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Experimental studies of plasma-antenna coupling with the JET Alfvén Eigenmode Active Diagnostic

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Abstract.

This paper presents a dedicated study of plasma-antenna (PA) coupling with the Alfvén Eigenmode Active Diagnostic (AEAD) in JET. Stable AEs and their resonant frequencies f , damping rates $\gamma < 0$, and toroidal mode numbers n are measured for various PA separations and limiter versus X-point magnetic configurations. Two stable AEs are observed to be resonantly excited at distinct low and high frequencies in limiter plasmas. The values of f and n do not vary with PA separation. However, $|\gamma|$ increases with PA separation for the low- f , but not high- f , mode, yet this may be due to slightly different edge conditions. The high- f AE is detected throughout the transition from limiter to X-point configuration, though its damping rate increases; the low- f mode, on the other hand, becomes unidentifiable. The linear resistive MHD code CASTOR is used to simulate the frequency scan of an AEAD-like external antenna. For the limiter pulses, the high- f mode is determined to be an $n = 0$ GAE, while the low- f mode is likely an $n = 2$ TAE. During the transition from limiter to X-point configuration, CASTOR indicates that $n = 1$ and 2 EAEs are excited in the edge gap. These results extend previous experimental studies in JET and Alcator C-Mod; validate the computational work performed by Dvornova *et al* 2020 *Phys. Plasmas* **27** 012507; and provide guidance for the optimization of PA coupling in upcoming JET energetic particle experiments, for which the AEAD will aim to identify the contribution of alpha particles to AE drive during the DT campaign.

Keywords: Alfvén Eigenmodes, stability, plasma-antenna coupling, magnetic configuration

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1. Introduction

The understanding of Alfvén Eigenmodes (AEs) and their stability is vital to the success of future tokamaks with significant energetic particle (EP) populations which can destabilize AEs and thereby lead to enhanced EP transport. Unstable AEs, with growth rates $\gamma > 0$, are often easily observed in the Fourier spectra of magnetic data as coherent structures with well-defined resonant frequencies $\omega_0 = 2\pi f_0$ and toroidal mode numbers n . However, if the EP population is insufficient to overcome various AE damping mechanisms - i.e. the total AE growth rate is $\gamma < 0$ - then the *stable* AEs can only be detected through active antenna excitation. This will likely be the case even in the upcoming JET DT campaign during which the alpha population alone may not destabilize AEs. Fortunately, studies of active antenna excitation have been pursued in JET [1–34] and Alcator C-Mod [19, 21, 35–37], among other devices.

The Alfvén Eigenmode Active Diagnostic (AEAD), also known as the AE antenna, comprises two arrays of four toroidally spaced antennas (eight in total) installed inside the JET vacuum vessel [22, 38, 39]. Six amplifiers power six of the eight antennas with currents typically of the order 5 – 10 A; thus, the system is only slightly perturbative with $|\delta B/B| \leq 10^{-3}$ at the plasma edge [22, 31]. Independent phasing of the antennas allows power to be injected into a spectrum of toroidal modes with $n \leq 20$ [31, 34]. Three frequency filters allow the AE antenna to scan the ranges $\Delta f = 25 - 50$ kHz, 75 – 150 kHz, and 125 – 250 kHz. As the antenna frequency passes through an AE resonant frequency, the plasma responds like a driven, weakly damped harmonic oscillator, and the excited mode is detected by up to fourteen fast magnetic probes. Resonance parameters f_0 , γ , and n can be calculated from the synchronously detected magnetic data; for further details, see [34].

It is of interest to study the coupling of the AE antenna with the plasma [40], that is, to study the ability of the antennas to excite AE resonances. This is determined not only by the applied currents, frequencies, and relative phases of the antennas set by AEAD operators, but also by plasma parameters. For example, the efficiency of the AE antenna has been found to decrease with the plasma current, i.e. for $I_p > 2$ MA, in recent work [34]. In this paper, we explore the impact of the magnetic geometry on plasma-antenna (PA) coupling and AE stability. In particular, we focus on the magnetic configuration (i.e. limiter versus X-point-see Fig. 2b, for example) and PA separation. Importantly, for some JET experiments, the configuration and plasma position can be optimized to improve coupling and increase the likelihood of stable AE excitation. This is essential for the successful operation of the AE antenna in the upcoming JET DT campaign and for key measurements of alpha particle drive [41].

Yet it is not enough to have only the excitation of stable AEs; these resonances must also be measured by the magnetic sensors. However, the optimizations of resonance excitation and detection are separable because each action is performed by different system and thus can (usually) be assessed independently. For instance, the plasma can be shaped to decrease the plasma-antenna and/or plasma-sensor separation distances. In this work, we focus on

stable AE excitation as it relates to PA coupling, but do note when our actuation also affects detection.

The outline of the rest of the paper is as follows: In Section 2, we expand upon past studies of PA coupling and motivate this work. Then, we explore the impact of PA separation on coupling for limiter plasmas in Section 3. The effect of the magnetic configuration is investigated in Section 4 for plasmas transitioning from limiter to X-point. Sections 2 to 4 each have subsections on experimental and computational work. Finally, a summary is given in Section 5.

2. Motivation

In this section, we provide an overview of past experimental studies and recent computational efforts to understand the coupling between the plasma and AE antenna. Gaps in experiment and new predictions from simulations motivate this work.

2.1. Past experimental efforts

The original AEAD system in JET consisted of re-purposed, in-vessel saddle coils capable of probing low toroidal mode numbers $|n| \leq 2$ [1, 3]. In early JET experiments, stable AEs could not be excited by the AE antenna when the plasma was in an X-point (or diverted) magnetic configuration [4, 8, 11, 12]. This was attributed to wave absorption caused by strong edge magnetic shear. The first stable AEs observed during X-point in JET were reported in [10]; multiple modes were detected at different frequencies and identified as possible Drift Kinetic Toroidicity-induced Alfvén Eigenmodes (DK-TAEs). Following studies showed that real-time tracking of stable AEs could be achieved in JET X-point plasmas [21] and that the transition from limiter to X-point configuration could increase the AE damping rate approximately threefold [17, 28]. However, it should be noted that this latter observation may have been conflated with co-varying thermal plasma parameters.

Inspired by JET experiments, two poloidally separated antennas were installed at one toroidal location in Alcator C-Mod to actively probe stable AEs [35]. Resonances were measured in both limiter and X-point plasmas. Interestingly, lower damping rates (i.e. γ values closer to 0) were measured of stable AEs in X-point compared to limiter configuration, a trend opposite to that observed in JET. In addition, the damping rate was found to increase with the outer gap, and therefore with PA separation. The authors of [35] posited that differences in PA coupling for different magnetic configurations could be the cause.

Until this work, a dedicated study of PA coupling had not been performed in JET using the recently upgraded AE antenna system. The results have important implications for the interpretation of our measurements. In particular, we investigate how the magnetic geometry (configuration and PA separation) affect PA coupling, observations of resonances, and inferred resonance parameters (f_0 , γ/ω_0 , and n).

2.2. Recent computational efforts

This study is also motivated by recent computational work which accurately modeled PA coupling and explained some of the experimental observations of the previous section. In the study by Dvornova *et al* [40], the effects of PA separation and magnetic configuration on the efficiency of the JET AE antenna were thoroughly investigated using the linear, resistive MHD code CASTOR [42,43] and nonlinear, reduced MHD code JOREK [44]. In both codes, an external antenna was modeled in the vacuum region between the plasma and wall. An $n = 1$ antenna perturbation was simulated, and its frequency was scanned to diagnose the response of the plasma (specifically JPN 42870).

Here, we briefly summarize the main results of their study: In limiter configuration, two resonant modes ($n = 1$ TAEs) were excited and identified with distinct “low” and “high” frequencies within the simulated frequency scan, $\Delta f \approx 100 - 150$ kHz. The low- f mode was found to be more stable - i.e. having a greater absolute damping rate - than the high- f mode. The damping of both modes increased as the simulated plasma boundary approached the separatrix, i.e. becoming more X-point-like. Then, the low- f mode became unidentifiable as a resonance, or “disappeared,” in X-point configuration, indicating an enhancement of continuum damping with the changing magnetic geometry.

