusters ω_i, n_i into ω, n cluster ω tuples notation are detailed in Tab. 2. It should be noted that for any two body cluster, the point and corresponding pair sub-clusters add up forming $4 + 6 = 10$ symmetrically unique correlation functions $\langle \Gamma_{\omega, n}^{(ij)}[\vec{\sigma}] \rangle$.

In general the total number correlation functions K^ω required to describe a maximal cluster in the CE can be found by summing the total number of symmetrically unique decorations for all of the sub-clusters included in a given maximal cluster. The symmetry unique decorations for each of the sub-clusters is reported in ATAT clusters.out file and here it is summarized in the Tab. 1, and the particular sub-clusters included in a maximal cluster are listed in the Tab. 2. If the sub-cluster has $\omega_i < \omega$, then the decorations from the sub-cluster can be transferred into the decorations of the

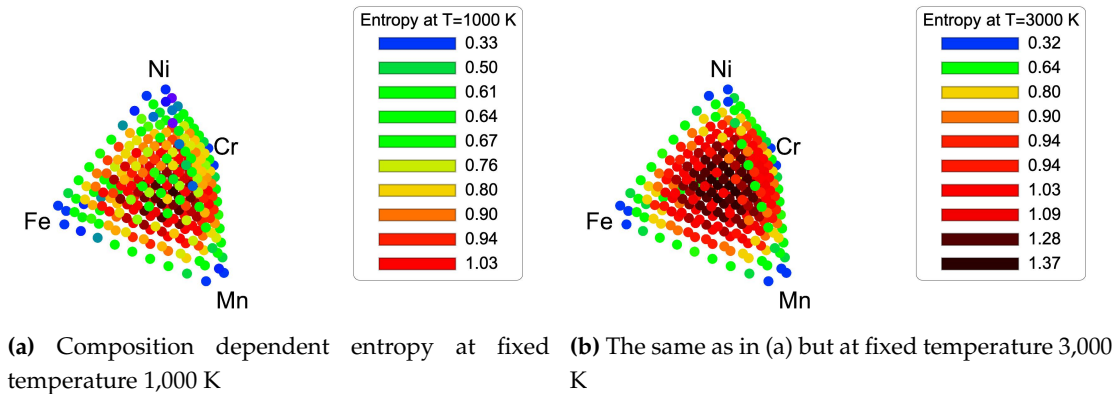


Figure 3. Composition dependent entropies obtained from Monte Carlo simulations in CE.

357 maximal cluster by using the permutation operators in Tab. 2 including X for the empty site. For
 358 example, the cluster ($\omega = 3, n = 1$) has 3 sub-clusters ($\omega_1 = 1, n_1 = 1$), ($\omega_2 = 2, n_2 = 1$) and
 359 ($\omega_3 = 3, n_3 = 1$), the number of permutation operators associated with sub-cluster ($\omega_1 = 1, n_1 = 1$)
 360 is 4; for ($\omega_2 = 2, n_2 = 1$) we find 6 permutation operators; and for the cluster itself ($\omega_3 = 3, n_3 = 1$)
 361 we find 6 permutation operators. The point sub-cluster ($\omega_1 = 1, n_1 = 1$) has, according to Tab. 1,
 362 4 decorations associated to it; the two body cluster ($\omega_2 = 2, n_2 = 1$) has 6 decorations associated to
 363 itself; and finally the sub-cluster ($\omega_3 = 3, n_3 = 1$) has 10 decorations associated to itself. On the other
 364 hand, the number of symmetrically unique correlation functions, which is smaller than K^ω , but can
 365 nevertheless fully describe cluster ($\omega = 3, n = 1$) with $K = 4$ components is given by $4 + 5 + 10 = 19$
 366 correlation functions. The remaining decorations 45 are obtained by using appropriately the $3 + 6 +$
 367 $6 = 15$ permutation operators. Similarly maximal cluster ($\omega = 3, n = 2$) has 34 symmetrically unique
 368 decorations and ($\omega = 4, n = 1$) has 35 decorations.

