

Active Cells: The robotic radioactive waste processing facility at the European Spallation Source*

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The European Spallation Source Active Cells Facility is a unique facility for processing highly radioactive waste produced by the experiment. Due to the levels of radiation produced by the waste components combined with the scale of operations, the facility was designed to be operated without windows, using robotic manipulation systems and cameras for visual feedback. This article presents the challenges faced in delivering the processes required for size reduction and packing of the waste components along with the resulting design of the facility including key equipment and infrastructure developed to support the facility. Key subsystems are described in detail along with the considerations for maintenance and upgrades and the overall approach to safety. Finally, lessons learned and useful experiences are shared in the hope of informing the successful delivery of other similar facilities in the future.

Keywords: ESS, robotic, waste, hot cell, radiation, size reduction

I. INTRODUCTION

The European Spallation Source (ESS) is a high-performance, multi-disciplinary research facility centred on the worlds most powerful neutron source [1]. At full capacity, a 5 MW proton accelerator delivers 2 GeV protons onto a rotating tungsten Target Wheel. The resulting spallation reaction produces free neutrons, which are moderated and reflected using water, hydrogen, and beryllium before being directed via beamlines to experimental stations.

Although the principles and technology behind spallation sources are well established [2], the ESS surpasses all previous facilities in scale and beam power, introducing a range of new engineering challenges and complexities.

The Target Wheel assembly, including its central shaft, has a total mass of 10 tonnes, a height of 5.6 m, and a wheel diameter of 2.7 m. During operation, the wheel and adjacent components become highly radioactive, precluding direct human access. As such, these activated components must be removed and processed using remote handling systems.

The extraction from the target is carried out by the Cask Assembly a set of shielded casks with an internal hoisting system. The casks are then used to deliver the components to the Active Cells, the facility designated for processing and packaging the waste components.

This paper provides an holistic overview of core remote system design enabling safe, long-term operations of Active Cells Facility at the European Spallation Source.

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A. The Active Cells facility

The Active Cells Facility (ACF) is a large, shielded hot cell complex designed for the remote processing and packaging of activated waste materials generated by the spallation source. An overview of the facility layout and cell contents is shown in Figure 1.

Given the scale of the ACF and the high radiation levels involved, conventional through-wall operations using lead-glass windows for direct viewing is not feasible. Instead, the facility is operated entirely remotely, employing a combination of camera-based viewing systems and electrically and digitally controlled manipulators, hoists, and associated tooling. This approach enables safe and effective handling of high-activity components while maintaining operational flexibility and precision.

A wide variety of activated components are expected to be transferred to the Active Cells during the scheduled six-monthly shutdowns of the neutron source. Component lifetimes vary from approximately six months to five years, necessitating a processing throughput that can match the maintenance schedule to avoid delays in restarting operations, while maintaining strict safety standards for personnel.

The primary components identified for remote handling and processing include the Target Wheel assembly a large structure comprising a 2.6 m diameter tungsten wheel [3] mounted on a 5 m vertical shaft [4] and the Moderator Reflector assembly, which incorporates beryllium and steel elements. In addition, a number of smaller but still highly activated components will require processing. These include, but are not limited to, instrumentation plugs and the proton beam window.

All components entering the Active Cells will be pre-drained of process fluids, and will therefore consist exclusively of solid waste. The bulk of the structural material is stainless steel (grades 304 and 316), with component-specific materials included depending on functional requirements. Notably, tungsten and beryllium are present in the target and moderator assemblies respectively, while other com-