In addition, the kinetic energy of each mode was observed to decrease in two ways: (i) as the plasma transitioned from limiter to X-point, and (ii) with increasing PA separation. Importantly, however, the computed damping rate did not change with PA separation for a given magnetic configuration. These results indicate a decrease in PA coupling which led to less (or no) antenna power absorbed by the mode, but otherwise had no impact on the inherent mode damping.

Our goals in the following sections are to identify both low- f and high- f stable AEs in the frequency scan of the AE antenna, assess the dependence of measured resonance parameters on PA separation, and monitor the evolution of AEs through a transition from limiter to X-point configuration, thereby further validating the modeling in [40].

3. Plasma-antenna separation

We begin by studying the effect of PA separation on PA coupling and measured AE parameters. As mentioned in Section 1, the data in the following sections include a wide range of plasma-*sensor* separations. However, because the fourteen magnetic probes are located at various poloidal (and toroidal) positions, and not all probes measure each resonance, plasma-*sensor* separation is not studied specifically.

3.1. Experimental study of plasma-antenna separation

During the 2019-2020 JET deuterium campaign, approximately 5000 resonances were excited by the AE antenna in almost 500 plasmas [34]. Three of these (limiter) plasmas - JPN 96585, 96587, and 96588 - comprised a dedicated study of PA separation, here defined as the

minimum distance between the AE antenna ($R \approx 3.68$ m, $Z \approx -0.65$ m) and last closed flux surface from EFIT [45]. However, before turning to these specific pulses, we first investigate trends in the bulk data. § Figure 1a shows the probability of resonance detection as a function of PA separation. This histogram (with all bin heights summing to one) is calculated as the ratio of the number of resonances detected within each bin to the number of times the AE antenna operated within the same range. || In general, the detection probability decreases as the PA separation increases.

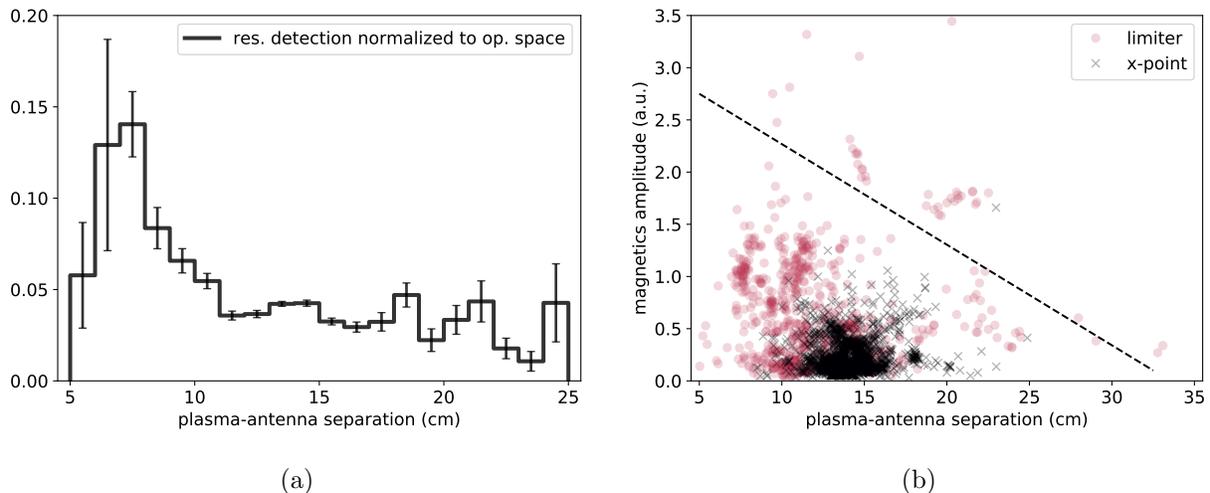


Figure 1: (a) A histogram of the probability of resonance detection (normalized to the operational space) versus plasma-antenna (PA) separation, with the total number of resonances $N_{\text{tot}} = 3408$. Uncertainties are shown as error bars. (b) Magnetic resonance amplitudes (the sum of all probes) versus PA separation for both limiter ($N_{\text{tot}} = 837$) and X-point ($N_{\text{tot}} = 2356$) configurations. The dashed line represents an approximate upper bound. These data were collected during no external heating (NBI or ICRH). Note the different horizontal axes.

The “total” amplitude of the detected resonance, calculated as the sum of all fast magnetic probe amplitudes at the time of the resonant frequency $\omega = \omega_0$ and normalized to the antenna current, is plotted versus PA separation in Fig. 1b. Data are split into resonances detected during limiter (light circles) and X-point (dark crosses) configurations. The PA separation during X-point is usually $d \geq 10$ cm, while that during limiter configuration spans a wider range. We see a general trend of the maximum amplitude decreasing with PA separation. An approximate upper bound is shown in Fig. 1b as a dashed line, with $\sim 99\%$ of data falling below it. The results of Figs. 1a and 1b are consistent with the computational results [40] mentioned in the previous section: the antenna coupling efficiency and antenna-driven mode energy both decrease as PA separation increases.

§ Data collected during external heating (NBI and/or ICRH) are excluded in this work so that EP effects can be neglected.

|| See [34] for details regarding the calculations of the probability of resonance detection, damping rate, and toroidal mode number.

Plasma parameters for the three ohmically heated discharges of this dedicated study are shown in Fig. 2a. Flattop values are $B_0 = 3$ T, $I_p = 1.7$ MA, $q_0 \approx 1$, $q_{95} \approx 3.3 - 3.5$, $n_{e0} \approx 3.8 \times 10^{19} \text{ m}^{-3}$, and $T_{e0} \approx 1.5$ keV; thus, the nominal TAE gap frequency is $f_{\text{TAE}} = v_A/(4\pi qR) \approx 240$ kHz. Since no external heating is applied, the plasma rotation is expected to be low and is thus neglected. There is good reproducibility among the three plasmas, with the exception of the timing of the plasma current ramp-down. The plasma boundary and magnetic axis, from EFIT, for these limiter pulses are shown at $t = 10$ s in Fig. 2b. Also plotted are the approximate location, orientation, and dimensions of the AE antenna (AEAD), as well as the poloidal position of a representative fast magnetic probe. Discharges JPN 96585 and 96587 were maintained with a PA separation $d \approx 15$ cm; then the separation was decreased to $d \approx 10$ cm in JPN 96588 by lowering the vertical position. Time traces of PA separation are shown in Fig. 3.