369 The structure with configuration Mn-Mn-Ni-Ni can be understood as L1₀ in strukturbericht
 370 notation with Mn and Ni, similarly the structure with composition Cr-Fe-Fe-Fe can be understood as
 371 L1₂ in strukturbericht notation; both of these structures are depicted in Fig. 2. The entropy increase
 372 (Fig. 3) with temperature corresponding to the equiatomic alloy composition can thus be understood
 373 by the decrease in probabilities (Figs. 1) with temperature of the ordered states corresponding
 374 to the structures L1₀ towards the disorder configuration A1 (see Fig. 2 depicting this ordered
 375 structure and the disordered phase). Similarly, in the alloy with composition Cr₁₈Fe₂₇Mn₂₇Ni₂₈,
 376 the high probability of the configuration Cr-Fe-Fe-Fe is found to be correlated to the ordered
 377 structure L1₂-CrFe₃. In particular, the latter structure has been found to be stable due to the strong
 378 anti-ferromagnetic interaction between Cr and Fe from DFT calculations performed for the FeCrNi
 379 system [38]. In that work, Monte Carlo simulations using magnetic cluster expansion indicated that
 380 ordered magnetic structures in the Ni-rich corner (ferromagnetic) of the *FeCrNi* system persists until
 381 temperatures of 600 K, and that for the atomic compositions between CrFe₂ and CrFe₃ magnetic order
 382 (anti-ferromagnetic) was retained beyond 500 K. Similarly the structure L1₀-MnNi was found to be
 383 among the most stable intermetallic structures with the smallest enthalpy of mixing in the FeCrNi
 384 FCC system [39].

385 4. Configuration entropy in Cr-Fe-Mn-Ni system

386 Composition dependent entropies at fixed temperatures 1000 K and 3000 K are shown in Fig.
 387 3 a-b. At each of these temperature values, any of the configuration entropy expressions from Tab.
 388 2 provides approximately the same value. At 3000 K, the entropy is maximized in the center of the
 389 tetrahedron namely at the equiatomic composition to $1.37 k_B$, and it is decreased upon lowering the