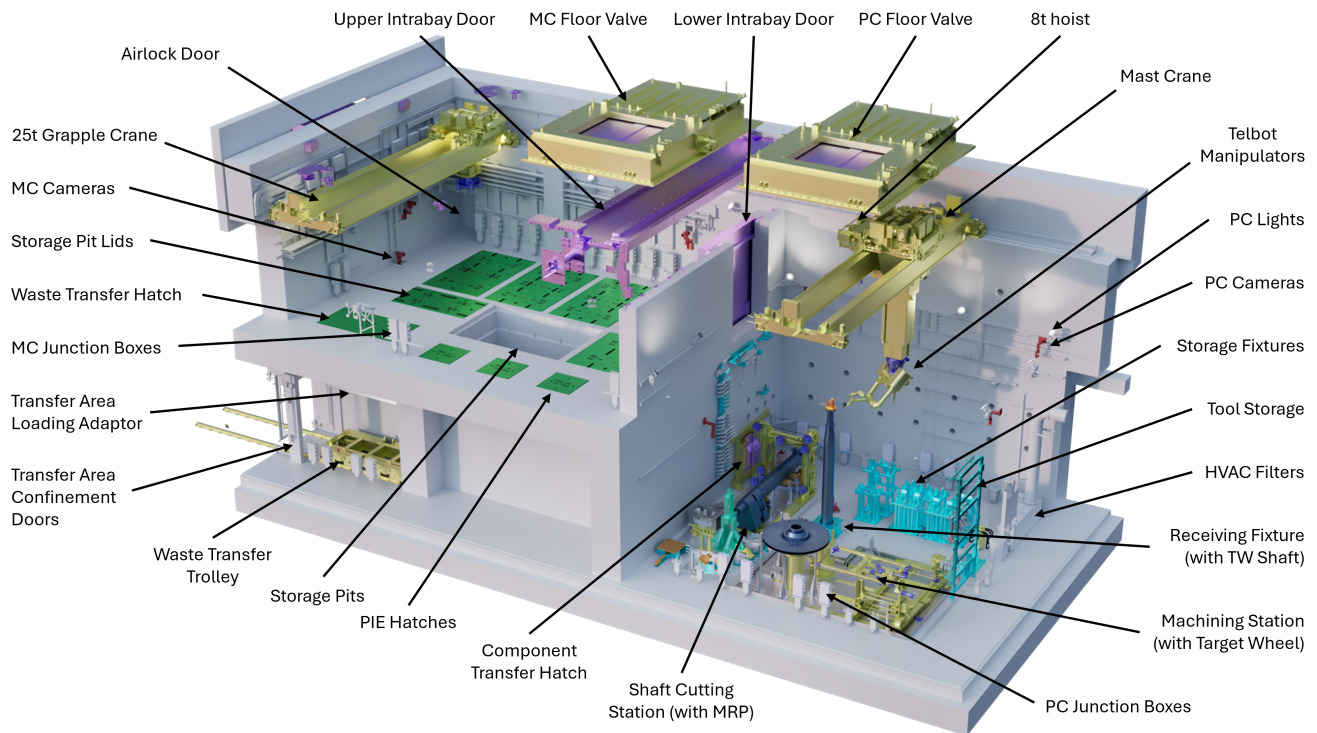


Fig. 1. Overview of the ESS Active Cells Facility with Process Cell shown on the right and maintenance cell shown on the left, separated by intrabay doors. The intrabay doors allow the transit of cranes between the process cell and maintenance cell whilst providing shielding protection for the maintenance cell. Key equipment within the facility is labelled.

ponents may include copper, silicon wafers, and various types of embedded instrumentation, such as thermocouples.

The processing operations within the Active Cells are focused on three core objectives that define the current handling strategy for activated components. First, large components must be reduced in size to meet the dimensional and mass constraints of standardised waste packages, enabling compliant storage, transport, and disposal.

Second, material segregation is essential for both radiological and waste classification purposes. The tungsten used in the Target Wheel must be separated from the structure of the Target Wheel to allow for appropriate treatment and disposal pathways (including size reduction of the wheel itself for transportation and storage). Likewise, the beryllium incorporated in the Moderator Reflector assembly must be carefully isolated from its stainless steel housing. This is necessary due to beryllium's unique radiological, chemical, and regulatory handling requirements.

Third, sample retrieval allows for post irradiation samples to be extracted from a defined location within the Moderator Reflector assembly. This requires precise cutting operations and delicate handling to extract the samples without damage or contamination.

These processing tasks drive the specification of remote handling equipment, including cutting tools, gripping systems, and inspection technologies, as well as influencing the spatial layout and shielding requirements of the Active Cells Facility.

The tungsten within the Target Wheel is distributed across thirty-six radial cassettes, while the beryllium is housed within the body of the Moderator Reflector. To accommodate the differing geometries and material configurations, cutting operations are categorised into two primary types: single-directional cuts for large, roughly uniform structures such as shafts and instrumentation plugs, and more complex multi-directional cutting for smaller, irregular components. As a result, two dedicated size-reduction stations are incorporated within the Active Cells to address these distinct processing needs.

Carrying out these cutting operations presents several significant challenges. Neutron irradiation causes substantial hardening and embrittlement of the component materials, particularly the steels [5], presenting challenges for mechanical cutting. These effects directly impact the choice and design of cutting technologies. Reference data used to inform processing strategies are drawn from established nuclear engineering codes, including the French RCC-MRx for the design and construction of nuclear installations [6], and the ITER structural design criteria for in-vessel components [7]. The use of cutting fluids is prohibited due to radiological safety and waste handling constraints, necessitating dry cutting methods. Additionally, strict limits are imposed on the generation of airborne radioactive particulates, requiring close control of the dust generation and management within the Active Cells.