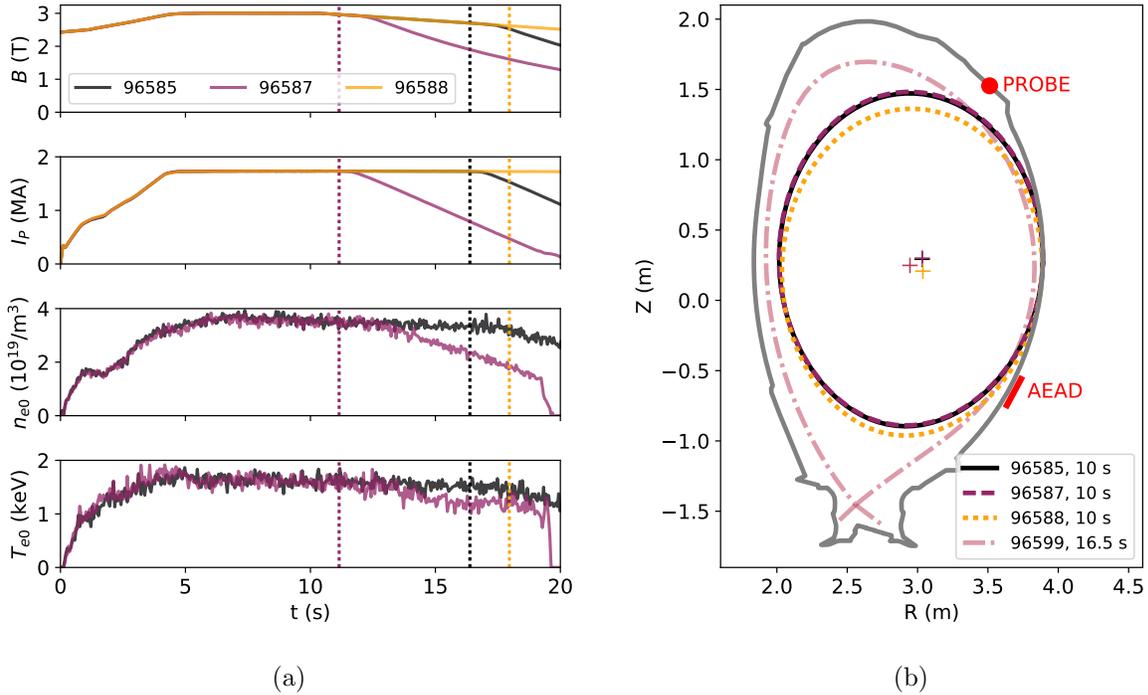


Figure 2: (a) Plasma parameters for JPN 96585, 96587, and 96588: the toroidal magnetic field, plasma current, and on-axis electron density and temperature. Vertical (dotted) lines indicate the end of AE antenna operation. Note that there were no Thomson Scattering data for 96588. (b) A poloidal cross-section of the JET vacuum vessel with plasma boundaries and magnetic axes (+) from EFIT [45] and locations of the AE antenna (AEAD) and a representative fast magnetic probe. An X-point configuration is also shown for JPN 96599; see Section 4 and Fig. 7.

During these discharges, antennas 1-5 were driven with the same phase. Therefore, power was injected into primarily *even* toroidal mode numbers, with a power spectrum peaked at $n = 0$ and decaying for $n = \pm 2, \pm 4, \dots$ and so on; power in odd mode numbers was ~ 3 times less. The antenna frequency was scanned from $\Delta f = 125 - 240$ kHz in JPN 96585 and

$\Delta f = 160 - 240$ kHz in JPN 96587 and 96588, as indicated by the triangular waveforms (dashed lines) in Fig. 3. Two stable AEs were consistently detected within this scan throughout the three discharges: a high- f mode with resonant frequency $f_0 \approx 230 - 240$ kHz and low- f mode with $f_0 \approx 170 - 180$ kHz, distinguished as circles and triangles, respectively. As expected, the mode frequency does not change with PA separation.

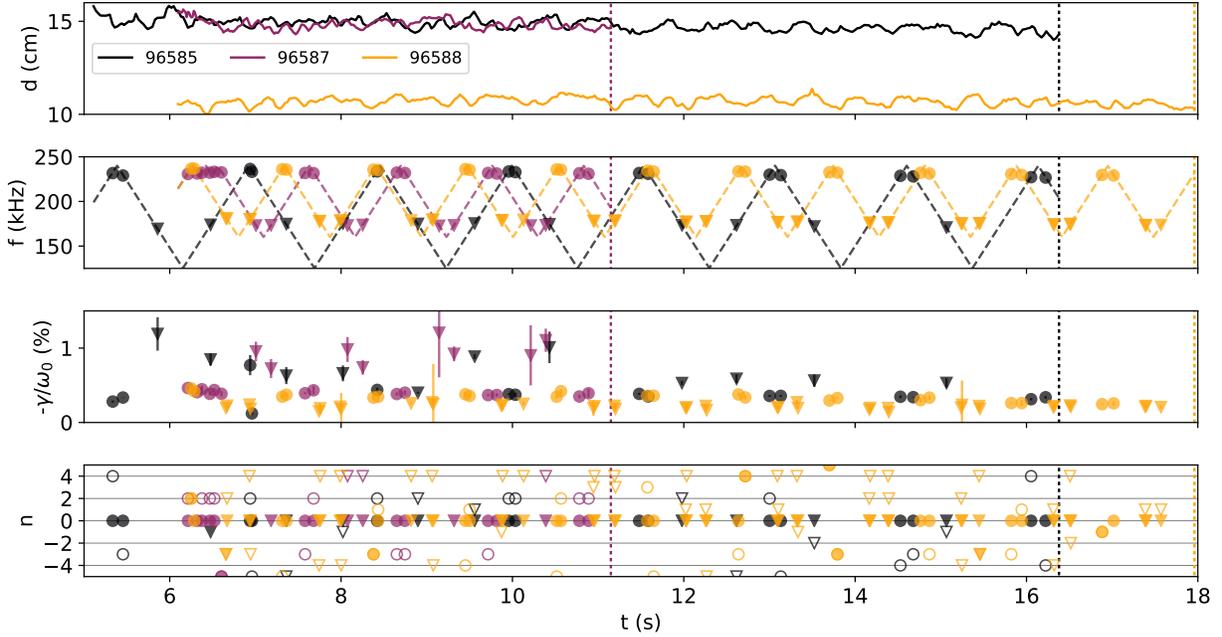


Figure 3: Plasma-antenna separation and measurements of magnetic resonances for JPN 96585, 96587, and 96588: antenna (dashed) and resonant frequencies, normalized damping rate, and estimated toroidal mode number. High/low frequency resonances are distinguished as circles/triangles. Filled/open symbols are toroidal mode number estimates including/excluding $n = 0$. Vertical (dotted) lines indicate the end of antenna operation.

The normalized damping rates γ/ω_0 for both high- f and low- f modes are also shown in Fig. 3. The damping rate for the high- f mode (circles) is consistently $-\gamma_{\text{high}}/\omega_0 \approx 0.4\%$ throughout the three discharges and does not vary with PA separation. This result agrees with the simulations in [40]. Interestingly, there is a wider range of the measured damping rate of the low- f mode, $-\gamma_{\text{low}}/\omega_0 \approx 0.2\% - 1.2\%$. For a PA separation $d \approx 15$ cm, the low- f mode is more stable than the high- f mode, i.e. $|\gamma_{\text{high}}| < |\gamma_{\text{low}}|$, which agrees with the findings of [40]; however, for $d \approx 10$ cm, it is the opposite: $|\gamma_{\text{low}}| < |\gamma_{\text{high}}|$. Thus, the damping rate appears to increase with PA separation for the low- f mode; this agrees with the experimental results from C-Mod, but not the simulations from [40].

This variation in γ_{low} could be explained, in part, by the slightly different edge conditions for the plasmas with two PA separations: $q_{95} \approx 3.3$ and 3.45 for $d \approx 10$ cm and 15 cm, respectively. In [34], the damping rate was found to increase with q_{95} for data in the same stable AE database described above, consistent with enhanced continuum damping. As will

be discussed in the next section, this could more strongly affect the low- f mode due to its localization in the outer plasma region, whereas the high- f mode has a more global structure. Yet, it is difficult to say whether this alone could account for the wide range $\Delta(\gamma_{\text{low}}/\omega_0) \approx 1\%$, and the kinetic modeling required to accurately assess the damping rate is beyond the scope of the present study.

The toroidal mode number of each resonance is estimated via two complementary methods: (i) a weighted chi-square spectrum comparing the toroidal locations of the magnetic probes and phase angles of the magnetic signals, and (ii) sparse spectral decomposition with the SparSpec algorithm [20].^{||} Because both methods typically agree, we only include the chi-square results in this paper. The best estimates of n (i.e. global minima of the chi-square spectra) are shown in Fig. 3 as solid symbols, limited to the range $|n| \leq 5$. For almost all high- f and low- f resonances, $n = 0$ is estimated which could indicate that these are Global AEs (GAEs). The best $n \neq 0$ estimates (i.e. the minima of the chi-square spectra *excluding* $n = 0$) are shown as open symbols. As expected, these often have even values, e.g. $|n| = 2$ and 4, due to the dominantly even n -spectrum driven by the AE antenna. As will be discussed in the next section, MHD simulations indicate that the high- f mode is an $n = 0$ GAE, while the low- f mode is likely an $n = 2$ TAE.

Here, it is important to note that the plasma shape was kept fixed in these experiments; therefore, decreasing the PA separation actually *increased* the distance between the antenna and (some) fast magnetic probes (see Fig. 2b). While we improved PA coupling and the excitation of AEs by decreasing PA separation, the detection of AEs, in principle, became more difficult. This could have been avoided by increasing the plasma elongation; however, that could have affected PA coupling (and general plasma performance) in turn. This presents an interesting optimization problem, the solution to which will be pursued in upcoming JET EP experiments [41] in preparation for the DT campaign.