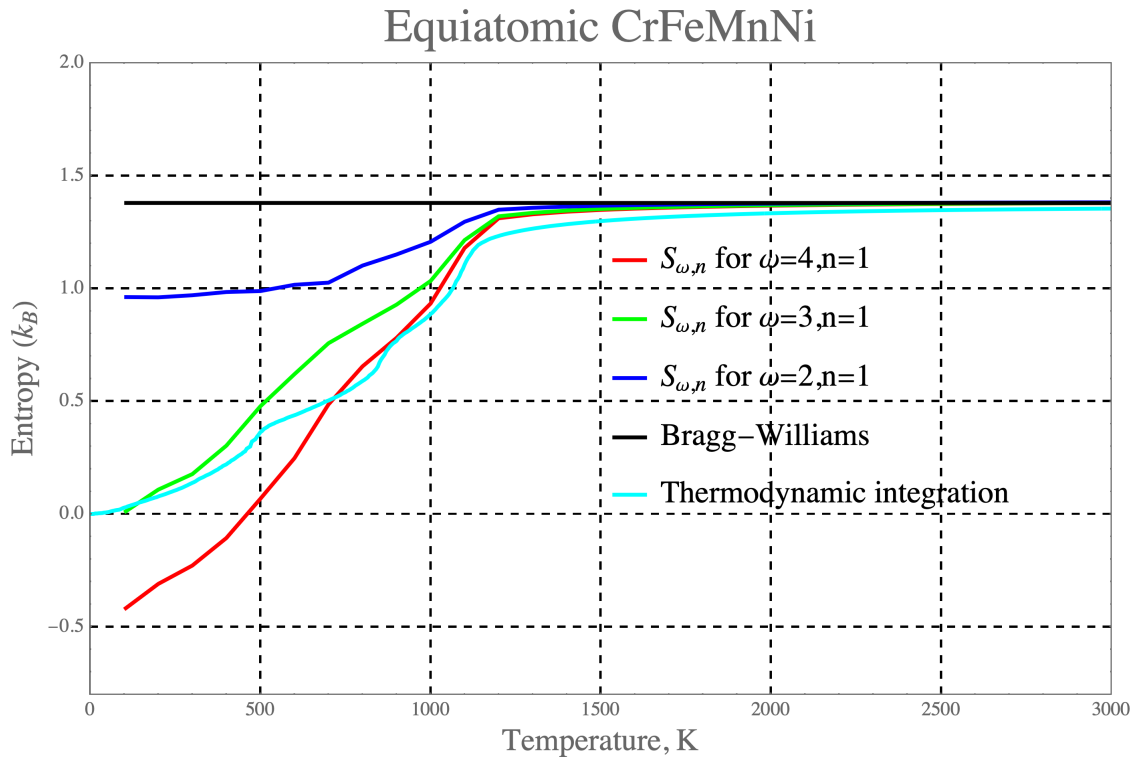


Figure 4. Temperature dependent entropy in equiatomic composition $\text{Cr}_{25}\text{Fe}_{25}\text{Mn}_{25}\text{Ni}_{25}$

390 temperature at all of the composition points. The variation of configuration entropy is too complex to
 391 be captured in the fixed temperature plots, therefore we use specifically the equiatomic composition
 392 and calculate the configuration entropy as a function of temperature in Fig. 4. Regarding the high
 393 temperature limit value of entropy Figs. 4, we use as maximal cluster that from the four body, three
 394 body and two body in the nearest neighbor cluster probabilities. We see that at low temperatures,
 395 the entropy becomes slightly negative with respect the thermodynamic integration value, whilst the
 396 high temperature limit of disordered solid solution $-k_B \sum_p x_p[\vec{\sigma}] \ln(x_p[\vec{\sigma}])$ is achieved faster than in
 397 the thermodynamic integration approximation. The reason the high temperature limit is preserved
 398 can be clearly seen from the factorization of the CE expression that resulted in Eq. 15.

399 5. Conclusions

400 The design of radiation tolerant materials for advanced nuclear reactor systems can be
 401 accelerated by using ab initio computational materials science. The composition $\text{Cr}_{18}\text{Fe}_{27}\text{Mn}_{27}\text{Ni}_{28}$
 402 multicomponent system has been studied for advanced nuclear applications due to the removal of
 403 Co, which can cause activation by transmutation of ^{60}Co isotope during service in a nuclear reactor
 404 and promising irradiation resistance with regards to void swelling.

405 In this work we develop a matrix formalism to study multi-body ordering probabilities, SRO
 406 and configuration entropy. We apply our methods to the system CrFeMnNi for use in the CE. The
 407 cluster probabilities are worked out by explicit inversion and direct product of a matrix formulation
 408 obtained from symmetry independent correlation functions. The correlation functions are determined
 409 from semi-canonical Monte Carlo simulations and ECIs derived from DFT calculations. In particular,
 410 we apply our methods to the specific case of FCC CrFeMnNi HEA by considering 285 different alloy
 411 compositions covering the compositional space of the quaternary alloy as a function of temperature.
 412 To further assess our formulated expressions for configuration entropy, focus is put at two alloy
 413 compositions equiatomic $\text{Cr}_{25}\text{Fe}_{25}\text{Mn}_{25}\text{Ni}_{25}$ and $\text{Cr}_{18}\text{Fe}_{27}\text{Mn}_{27}\text{Ni}_{28}$ to obtain cluster probabilities
 414 and understand the variation in configuration entropy with temperature due to the lowering the

415 ordering probability corresponding to the ordered configuration. The cluster probability plots against
 416 temperature show that for the composition $\text{Cr}_{18}\text{Fe}_{27}\text{Mn}_{27}\text{Ni}_{28}$ there is high probability of formation of
 417 the $L1_0$ MnNi phase at low temperatures below 1300 K and for the $L1_2$ CrFe_3 phase in the temperature
 418 range 500-1200 K. Similarly for the equiatomic composition the $L1_0$ MnNi phase appears stable in the
 419 temperature range 900-1200 K, while the lower temperature region is preferred for the configuration
 420 Cr-Fe-Mn-Ni. The configuration Cr-Cr-Cr-Cr was found to be the least probable configuration at
 421 all temperature ranges for both compositions of the Cr-Fe-Mn-Ni system. Furthermore, configuration
 422 entropy as a function of temperature was derived from these probabilities: the high-temperature limit
 423 is in accordance with random solid solution approximation; but at low temperatures, the entropy is
 424 seen to be reduced due to ordering or segregation tendencies.