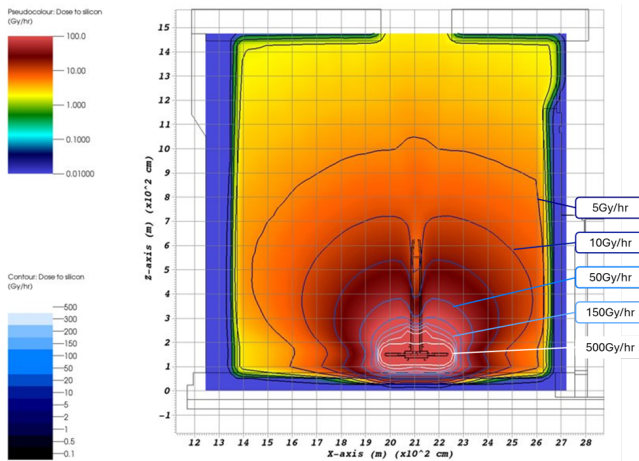


Fig. 2. Dose to silicon for a 4 year cooled Target Wheel placed within the process cell.

B. Key challenges

The operations carried out within the Active Cells Facility are not only complex from a mechanical and logistical standpoint but are further complicated by the extreme radiological environment. The primary radiological hazard arises from intense gamma radiation emitted by the activated components, particularly along direct shine paths and in close proximity to the waste materials. In addition to gamma emissions, there is some off-gassing of radioactive isotopes such as tritium or activated noble gases depending on the component and its operational history. Furthermore, a low-level of secondary neutron flux is expected due to photodisintegration reactions, particularly involving the beryllium in the moderator assembly.

The gamma dose rate in the vicinity of activated components has been assessed through a multi-stage simulation workflow [8].

In the first stage, the neutron flux induced in components during service in the spallation source was modelled using MCNP6 [9]. These simulations provided spatially resolved, energy-dependent neutron flux distributions, predominantly generated by spallation reactions in the tungsten target.

In the second stage, the neutron-induced activation and subsequent radioactive decay of structural and functional materials at the end of their service life were evaluated using MCR2S [10] and FISPACT-II [11]. This allowed for the generation of gamma source terms and the production of unshielded gamma radiation intensity maps, which represent the raw emission profile from the activated components.

A final set of simulations was performed using MCNP6 to assess the dose distribution within the fully modelled Active Cells Facility. These simulations incorporated the physical geometry and shielding characteristics of the cell infrastructure, yielding detailed maps of gamma dose rates throughout the facility. An example dose map within the process cell volume is shown in Figure 2.

The components processed in the Active Cells are expected to accumulate radiation damage levels of up to 4.5 displacements

per atom (dpa) over their operational lifetime. This radiation damage will result in source terms including gamma emitters such as Tungsten-187 and Hafnium-172, beta emitters like Tritium and Tantalum-182 and pure alpha emitters such as Gadolinium-148 [12]. Following shutdown and cooling, some components (such as the Target Wheel) can exhibit surface gamma dose rates as high as 700 Gy/hr.

The primary challenge relates to the radiation levels present in the facility, however in tackling the radiation challenge, a number of knock-on secondary challenges are seen. These include the need to incorporate features to allow for remote operations and maintenance of the equipment in the cell using a robotic handling system, and impacts related to the need for significantly limiting the range of technology based on radiation tolerance. Additionally, the levels of hazardous contamination that will be present complicates and limits the use of liquids due to the risk of spreading contamination and producing additional hazardous waste, creating complications and limitations on systems such as cutting and fire suppression systems where liquids would normally be used.

In typical cutting scenarios, cutting fluid is used to remove heat and reduce friction, however the use of cutting fluid is prohibited by the ESS facility owner due to concerns that it would spread contamination and prove difficult to decontaminate and dispose of. Without it, tool life becomes significantly reduced and the cutting significantly more challenging.

Early in the project, a survey was conducted to identify potential cutting methods, and a series of trials conducted using bandsaws and milling machines to establish feasibility of the identified methods including whether bandsaw blades could be changed remotely using remote-handling compatible technology. The feasibility trials established that, although challenging the dry cutting was achievable on material samples that presented similar challenges.

The trials also measured the volume of airborne dust produced during bandsaw cutting. By scaling this to account for the full cross section of the largest waste component, it was established that a typical density of airborne dust 0.3m from the cut was 0.058 mg/m^3 . By taking measurements at various distances from the cut, the total airborne dust produced during the trial was estimated to be around 33mg. The limit for airborne dust in the cell had been set at 4000 DAC (Derived Air Concentration) to ensure the safety of personnel in areas surrounding the Active Cells if a leak were to occur. By assessing the radioactive content of the material being cut, this was calculated to correspond to total of 22g of cutting dust, significantly higher than what was measured in the trial.