3.2. Computational analysis of plasma-antenna separation

A suite of MHD codes is used to analyze the JET plasmas of the previous section and the next. First, the magnetic geometry from EFIT[¶] [45] is converted into the appropriate format, via HELENA [46], to compute the Alfvén continuum with CSCAS [47] with no sound wave coupling included. Here, an even, eighth-order polynomial is fit to the electron density profile, and $n_i = n_e$ is assumed for the ion density. For example, the fitted density and safety factor profiles for JPN 96585 at $t = 10$ s are plotted in Fig. 4a as a function of the square root of the normalized poloidal flux, $s = \sqrt{\psi_N}$, not to be confused with the magnetic shear discussed in the next section.

Next, the linear resistive MHD code CASTOR [42, 43] is run with the external antenna module enabled. With the plasma boundary at $s = 1$, the locations of the antenna and wall are $s_{\text{ant}} = 1.1$ (unless otherwise noted) and $s_{\text{wall}} = 1.2$, respectively. For a given toroidal

[¶] Magnetic geometries constrained by pressure (EFTP) and polarimetry (EFTF) are also available, but results are found to agree best with EFIT. Relative differences among them are typically of order 10%.

mode number n , a range of antenna frequencies is “scanned”; at each, the AE mode structure and absorbed power are computed. Due to computational constraints, the maximum number of plasma and antenna harmonics simulated is $M = 7$, and number of vacuum harmonics is $M' = 9$. In addition, the same normalized resistivity $\hat{\eta} = \eta/(\mu_0 v_A R_0) = 1.6 \times 10^{-9}$ is used for the following simulations. For the plasmas of this section and the next, this corresponds to a resistivity $\eta \approx 5 \times 10^{-8} \Omega\text{m}$. As will be discussed, the plasma response is relatively insensitive to the choice of $\hat{\eta}$.

We focus first on the high- f , $n = 0$ mode observed in JPN 96585, 96587, and 96588. Because it was measured consistently throughout the three discharges, we simulate JPN 96585 at $t = 10$ s as a representative time slice. Results for $n = 0$ are shown in Fig. 4. The Alfvén continua from CSCAS (dark crosses in Fig. 4b) have minima near the edge, $s \approx 1$. Here, an $n = 0$ GAE exists having an eigenvalue $\omega_0 R_0/v_A = 0.532$ ($f_0 \approx 211$ kHz) and exhibiting strong coupling of poloidal harmonics $m = \pm 1$ [48]. This eigenfrequency is lower than the experimentally observed frequency $f_0 \approx 235$ kHz, but agrees within uncertainties ($\lesssim 10\%$) of the central safety factor q_0 .

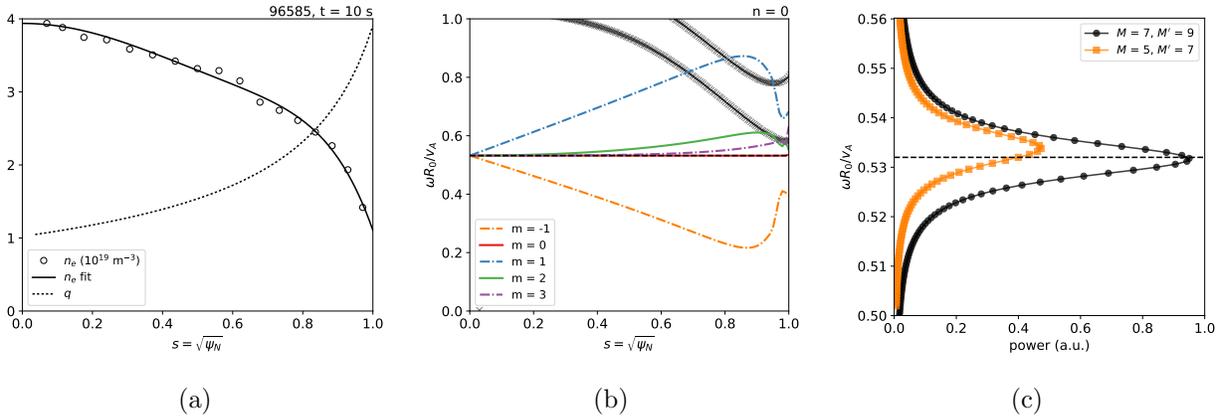


Figure 4: (a) Density and safety factor profiles for JPN 96585 at $t = 10$ s. (b) Alfvén continua (crosses) from CSCAS overlaid with the real part of velocity perturbation (solid, dot-dashed) from CASTOR for $n = 0$, $m = -1$ to 3, and eigenvalue $\omega_0 R_0/v_A = 0.532$ (dashed). (c) Power absorbed versus frequency from CASTOR for two simulation “domain” sizes, with M and M' the number of poloidal harmonics of the plasma/antenna and of the vacuum, respectively. Note the different horizontal and vertical axes.

The power absorbed by this $n = 0$ GAE, as calculated from CASTOR⁺, is seen in Fig. 4c and has the characteristic bell-shape of a driven, weakly damped resonance. The mode structure shown in Fig. 4b is that from the peak of the absorbed power. Though not shown in Fig. 4c, no other $n = 0$ GAE resonance is found within the full frequency range of the AE antenna, i.e. $\omega_0 R_0/v_A \in [0.3, 0.6]$. In addition, a CASTOR simulation with reduced numbers of poloidal harmonics ($M = 5$ and $M' = 7$) finds the same mode, although with

⁺ CASTOR was recently updated by the authors to allow the toroidal mode number $n = 0$, which caused divergences in previous versions.

the peak of power absorption offset by only $\Delta(\omega_0 R_0/v_A) \approx 0.01$. When normalized to their respective maximum powers and translated vertically, the two curves in Fig. 4c overlay almost exactly, giving us confidence in the converged solution.

While it is tempting to compute a damping rate from the absorbed power to compare with experiment, we must be cautious for two reasons: (i) the 3D AE antenna geometry and resulting drive are not fully modeled here (as they were in [40]), and (ii) CASTOR does not include all sources of damping, e.g. radiative or Landau damping. Nevertheless, we see that the half width at half maximum (HWHM, $\sim \gamma/\omega_0$) is $\sim 1\%$ which is at least the right order of magnitude and likely indicates a predominance of continuum damping.

Because no low- f mode was found in the above CASTOR scan for $n = 0$, we instead investigate $n = 2$ for the experimentally measured low- f AE. An open $n = 2$ TAE gap is seen in the CSCAS results of Fig. 5b around $\omega_0 R_0/v_A \approx 0.4$. As seen in Fig. 5c, a frequency scan in CASTOR finds a clear resonance with peak at $\omega_0 R_0/v_A = 0.419$ ($f_0 \approx 166$ kHz). This eigenfrequency agrees well with the experimentally observed resonant frequency $f_0 \approx 175$ kHz. We also note that no high- f , $n = 2$ mode is found within the frequency scan of CASTOR.

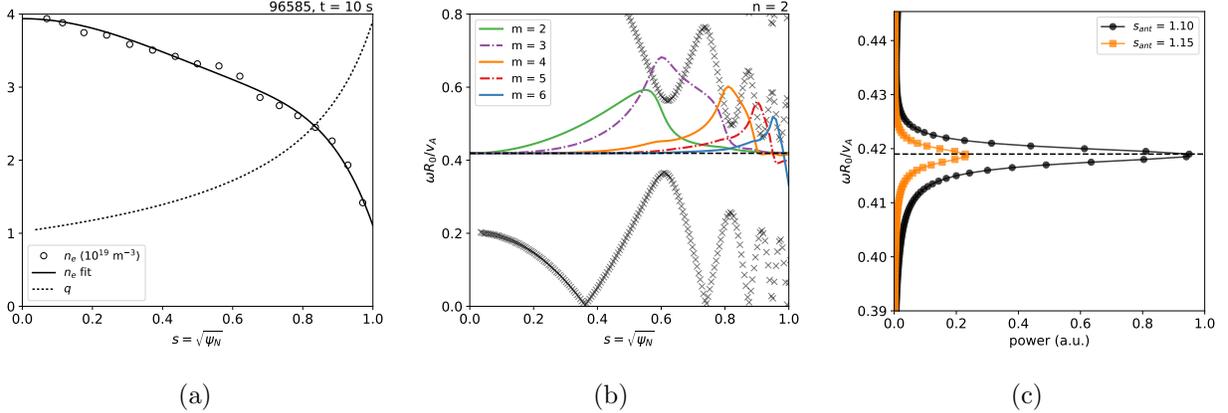


Figure 5: (a) Density and safety factor profiles for JPN 96585 at $t = 10$ s (same as Fig. 4a). (b) Alfvén continua (crosses) from CSCAS overlaid with the real part of velocity perturbation (solid, dot-dashed) from CASTOR for $n = 2$, $m = 2$ to 6, and eigenvalue $\omega_0 R_0/v_A = 0.419$ (dashed). (c) Power absorbed versus frequency from CASTOR for two plasma-antenna separations, with antenna radial positions $s_{\text{ant}} = 1.10$ and 1.15. Note the different horizontal and vertical axes.