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 437 CrFeMnNi system. AFC, DNM and JSW wrote the manuscript and PMM checked grammar. JSW and MF
 438 provided the results of DFT-based semi canonical Monte Carlo simulations for CrFeMnNi system. All the authors
 439 made comments into the final version before its submission.

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441 Abbreviations

442 The following abbreviations are used in this manuscript:

443
 444 CE: Cluster Expansion

445 CVM: Cluster Variation Method

446 HEA: High-Entropy Alloy

447 K : Number of components in alloy

448 DFT: Density Functional Theory

449 GS: Ground States

450 G : Space Group of the disordered high temperature structure

451 (ω_i, n_i) : i^{th} sub-cluster of a maximal cluster (ω, n)

452 $\mathcal{N}_{\omega_i, n_i}$: operators $g \in G$ acting on the sites of cluster (ω_i, n_i) to rearrange the sites i.e. a permutation

453 N_{ω_i, n_i} : site multiplicity of the cluster ω_i

454 $N_{\omega, n}^{\beta}$: sub-cluster multiplicity of the cluster $\beta \in (\omega, n)$

455 $\Omega[\omega, n]$: Number of times a cluster ω, n is contained in a supercell structure, generally used for
 456 Monte Carlo simulations, for obtaining thermodynamic quantities.

457

458 Bibliography

- 459 1. Cantor, B.; Chang, I.; Knight, P.; Vincent, A. Microstructural development in equiatomic multicomponent
 460 alloys. *Materials Science and Engineering A* **2004**, *375-377*, 213–218.
- 461 2. Yeh, J.W.; Chen, S.K.; Lin, S.J.; Gan, J.Y.; Chin, T.S.; Shun, T.T.; Tsau, C.H.; Chang, S.Y. Nanostructured
 462 High-Entropy Alloys with Multiple Principal Elements: Novel Alloy Design Concepts and Outcomes.
 463 *Advanced Engineering Materials*, *6*, 299–303.
- 464 3. Gali, A.; George, E.P. Tensile properties of high- and medium-entropy alloys. *Intermetallics* **2013**, *39*, 74–78.