The result of the preliminary work indicates the need for a fully remotely operated facility with capability for large-scale size reduction and segregation tasks. All equipment installed into the cell would require remote operation as well as fully remote maintenance through the lifetime of the equipment.

209 C. Translating experience from fusion remote maintenance at 210 the Joint European Torus

211 Robotic technology in support of remote handling has been
212 a central part of fusion energy research for decades. A key
213 example of this is the remote handling system at the Joint Eu-
214 ropean Torus (JET) experiment [13], a capability developed
215 at UKAEA over a long period of maintaining and upgrad-
216 ing the JET system with robotic systems including long-reach
217 booms for deployment into the vessel as well as haptic tele-
218 manipulator technologies such as MASCOT [14].

219 More recently, the potential for translating capability de-
220 veloped through remote maintenance of the JET experiment
221 has been explored in other areas including maintenance of fu-
222 ture fusion plants [15], the decommissioning of legacy nu-
223 clear facilities in the UK such as gloveboxes [16], and in
224 support of decommissioning operations following the nuclear
225 disaster at Fukushima Daiichi [17].

226 It has been recognised that there is significant opportu-
227 nity to apply remote handling technology, operational expe-
228 rience, and know-how developed within the fusion domain
229 more widely [18]. This includes other challenging environ-
230 ments including high-energy physics experiments like the Eu-
231 ropean Spallation Source and beyond.

232 In particular, operational expertise developed during
233 decades of remote operations at JET was utilised in analysing
234 tasks to be undertaken within the Active Cells Facility as well
235 as equipment to be used. This allowed for translating prac-
236 tical experience from a similar remote handling domain in
237 order to influence the equipment selection and design as well
238 as the ways in which the operations would take place towards
239 a practical and robust solution.

240 D. Overview

241 This paper presents an overview of the overall design and
242 intended operation concept for the Active Cells Facility, the
243 waste processing cell at the European Spallation Source. The
244 specific challenges of carrying out the necessary processes
245 and environmental conditions will be explored along with an
246 exploration of how knowledge gained from other facilities
247 can be translated to the Active Cells Facility.

248 An overview of high-level subsystems is then provided,
249 followed by descriptions of each of the key subsystems. Ad-
250 ditionally, specific detail on some of the key subsystems, and
251 more challenging subsystems is provided. A discussion of
252 future needs and planned upgrades - the future of the ACF
253 is then laid out, exploring how the facility is anticipated to
254 evolve, and what accommodations have been made for poten-
255 tial future changes.

256 Finally, lessons learned and implications for other future
257 hot cell and similar facilities is presented, with the aim
258 of sharing useful experiences relevant to other high energy
259 physics experiments and environments that stand to benefit
260 from remote or robotic operation and maintenance.

261 II. OVERALL FACILITY DESIGN AND APPROACH

262 Requirements for the facility were initially developed from
263 the ESS facility needs. This captured the necessity for tran-
264 sitioning large, activated waste components into boxed waste
265 suitable for road transportation. Development of the Active
266 Cells was constrained by the existing civil design of the build-
267 ing which included the division of the facility into defined
268 areas, including the Process Cell and Maintenance Cell.

269 The complexity of the facility development necessitated a
270 systems engineering approach. A systems requirements docu-
271 ment was developed in conjunction with the ESS organi-
272 sation to ensure that the requirements for the facility were
273 fully understood and well defined. These requirements were
274 then further developed by breaking them down into functional
275 subsystem groups, then further into requirements for specific
276 equipment which could relate to hardware or purely software.

277 This structure ensured that every functional requirement
278 identified at a system level was addressed by the lower-level
279 conceptual subsystems and equipment. The management of
280 interfaces was of vital importance, with interfaces carefully
281 defined to ensure that concurrent development could proceed
282 successfully.

283 Feasibility studies were undertaken by assessing existing
284 products and technologies, as well as similar use cases, to as-
285 sess technological risk and maturity. The constraints of the
286 facility dictated that some non-standard or challenging un-
287 conventional approaches were required, steering the overall
288 approach and determining the necessity for further practical
289 trials. Requirements and concept designs were provided to
290 suppliers, while allowing for alternative concepts to be pro-
291 vided, encouraging innovative solutions. Over the course of
292 the project over £30 million has been spent in the UK and
293 European supply chain, with over 345 companies directly in-
294 volved.