The resonant mode structure, shown in Fig. 5b, indicates that this is an $n = 2$ TAE [49] with strongest coupling between the poloidal harmonics $m = 2, 3$ at $s \approx 0.6$ and $m = 3, 4$ at $s \approx 0.8$. Note also in Fig. 5c that another frequency scan was performed with the antenna moved farther away from the plasma, to $s_{\text{ant}} = 1.15$. As expected, the same resonance is identified, but the absorbed power decreases due to the increased PA separation. Though not shown, when normalized to their respective maximum powers, the two curves match exactly, indicating that mode damping is independent of PA separation in CASTOR. Simulations were also performed for JPN 96587 and 96588. While their frequency scans (not shown)

indicate some variation due to the slight differences in plasma parameters, their HWHM values agree within expected uncertainties. Thus, it is difficult to conclude what causes the trend of increasing γ_{low} with PA separation using CASTOR alone.

The simulation results of this section indicate that two AEs, with distinct low and high frequencies, can be detected by the frequency scan of an external antenna in JET plasmas, in agreement with the computational studies in [40]. For these particular discharges, the experimentally measured high- f mode is consistent with an $n = 0$ GAE, and the low- f mode with an $n = 2$ TAE. However, we note that these are not necessarily unique solutions. As current computational constraints limit our modeling of toroidal mode numbers to $n \leq 2$, a more exhaustive study of higher mode numbers is left for future work.

4. Magnetic configuration: limiter versus X-point

In this section, we consider the impact of the magnetic configuration (limiter versus X-point) on PA coupling and measured AE parameters.

4.1. Experimental study of limiter versus X-point configuration

Utilizing the same database from [34], we provide a breakdown of AE antenna operation and resonance detection in Table 1 for both limiter and X-point magnetic configurations. Because most JET experiments require diverted plasmas, the AE antenna was operated far less often in limiter compared to X-point configuration: 12% compared to 88% of the time. Naturally, the fraction of resonances detected in limiter plasmas (18%) is also less than that for X-point plasmas (82%). However, the *probability* of resonance detection is greater in limiter (62%) compared to X-point configuration (38%). This is consistent with the simulation results of [40] which indicated reduced PA coupling in X-point, as discussed in Section 2.2. We also note that PA separation is a conflating factor since it is typically greater for X-point compared to limiter plasmas (see Fig. 1a).

Table 1: Breakdown of AE antenna operation, resonance detection ($N_{\text{tot}} = 4768$), and detection probability in limiter versus X-point magnetic configurations, rounded to the nearest percentage. See [34] for further details of the calculation of detection probability.

Magnetic configuration	Operational space	Resonance detection	Detection probability
limiter	12%	18%	62%
X-point	88%	82%	38%

Figure 6a shows the measured AE damping rate as a function of the edge magnetic shear, $s_{95} = (r/q)(dq/dr)|_{q=q_{95}}$, for resonances detected in X-point configuration and during times with no external heating (NBI or ICRH). Though not shown, no clear trend is observed in the limiter data; this could be due to a variety of reasons including the wide range of

plasma parameters in the parameter space or perhaps more core-localized modes. For X-point data, however, a strong increase in the damping rate is seen for $s_{95} > 5$. The data are well-correlated, having a weighted, linear correlation coefficient of 0.675. This trend likely indicates a predominance of edge-localized AEs and increased continuum damping [50–52] at the edge, which is consistent with a similar trend of $|\gamma/\omega_0|$ increasing with q_{95} , reported in [34]. The nonlinear, almost parabolic shape could also indicate some contribution from radiative damping, as discussed in [1, 53] among others.

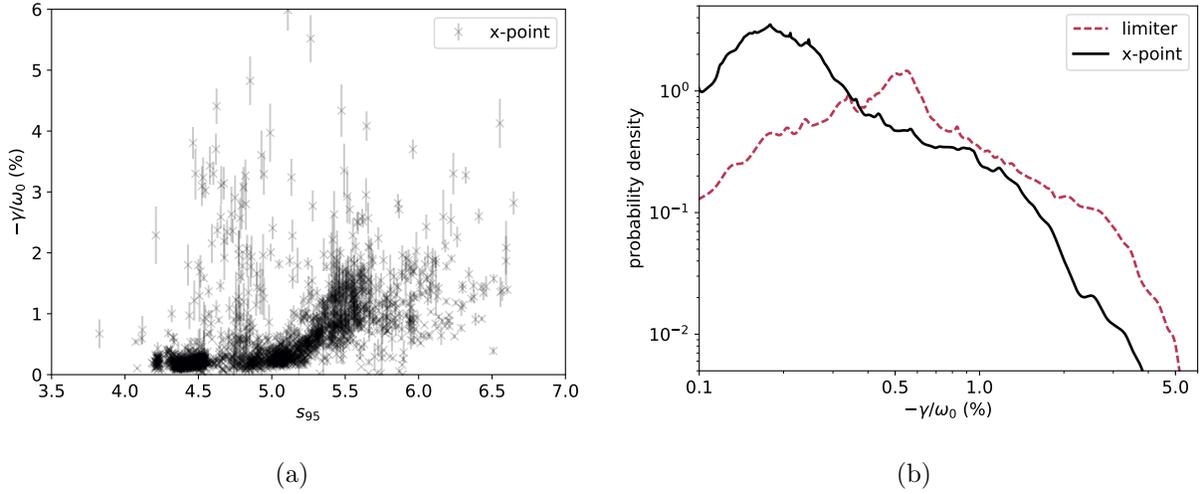


Figure 6: (a) Normalized damping rate versus edge magnetic shear in X-point configuration ($N_{\text{tot}} = 2503$). (b) Probability density functions of the normalized damping rate for limiter ($N_{\text{tot}} = 786$) and X-point ($N_{\text{tot}} = 2503$) configurations. These data were collected during no external heating (NBI or ICRH). Note the linear and logarithmic axes.

The distributions of damping rates for limiter and X-point geometries, including the data of Fig. 6a, are shown in the probability density functions* (pdfs) of Fig. 6b. Again, none of the data was collected during external heating. The pdf of limiter data is peaked at $-\gamma/\omega_0 \approx 0.5\%$, while that for X-point data is peaked at $-\gamma/\omega_0 \approx 0.2\%$; both pdfs exponentially decay away from the peak. This can also be seen in the density of data points of Fig. 6a. Thus, “low” damping rates (i.e. $-\gamma/\omega_0 < 0.4\%$) are actually observed more often in X-point than in limiter configuration. This agrees with the findings from Alcator C-Mod discussed in Section 2.1. Yet this result comes from a collection of all *observations* of AE resonances, which are oftentimes independent, and does not necessarily indicate the dependence of AE stability during a limiter-to-X-point transition, which is pursued next. That is to say, there could be other conflating factors - such as varying plasma parameters - contributing to the difference in pdfs.

* An individual measurement is assumed to have a Gaussian pdf with mean equal to the measured damping rate γ/ω_0 and standard deviation equal to the associated uncertainty $\Delta(\gamma/\omega_0)$. The total pdf is then the normalized sum of all individual pdfs. See [34] for further details.