- 465 4. Carroll, R.; Lee, C.; Tsai, C.W.; Yeh, J.W.; Antonaglia, J.; Brinkman, B.A.W.; Leblanc, M.; Xie, X.;
466 Chen, S.; Liaw, P.K.; Dahmen, K.A. Experiments and Model for Serration Statistics in Low-Entropy,
467 Medium-Entropy, and High-Entropy Alloys. *Scientific Reports* **2015**, *5*, 16997.
- 468 5. Xia, S.; Gao, M.C.; Yang, T.; Liaw, P.K.; Zhang, Y. Phase stability and microstructures of high entropy
469 alloys ion irradiated to high doses. *Journal of Nuclear Materials* **2016**, *480*, 100–108.
- 470 6. Lucas, M.S.; Mauger, L.; Muñoz, J.A.; Xiao, Y.; Sheets, A.O.; Semiatin, S.L.; Horwath, J.; Turgut, Z.
471 Magnetic and vibrational properties of high-entropy alloys. *Journal of Applied Physics* **2011**, *109*, 07E307.
- 472 7. Calvo-Dahlborg, M.; Cornide, J.; Tobola, J.; Nguyen-Manh, D.; Wróbel, J.S.; Juraszek, J.; Jouen, S.;
473 Dahlborg, U. Interplay of electronic, structural and magnetic properties as the driving feature of
474 high-entropy CoCrFeNiPd alloys. *J. Phys. D: Appl. Phys.* **2017**, *50*, 185002.
- 475 8. Rossiter, P.L.; Wells, P. The dependence of the electrical resistivity on short-range order. *Journal of Physics*
476 *C: Solid State Physics* **1971**, *4*, 354–363.
- 477 9. Spruiell, J.E.; Stansbury, E.E. X-Ray study of short-range order in nickel alloys containing 10.7 and 20.0
478 at. % Molybdenum. *Journal of Physics and Chemistry of Solids* **1965**, *26*, 811–822.
- 479 10. Fisher, J.C. On the strength of solid solution alloys. *Acta Metallurgica* **1954**, *2*, 9–10.
- 480 11. Fernández-Caballero, A.; Wróbel, J.S.; Mummery, P.M.; Nguyen-Manh, D. Short-Range Order in High
481 Entropy Alloys: Theoretical Formulation and Application to Mo-Nb-Ta-V-W System. *Journal of Phase*
482 *Equilibria and Diffusion* **2017**, *38*, 391–403.
- 483 12. Santodonato, L.J.; Zhang, Y.; Feygenson, M.; Parish, C.M.; Gao, M.C.; Weber, R.J.K.; Neuefeind, J.C.;
484 Tang, Z.; Liaw, P.K. Deviation from high-entropy configurations in the atomic distributions of a
485 multi-principal-element alloy. *Nature communications* **2015**, *6*, 5964.
- 486 13. Leong, Z.; Wróbel, J.S.; Dudarev, S.L.; Goodall, R.; Todd, I.; Nguyen-Manh, D. The Effect of Electronic
487 Structure on the Phases Present in High Entropy Alloys. *Scientific Reports* **2017**, *7*, 39803.
- 488 14. Van de Walle, A. Multicomponent multisublattice alloys, nonconfigurational entropy and other
489 additions to the Alloy Theoretic Automated Toolkit. *Calphad: Computer Coupling of Phase Diagrams and*
490 *Thermochemistry* **2009**, *33*, 266–278.
- 491 15. Lu, Z.W.; Wei, S.H.; Zunger, A.; Frota-Pessoa, S.; Ferreira, L.G. First-principles statistical mechanics of
492 structural stability of intermetallic compounds. *Physical Review B* **1991**, *44*, 512–544.
- 493 16. Lechermann, F.; Fähnle, M.; Sanchez, J.M. First-principles investigation of the Ni-Fe-Al system.
494 *Intermetallics* **2005**, *13*, 1096–1109.
- 495 17. Ackermann, H.; Inden, G.; Kikuchi, R. Tetrahedron approximation of the cluster variation method for
496 b.c.c. alloys. *Acta Metallurgica* **1989**, *37*, 1–7.
- 497 18. Tepesch, P.D.; Asta, M.; Ceder, G. Computation of configurational entropy using Monte Carlo
498 probabilities in cluster-variation method entropy expressions. *Modelling and Simulation in Materials Science*
499 *and Engineering* **1998**, *6*, 787–797.
- 500 19. Kumar, N.K.; Li, C.; Leonard, K.; Bei, H.; Zinkle, S. Microstructural stability and mechanical behavior of
501 FeNiMnCr high entropy alloy under ion irradiation. *Acta Materialia* **2016**, 113.
- 502 20. Hart, G.L.W.; Forcade, R.W. Algorithm for generating derivative structures. *Physical Review B - Condensed*
503 *Matter and Materials Physics* **2008**, 77.
- 504 21. Cenedese, P.; Gratias, D. Multicomponent formalism in the mean-field approximation: a geometric
505 interpretation of Chebychev polynomials. *Physica A: Statistical Mechanics and its Applications* **1991**,
506 179, 277–287.
- 507 22. Sluiter, M.H.; Kawazoe, Y. Invariance of truncated cluster expansions for first-principles alloy
508 thermodynamics. *Physical Review B - Condensed Matter and Materials Physics* **2005**, *71*, 1–2.
- 509 23. Blum, V.; Zunger, A. Prediction of ordered structures in the bcc binary systems of Mo, Nb, Ta, and W from
510 first-principles search of approximately 3,000,000 possible configurations. *Physical Review B - Condensed*
511 *Matter and Materials Physics* **2005**, *72*, 3–6.
- 512 24. Finel, A. The cluster variation method and some applications. In *Proceedings of NATO Advanced Study*
513 *Institute on Statics and Dynamics of Alloy Phase Transformations*; Turchi, P.E.A.; Gonis, A., Eds.; Springer:
514 Rhodes, Greece, 1992; pp. 495–540.
- 515 25. Kikuchi, R. A Theory of Cooperative Phenomena. *Physical Review* **1951**, *81*, 988–1003.
- 516 26. Barker, J.A. Methods of Approximation in the Theory of Regular Mixtures. *Proceedings of the Royal Society*
517 *A: Mathematical, Physical and Engineering Sciences* **1953**, *216*, 45–56.