295 In the resulting design, the Process Cell includes equip-
296 ment for receiving, temporarily storing, cutting, and packing
297 the waste components. The nature of the operations carried
298 out mean that the area will become highly contaminated, and
299 as such, the entire Process Cell is designed to be operated and
300 maintained without requiring access for operators: all activi-
301 ties will be conducted by remote control. The volume of the
302 cell is too large for effective use of viewing windows, so the
303 facility will be operated using cameras.

304 The Maintenance Cell is designated for maintenance of
305 equipment. Access between the Process Cell and Mainte-
306 nance Cell is controlled by two steel shielding doors, allowing
307 operators to access the Maintenance Cell whilst waste com-
308 ponents are present in the Process Cell. When open, these
309 doors allow the cranes of the Remote Handling System to
310 pass between the two cells. With the doors closed, opera-
311 tors in protective suits will be able to access the Maintenance
312 Cell to maintain the cranes and other critical systems.

313 Beneath the floor of the Maintenance Cell are six storage
314 pits for the temporary storage of waste prior to shipment off
315 site. When a shipment is ready, it is lowered from the Main-
316 tenance Cell into the Waste Transfer Area, where it is then
317 removed from the Active Cells using the waste transfer trol-

318 ley.

319 The walls of the Active Cell are 1.3 m thick high-density
320 concrete for shielding, lined with a stainless steel liner for
321 confinement. A ventilation system keeps the cells at a depres-
322 sion of 200 Pa from the surrounding rooms to ensure that any
323 leaks result in airflow inwards. All penetrations into the cell
324 need to ensure that the shielding and air-tight confinement are
325 not compromised.

326 The safety case for the facility was developed in parallel
327 with the design and delivery of the facility, as were the main
328 infrastructure elements such as electrical and data systems.

329 A. Cross-cutting infrastructure design

330 The overall design features the distinct encapsulated sub-
331 systems such as the handling system and shaft cutting sta-
332 tion but also elements of cross-cutting infrastructure that in-
333 terfaces with all of the major subsystems, providing essential
334 services. This infrastructure was more difficult to fully spec-
335 ify in advance in the absence of detailed information about
336 the individual subsystems and machines, and so was devel-
337 oped centrally throughout the delivery of the facility in par-
338 allel with the design, manufacture, and installation of other
339 items of equipment.

340 The major cross-cutting infrastructure elements include:

- 341 • Electrical infrastructure
- 342 • High-Level Control System and data distribution
- 343 • Emergency Stop system
- 344 • Radiological Safety System

345 B. Electrical infrastructure

346 The electrical infrastructure of the cell is a significant, com-
347 plex, and critical part of the overall system design. This in-
348 cludes:

- 349 • 80km of specialist radiation resistant cable
- 350 • 37 densely packed electrical control cubicles across 2
351 rack rooms
- 352 • 11 fully remote handleable Junction Boxes in the Pro-
353 cess Cell
- 354 • 16 modular and easily replaceable Junction Boxes in
355 the Maintenance Cell
- 356 • 4 modular and easily replaceable Junction Boxes in the
357 Waste Transfer Area
- 358 • 35 conduits into the active cells forming part of the con-
359 tainment boundary.
- 360 • 43 cold-side junction boxes



Fig. 3. Electrical Junction Boxes installed within the Active Cells Facility.

361 Dedicated low voltage distribution racks provide a bespoke
362 and easily customisable means of power distribution within
363 the two rack rooms provided for the Active Cells. Each one
364 has a 120A feed and together these supply nearly all of the
365 other subsystems with power.

366 The electrical infrastructure provides power and signals to
367 the Safety Systems, Lighting and Viewing systems, Compon-
368 ent Transfer Hatch, Floor Valves, Environmental Monitoring
369 System, Machining Station, Waste Transfer System, Intra-bay
370 Doors, and Supervisory Control System. The infrastructure is
371 built with redundant cabling that can be utilised in the event
372 of failures, or for reconfiguration or expansion of the capabil-
373 ities.

374 C. Network and Data Processing Design

375 The diverse range of equipment present within the Active
376 Cells include a variety of low level electronic control systems
377 under the direction of a higher level control architecture (See
378 Figure 4). In addition, a multi-camera, low latency, radia-
379 tion hardened viewing system gives operators a detailed view
380 of operations. Also, virtual reality displays show additional
381 views of operations with viewing angles that are not viable
382 with camera deployment.