Two ohmically heated JET plasmas, JPN 96599 and 96600, were part of a dedicated study of PA coupling in different magnetic geometries. Their plasma parameters are shown in Fig. 7, with vertical lines (dotted) indicating transitions in the magnetic configuration: First, the plasma transitions from being limited on the outer limiter (low-field side) to the inner limiter (high-field side) at $t \approx 10$ s, and then from (inner) limiter to X-point configuration at $t \approx 12$ s. Some parameters remain relatively constant during these transitions, including the toroidal field $B_0 = 3$ T, plasma current $I_p = 1.8$ MA, and on-axis safety factor $q_0 \approx 1$. Other quantities fluctuate, like the electron density n_{e0} and temperature T_{e0} along with the PA separation d (and plasma-sensor separations, though not shown). As expected, the edge safety factor q_{95} , edge shear s_{95} , elongation κ , and triangularity δ all increase during the limiter-to-X-point transition. Good reproducibility is seen for the two pulses.

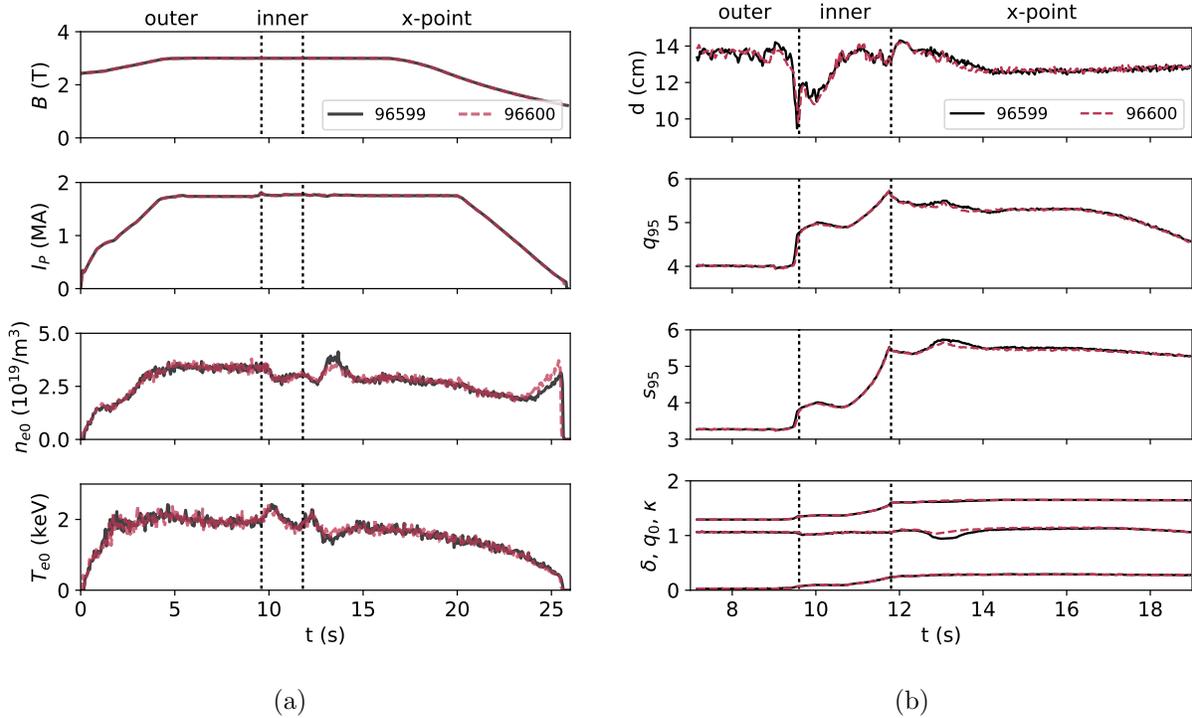


Figure 7: Plasma parameters for JPN 96599 and 96600: (a) the toroidal magnetic field, plasma current, and on-axis electron density and temperature, and (b) plasma-antenna separation, edge safety factor, edge magnetic shear, elongation, central safety factor, and average of upper and lower triangularity. Vertical (dotted) lines separate magnetic configurations: outer limiter, inner limiter, and X-point.

The AE antenna was operated during all three phases of the two discharges ($t = 7-19$ s), and resonance measurements are shown in Fig. 8. Unlike the antenna setup in Section 3.1, only antennas 1-4 were powered here (i.e. those in one toroidal octant); thus, power was injected broadly into both even and odd modes, with similar magnitudes for $|n| \leq 3$. The antenna frequency was scanned throughout the range $\Delta f = 125 - 240$ kHz in JPN 96599, while real-time mode tracking was employed in JPN 96600. As seen in Fig. 8, the measured

resonant frequencies, damping rates, and toroidal mode numbers agree well for both pulses.

In JPN 96599, both high- f (circles) and low- f (triangles) AEs are measured during the outer limiter phase at frequencies $f_0 \approx 225$ kHz and 150 kHz, respectively. Yet, during the transition to inner limiter and then X-point geometry, the low- f mode is no longer detected. In the inner limiter phase, as the high- f mode drops in frequency, it could be that the low- f mode frequency is below the antenna's range, i.e. $f_0 < 125$ kHz. While this could still be the case during X-point, the high- f mode frequency has regained a frequency $f_0 > 200$ kHz, and the low- f mode is still not detected. Assuming that the low- f mode is within the antenna's frequency range, the disappearance of this mode is consistent with the JOREK simulation results of [40], as discussed in Section 2.2, in which the low- f mode damping grew too strongly. Also note that the PA separation actually decreases from $d \approx 14$ cm to 12 cm from outer limiter to X-point configuration (see Fig. 7b), although the improvement in resonance detection is marginal (see Fig. 1a).

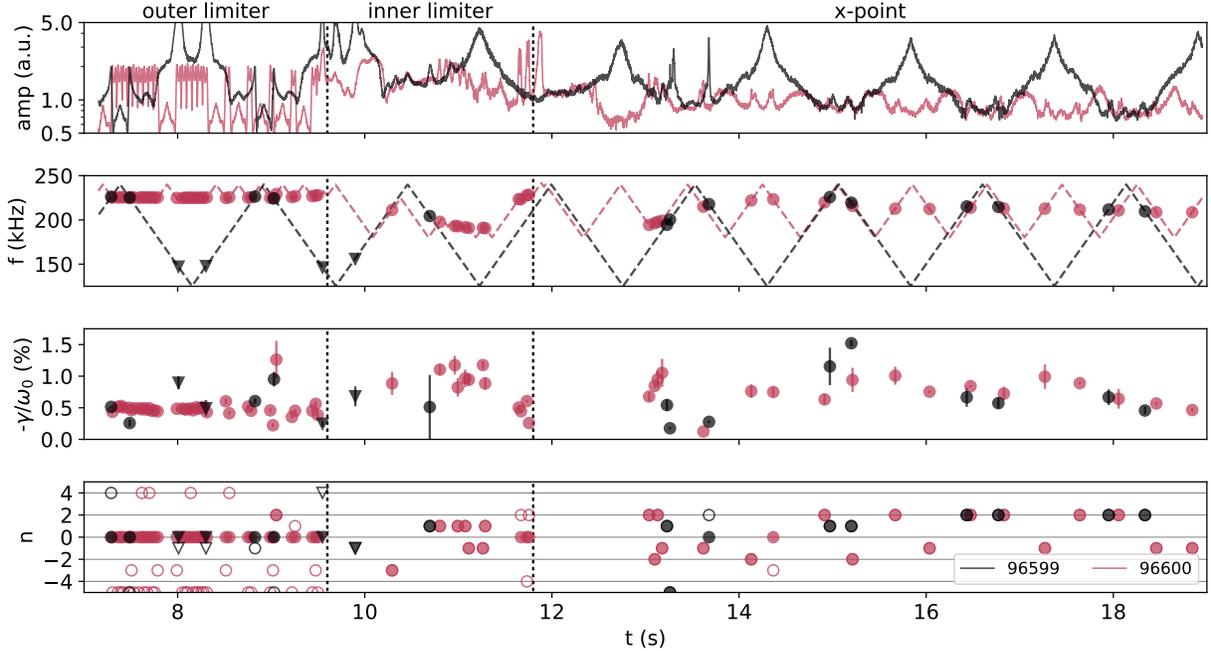


Figure 8: Measurements of magnetic resonances for JPN 96599 and 96600: the sum of all probe amplitudes, antenna (dashed) and resonant frequencies, normalized damping rate, and estimated toroidal mode number. High/low frequency resonances are distinguished as circles/triangles. Filled/open symbols are toroidal mode number estimates including/excluding $n = 0$. Vertical (dotted) lines separate magnetic configurations: outer limiter, inner limiter, and X-point.