- 518 27. Gratias, D.; Sanchez, J.; De Fontaine, D. Application of group theory to the calculation of the
519 configurational entropy in the cluster variation method. *Physica A: Statistical Mechanics and its Applications*
520 **1982**, *113*, 315–337.
- 521 28. Van de Walle, A.; Asta, M. Self-driven lattice-model Monte Carlo simulations of alloy thermodynamic
522 properties and phase diagrams. *Modelling and Simulation in Materials Science and Engineering* **2002**,
523 *10*, 521–538.
- 524 29. Wróbel, J.S.; Nguyen-Manh, D.; Kurzydłowski, K.J.; Dudarev, S.L. A first-principles model for anomalous
525 segregation in dilute ternary tungsten-rhenium-vacancy alloys. *Journal of Physics: Condensed Matter* **2017**,
526 *29*, 145403.
- 527 30. Blöchl, P.E. Projector augmented-wave method. *Phys. Rev. B* **1994**, *50*, 17953–17979.
- 528 31. Kresse, G.; Hafner, J. Ab initio molecular-dynamics simulation of the
529 liquid-metal–amorphous-semiconductor transition in germanium. *Phys. Rev. B* **1994**, *49*, 14251–14269.
- 530 32. Kresse, G.; Joubert, D. From ultrasoft pseudopotentials to the projector augmented-wave method. *Phys.*
531 *Rev. B* **1999**, *59*, 1758–1775.
- 532 33. Kresse, G.; Hafner, J. Ab initio molecular dynamics for liquid metals. *Phys. Rev. B* **1993**, *47*, 558–561.
- 533 34. Kresse, G.; Furthmüller, J. Efficient iterative schemes for ab initio total-energy calculations using a
534 plane-wave basis set. *Phys. Rev. B* **1996**, *54*, 11169–11186.
- 535 35. Kresse, G.; Furthmüller, J.; Furthmüller B', J. Efficiency of ab-initio total energy calculations for metals
536 and semiconductors using a plane-wave basis set. *Comput. Mater. Sci.* **1996**, *6*, 15–50.
- 537 36. Perdew, J.P.; Burke, K.; Ernzerhof, M. Generalized Gradient Approximation Made Simple. *Phys. Rev.*
538 *Lett.* **1996**, *77*, 3865–3868.
- 539 37. Monkhorst, H.J.; Pack, J.D. Special points for Brillouin-zone integrations. *Phys. Rev. B* **1976**, *13*, 5188–5192.
- 540 38. Lavrentiev, M.Y.; Wróbel, J.S.; Nguyen-Manh, D.; Dudarev, S.L.; Ganchenkova, M.G. Magnetic cluster
541 expansion model for random and ordered magnetic face-centered cubic Fe-Ni-Cr alloys. *J. Appl. Phys.*
542 **2016**, *120*, 043902.
- 543 39. Wróbel, J.S.; Nguyen-Manh, D.; Lavrentiev, M.Y.; Muzyk, M.; Dudarev, S.L. Phase stability of ternary fcc
544 and bcc Fe-Cr-Ni alloys. *Phys. Rev. B* **2015**, *91*, 024108.