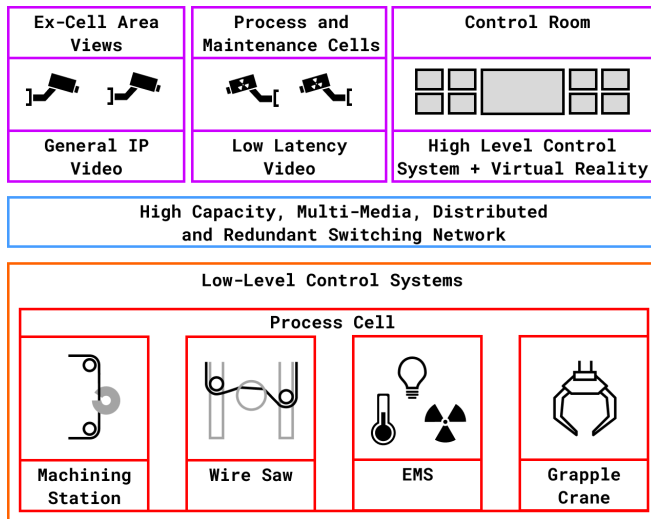


Fig. 4. ESS Active Cells operational systems, cameras, and high-level control systems are interconnected via high capacity network systems.

III. OPERATIONAL ANALYSIS AND DEVELOPMENT

From the first phase of specifying and designing the Active Cells Facility, analysis was conducted into the tasks that were expected to be performed in the cells in order to provide detail to the requirements, and identify any risks and issues.

The operational analysis provided significant input into the design and development of the Active Cells overall facility and remote handling system. Operational assessments have been developed across all aspects of the cell that require remote operation, ensuring that the functions of all equipment can be delivered reliably, repeatedly, safely, and with low risk.

The experience gained from operating the JET RH systems [19] has been used to offer input into the design process of the tooling and equipment to optimise operability and minimise operational risks and unforeseen issues.

Space is very limited inside the process cell with all equipment in place, therefore it is vital that operations can run in the most efficient manner. Virtual Reality (VR) assessments were undertaken on a wide range of components and assemblies for the active cells in order to explore feasibility of operations and maintenance activities. Areas of focus have included the Shaft Cutting Station, electrical junction boxes, and waste basket storage. The studies fed back into the design of the components and tools where necessary to ensure that tooling, equipment, and components were able to be manipulated effectively in the cell.

During the delivery of the Active Cells Facility, consideration was given to operator training needs, and a comprehensive training package was developed to be delivered to operators at the facility. Training needs follow on from sequence development as the training must be in sufficient depth to prepare competent and safe operators, including having a strong knowledge of the tooling, equipment, processes, and other aspects of the operations.

Significant experience from training and operating remote handling systems at the JET facility has been translated into the context of the Active Cells Facility and its equipment. This transfer of knowledge is essential in delivering equipment and hardware that will not only succeed to operate in the given conditions, but will do so in an optimal way.

The Active Cells Facility requires a large number of diverse tasks to be performed remotely during its lifetime. This includes operations in confined, cramped and awkward spaces that need careful consideration. Operational sequences defining step-by-step plans for each of the anticipated tasks were developed using virtual reality simulations and CAD models, taking experience from operational development processes used at JET [13]. Throughout this process, assessments were made on the effectiveness of tooling and positions within the cell. An example of this is the removal of the target wheel shaft, where the manipulator is required to remove a number of bolts from the joining flange. The order of these tasks is also significant. For example, by minimising tool and equipment changes the in-cell operations can be optimised to save time and resources.

The network and data processing systems for the ESS active cells facilitates the support of a wide range of network traffic types, a data integrity policy that is resilient to power disturbances and component failure, and a security policy that is compatible with the wider ESS facility policies.

Whilst the network and data processing systems interface with the wider ESS systems, they allow for operation that is fully autonomous from the wider ESS facility, except for the exchange of status data. Comprehensive status reporting of systems within the Active Cells is provided to the wider ESS facility, for diagnostics and preventative maintenance.

The network implementation utilises commercial off-the-shelf enterprise grade switching and routing equipment. To satisfy security policies, the major firewall implementation is located in the wider ESS network, however, a last line of defence is implemented within the active cells network in the form of an access control list. With control of network and server configurations confined to an isolated management network.

Advanced queue management within the switches protects different classes of traffic from mutual disturbances, whilst providing guaranteed bandwidth for vital inter-server communications. A fully automated run up / run down system, backed by uninterruptible power supplies, assures data integrity of the data processing systems in the event of power disturbances. Potentially damaging power inrush at startup is avoided using automated power sequencing.

Data processing is supported as a virtualised environment across multiple servers. Data storage is implemented as a multiply replicated, software implemented and distributed storage system. This affords maximum data integrity with fast recovery times and fast inter-server movements of virtual machines as required. Backed up virtual machine images allow for fast re-establishment of services in the event of major application software failure.