In JPN 96600, the high- f mode is tracked consistently throughout the outer limiter phase and somewhat during the inner limiter phase, but tracking is more difficult during X-point. The magnetics data provide an explanation: As seen in Fig. 8, the sharp peaks in the signal amplitude, corresponding to AE resonances, are easily identifiable in the outer limiter phase, but become less distinguishable during the inner limiter phase as the plasma

become more like X-point. In X-point, the high- f resonances are no longer high-amplitude, sharp peaks, but low-amplitude, broad “bumps.” These are still identifiable as resonances when including phase information, which is not shown here. The decrease in mode amplitude, as measured by the fast magnetics, is also consistent with a decrease in mode energy when comparing limiter to X-point plasmas, as found in [40].

During the outer limiter phase, the damping rate is consistently $-\gamma/\omega_0 \approx 0.5\%$, which then increases during the inner limiter phase to $-\gamma/\omega_0 \approx 1\%$, likely due to the increasing edge magnetic shear (see Fig. 7b). There is an exception of some low damping rates ($-\gamma/\omega_0 < 0.5\%$) for resonances measured just before the transition from inner limiter to X-point configuration ($t \approx 12$ s). This appears to be a marginally stable, high- f mode somehow destabilized by the change in magnetic geometry, but its explanation is beyond the scope of this paper. While there are some resonances measured with low damping rates in X-point, a majority have $-\gamma/\omega_0 > 0.5\%$, consistent with increased damping of AEs during a transition from limiter to X-point configuration. Furthermore, while plasma parameters are relatively constant during AE antenna measurements (see Fig. 7), a slight decrease is observed in n_e, T_e, q_{95} and s_{95} beyond $t > 16$ s; the concurrent reduction in the damping rate could therefore be explained by a decrease in collisional, Landau, and/or continuum damping.

The best estimates of the toroidal mode number - including (filled) and excluding (open) $n = 0$ - are also shown in Fig. 8. The high- f mode, measured during the outer limiter phase, appears to be a similar $n = 0$ GAE found in the limiter plasmas of Section 3.1. During the inner limiter phase, the AEs are measured to have $|n| = 1$. As mentioned, this is due to the broad power spectrum from only one octant of the AE antenna system. The measurement is confirmed by mode analysis of magnetic spectrograms, though they are not shown here. The simulations of the next section will also indicate that these are likely $|n| = 1$ AEs. Finally, after the transition to X-point, there is a wider range of estimated mode numbers $|n| \leq 2$. We will explore a single $n = 2$ AE at $t \approx 16.5$ s, but it is possible that the AE antenna resonates with a superposition of low- n modes.

4.2. Computational analysis of limiter versus X-point configuration

The same suite of MHD codes described in Section 3.2 is now applied to the two pulses of the previous section. We forgo the analysis of the outer limiter phase due to the similarities with the analyses of the limiter plasmas in Section 3.2. Instead, we focus on the inner limiter phase, during which the plasma is becoming more “X-point-like,” and then after the transition to X-point.

We begin by modeling JPN 96599 at $t = 11$ s in search of a $|n| = 1$ AE resonance at the experimentally measured frequency $f_0 \approx 200$ kHz. The fitted electron density and safety factor profiles for this time are shown in Fig. 9a. We see that the edge $q(s = 1)$ has increased significantly compared to the limiter pulses (see Fig. 5a). The $n = 1$ TAE gap, computed by CSCAS and shown in Fig. 9b, is closed at the edge, so no clear resonance is found in

the scan over low frequencies with CASTOR. Instead, a resonance is observed in the edge of the Ellipticity-induced AE (EAE) gap with peak power absorbed at $\omega_0 R_0/v_A = 0.455$ ($f_0 \approx 197$ kHz) and perhaps strongest coupling between poloidal harmonics $m = 3, 5$ at $s \approx 0.9$. Here, the eigenfrequency agrees well with the experimentally measured frequency.

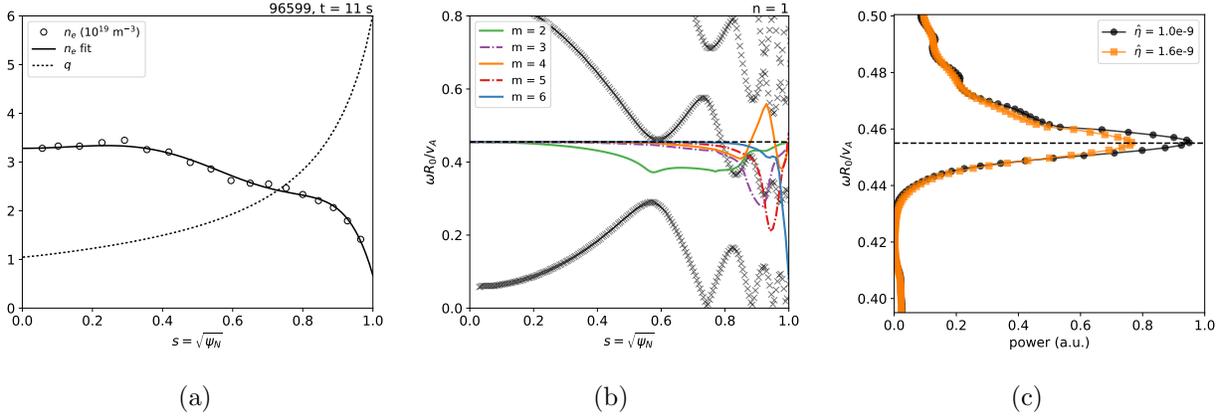


Figure 9: (a) Density and safety factor profiles for JPN 96599 at $t = 11$ s (limiter configuration). (b) Alfvén continua (crosses) from CSCAS overlaid with the real part of velocity perturbation (solid, dot-dashed) from CASTOR for $n = 1$, $m = 2$ to 6, and eigenvalue $\omega_0 R_0/v_A = 0.455$ (dashed). (c) Power absorbed versus frequency from CASTOR for two normalized resistivities $\hat{\eta} = 1.0 \times 10^{-9}$ and 1.6×10^{-9} . Note the different horizontal and vertical axes.

To highlight the relative insensitivity our CASTOR results to the normalized resistivity $\hat{\eta}$, two frequency scans are performed with $\hat{\eta} = 1.0 \times 10^{-9}$ and 1.6×10^{-9} (the default value). As seen in Fig. 9c, the same resonant peak is found for both $\hat{\eta}$ values. In addition, though not shown here, both curves overlap almost exactly when normalized to their respective maximum powers.

Next, we model the $n = 2$ AE observed during X-point, specifically in JPN 96599 at $t = 16.5$ s. Safety factor and density profiles are shown in Fig. 10a. The strong shear at the plasma edge introduces some complications in the modeling. For instance, CSCAS could only be simulated within $s \in [0, 0.9]$, as seen in the continua in Fig. 10b. As with the $n = 1$ TAE gap in Fig. 9b, the $n = 2$ TAE gap is closed, and instead a more highly damped mode is found in the edge of the EAE gap, here with strongest coupling between poloidal harmonics $m = 4, 6$ near $s \approx 0.8$. The frequency scan in CASTOR finds a resonant peak at $\omega_0 R_0/v_A = 0.570$ ($f_0 \approx 252$ kHz). This is higher than the experimentally measured resonant frequency $f_0 \approx 215$ kHz, but only by $\sim 17\%$ which is allowable within uncertainties of the density and safety factor profiles. Furthermore, better agreement would likely be attained with improved modeling of the edge plasma and scrape-off layer, which then requires a more computationally intensive code like JOEAK.

‡ Although an $n = 0$ GAE was observed during the outer limiter phase of JPN 96599 and 96600, CASTOR simulations found no $n = 0$ resonance during X-point at $t = 16.5$ s.