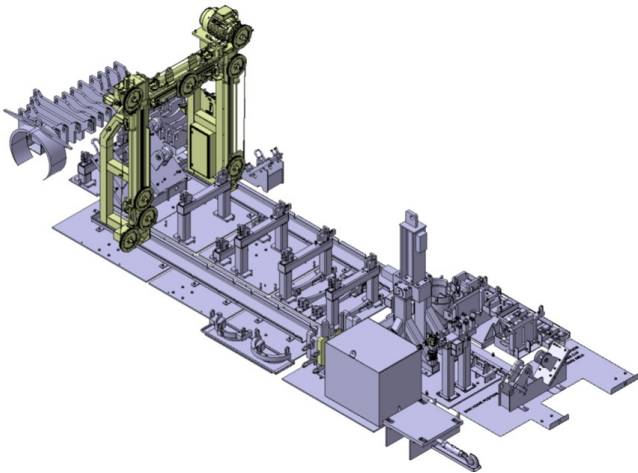


Fig. 5. Design of the Shaft Cutting Station. The wire saw shown in yellow sits above the rails and stands for supporting the shaft as it is cut into sections.

IV. PRIMARY FUNCTIONAL SUBSYSTEMS

The Active Cells Facility can be broken down into a number of distinct subsystems. The following sections provide a brief description of the most significant subsystems.

The primary functions of the cells relate to size reduction of waste components, transfer, and storage of waste. As such, the following sections will explore the implementation and design of the Shaft Cutting Station, the Machining Station, the Intrabay Doors, the Component Transfer Hatch, and the Waste Transfer System.

A. Shaft Cutting Station

The Shaft Cutting Station (SCS) performs the large-scale primary size reduction of activated items removed from the target station, such as cutting the 6.3m long Moderator Reflector Plug into smaller sections. The SCS is a large, remotely-operated wire saw as shown in Figure 5.

A diamond wire is used to cut through large components, reducing them to smaller sections compatible with handling, storage and export constraints. The cutting operations can require multiple wires and multiple days for a single cut. Components arrive in the cell vertically oriented and must be rotated horizontally to be cut. This is achieved by placing the component in a configurable, hinged cup, and laying it over by tracing an arc with the Grapple Crane. The components rest horizontally on a set of stands that are configured for each component using the Robotic Handling System.

The wire saw is moved between cutting locations using the 8 tonne hook on the Mast Crane, and locates in recessed features in two rails.

Cutting trials were conducted to assess the performance of the cutting system, as well as investigate other aspects such as the spread of contaminated swarf and dust during cutting. Super-duplex stainless steel was used as an approximation

for the material properties of irradiated 304 and 316 stainless steels with copper inserts used to represent the range of other materials present.

Initial trials were conducted with no ventilation present in the Active Cells. Dust measurements showed that airborne dust levels exceeded acceptable limits during the cutting. The trials were then repeated with a temporary ventilation system to simulate the airflow which will be present during operation. This showed a significant reduction in airborne dust, bringing the results comfortably back within acceptable limits.

The trials have shown that heat management is highly important during cutting. The wire temperature is a key parameter measured, and is used to control the progress of the cutting when the wire is too hot, cutting is slowed or halted. Overheating of the wire causes glazing of the wire which blunts the diamond beads and creates the need for premature replacement of the wire.

The test piece used were representative of the expected shaft cross sections, but thinner out of plane - with significantly less mass overall than the real waste components. Therefore, differences in the experienced heat transfer means work is ongoing to understand how the actual components will heat up during cutting.

A key challenge in the operation of the saw is the remote replacement of the cutting wire itself. Early trials were conducted on a representative pulley arrangement using a reacher-grabber tool operated manually to simulate the manipulators. During the Factory Acceptance Testing of the manipulator a further trial was conducted to ensure that the operation can be completed successfully.

B. Machining Station

The Machining Station (See Figure 6) is a diamond wire saw for performing accurate cuts on irradiated components, enabling the segregation of materials into specific waste streams, size reduction of components, and the retrieval of samples for analysis. The Machining Station is located in the Process Cell and is operated and maintained entirely remotely.

The diamond wire saw is mounted on a 4-degree of freedom gantry, enabling it to move in the X, Y and Z translational axes, as well as rotating the cutting face to enable vertical, horizontal and angled cuts. There are two stands that support distinct monolith components, and each is able to rotate presenting different faces of the component to the saw.

The machining station is operated using a suite of 8 motors, 8 resolvers, 8 limit switches, and 2 linear displacement sensors. Remote handleable connectors provide a cabling route to the control hardware, which is located outside the cell.