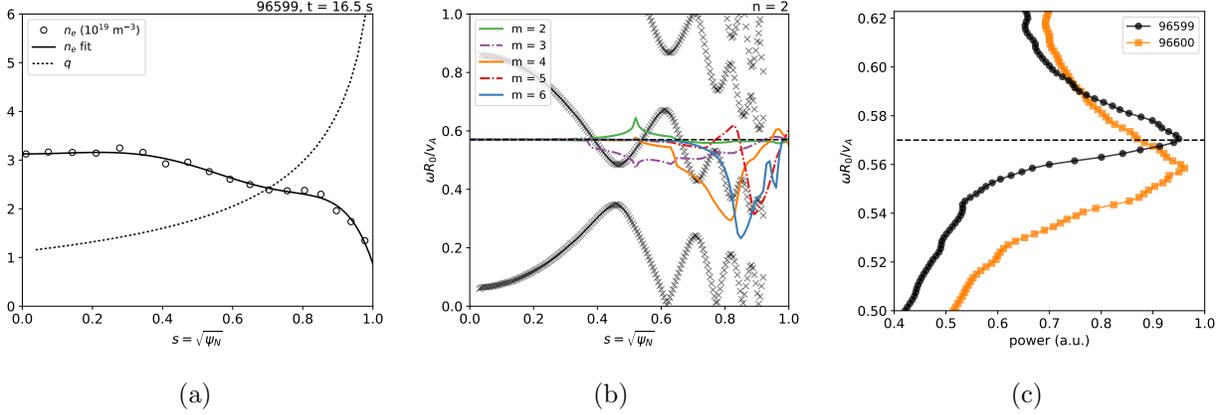


Figure 10: (a) Density and safety factor profiles for JPN 96599 at $t = 16.5 \text{ s}$ (X-point configuration). (b) Alfvén continua (crosses) from CSCAS overlaid with the real part of velocity perturbation (solid, dot-dashed) from CASTOR for $n = 2$, $m = 2$ to 6, and eigenvalue $\omega_0 R_0/v_A = 0.570$ (dashed). (c) Power absorbed versus frequency from CASTOR for JPN 96599 and 96600 (also at $t = 16.5 \text{ s}$). Note the different horizontal and vertical axes and limits.

We repeat the simulations for JPN 96600, also at $t = 16.5 \text{ s}$. Only the frequency scan in CASTOR is shown in Fig. 10c, which shows good agreement with the scan in JPN 96599. Both have similar maximum absorbed powers, but there is a slight offset of $\Delta(\omega_0 R_0/v_A) \approx 0.01$. Note that the HWHM of JPN 96600 is slightly wider than that of JPN 96599, indicating some variation or uncertainty in the damping rate. Yet, compared to the CASTOR scans of other modes (see Figs. 4c, 5c and 9c), the resonance width is greater, which is consistent with an increase in damping rate for a plasma transitioning from limiter to X-point configuration.

5. Summary

In this work, we reported on a dedicated study of plasma-antenna (PA) coupling between JET plasmas and the Alfvén Eigenmode Active Diagnostic, or AE antenna. The resonant excitation of stable AEs - and measurements of their frequencies f_0 , damping rates γ , and toroidal mode numbers n - were monitored while scanning the PA separation and varying the magnetic configuration (limiter versus X-point). These experiments were motivated by similar studies carried out previously in Alcator C-Mod and in JET with the old AE antenna system, as well as by recent computational efforts by Dvornova *et al* [40] to interpret past data.

In the first part of the study, we assessed the impact of PA separation on AE antenna coupling, stable AE excitation, and AE stability itself. From a database of almost 5000 AE resonances, it was found that two quantities decreased as PA separation increased: the probability of resonance detection (see Fig. 1a) and the magnetic amplitude of the detected resonance (see Fig. 1b). Both results are consistent with the conclusions of [40]: increasing PA

separation reduces PA coupling and leads to lower detected AE amplitudes as the antenna's magnetic perturbation decreases with distance and less power is absorbed by the mode. It is important to note here that conflating factors, e.g. varying magnetic and thermal plasma parameters, introduce uncertainties and scatter into the analysis of bulk data, yet general trends are still observed and can then be compared with our dedicated experiments.

Three ohmic limiter plasmas were reproduced to investigate the effect of PA separation in more detail (see Fig. 2): two with PA separations $d = 15$ cm, and the other with $d = 10$ cm (see Fig. 3). Two stable AEs at distinct low and high frequencies were detected within the AE antenna frequency scan, as was found in the CASTOR and JOREK simulations of [40]. The resonant frequencies (and estimated toroidal mode numbers) of both the low- f and high- f AEs did not vary with PA separation, and neither did the damping rate of the high- f mode, consistent with [40]. However, the damping rate of the low- f mode was found to increase with PA separation, in disagreement with [40] but agreeing with C-Mod results [35]. A closer inspection of these plasmas indicated that slightly differing edge conditions could explain this trend, at least in part; specifically, a lower q_{95} for the plasma with lower PA separation could lead to less continuum damping of the more edge-localized low- f mode. However, a quantitative assessment of the damping rate would require kinetic modeling, which is beyond the scope of this paper and left for future work.

One of the limiter plasmas was modeled with the linear, resistive MHD code CASTOR with the external antenna module enabled. A simulated scan of the antenna driving frequency determined that (i) the high- f mode was likely an $n = 0, m = \pm 1$ GAE with a global mode structure (see Fig. 4), while (ii) the low- f mode was likely an $n = 2$ TAE with strongest couplings of poloidal harmonics $m = 2, 3$ and $m = 3, 4$ within their respective gaps in the outer plasma region (see Fig. 5). These results are consistent with the AE antenna's power being injected into even, low- n modes when all are phased the same. A simulated increase in the PA separation by 50% confirmed the results of [40]: the same resonance was identified, but with less absorbed power (see Fig. 5c); moreover, the HWHM ($\propto \gamma$) of the simulated mode did not change with PA separation. This provides further support for the hypothesis that the plasmas were not perfectly reproduced in the PA separation scan.

In the second part of the study, we investigated the effect of the magnetic configuration on the efficiency of the AE antenna and AE stability. A database analysis revealed that resonance detection is $\sim 50\%$ more likely in limiter compared to X-point configuration (see Table 1). Furthermore, the damping rate was observed to increase strongly with edge magnetic shear for resonances detected in X-point configuration (see Fig. 6a). A closer look at the distribution of damping rates (see Fig. 6b) found that observations of low normalized damping rates, $-\gamma/\omega_0 < 0.4\%$, were more likely in X-point than in limiter configuration, agreeing with previous C-Mod results [35]. Once again, these data come from a wide variety of JET plasmas, yet the general trends observed - especially the enhancement in AE stability with edge shear - are then seen more clearly in our dedicated study.

Two ohmic plasma discharges were reproduced (see Fig. 7) to monitor the evolution of stable AEs throughout the transition from limiter to X-point configuration. While both

high- f and low- f AEs were observed initially during the limiter phase (see Fig. 8), the low- f mode could not be identified later as it further stabilized during the plasma's transition to X-point, consistent with JOREK simulations in [40]. In addition, the damping rate of the high- f mode increased as the edge shear increased during the limiter phase and into X-point. However, AEs with various toroidal mode numbers were observed during and after the configuration change, which was not assessed in [40] and cannot be easily explained. Nevertheless, CASTOR modeling was consistent with two EAEs, $m/n = 3/1 - 5/1$ and $m/n = 4/2 - 6/2$, being excited at the plasma edge (see Figs. 9 and 10, respectively), with a relatively higher damping rate inferred in X-point.

The experimental results of this paper have extended the results of previous studies and, in many ways, validated the simulation work in [40]. Modeling AE antenna excitation with CASTOR has proven to be necessary in the verification of toroidal mode number estimates and calculation of the mode structure and localization. Yet, additional modeling must be done to accurately assess the damping rate and compare with experiments; this is planned in the future. Finally, this work provides guidance in optimizing PA coupling for upcoming energetic particle experiments in JET, for which the AE antenna will play a crucial role in identifying the contribution of alphas to AE drive. If possible, the edge safety factor and edge magnetic shear could be lowered to widen the TAE gap and reduce continuum and radiative damping. Perhaps easier, we can decrease the PA separation to improve PA coupling while maintaining other plasma shaping parameters.

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