Operational challenges to the machining station include:

- Performing accurate cuts as the wire flexes during cutting
- Ensuring cables neither snag, or are damaged by the saw, in the full range of machine motion

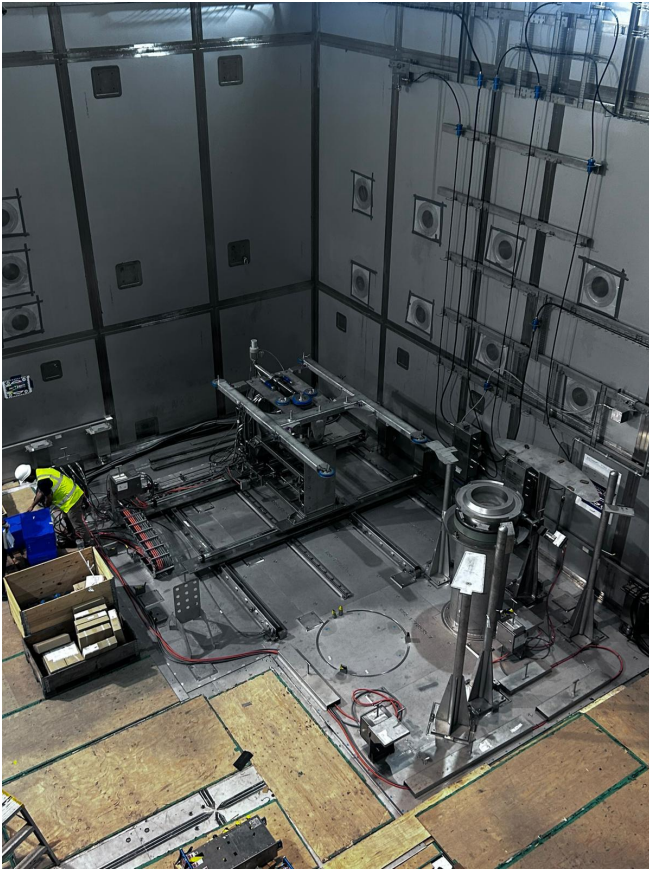


Fig. 6. Picture of the machining station during installation within the Active Cells, showing the diamond wire saw (back) mounted on its cartesian motion platform. On the bottom right, the component support stand for the target wheel can be seen (with the MRP stand still to be installed). The component stands include rotational functionality for the components, adding another degree of freedom to allow for more intricate cutting.

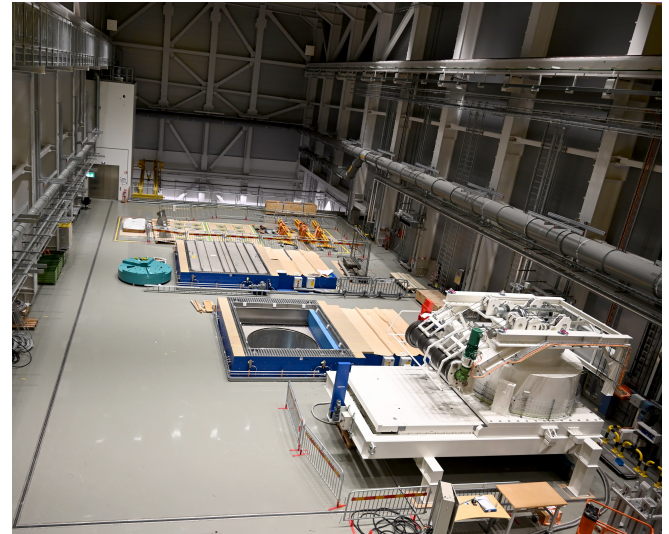


Fig. 7. View of the ESS High Bay, showing the floor valves and one of the ESS Transfer Casks

576

C. Floor Valves

577 The Floor Valves (See Figure 7) are a pair of gamma gates
 578 which cover two large openings in the ceiling of the Active
 579 Cells, each of which is 2.9m in diameter. The Floor Valves are
 580 the interface for the Active Cells with the ESS Transportation
 581 Casks - which are used to deliver components into the Active
 582 Cells from the ESS Monolith. When closed the Floor Valves
 583 provide the confinement and shielding barriers between the
 584 Active Cells and the ESS High Bay (which is a worker access
 585 area). The shielding requirement for the Floor Valves
 586 was defined as being equivalent to 1300mm of high density
 587 (MagnaDense 8s) concrete, with the shielding parameters en-
 588 hanced through the design process using neutrons analysis to
 589 minimise the risks to workers. The overall height of the Floor
 590 Valves is less than 1000mm, with the low profile required to
 591 minimise the lift height of the casks above the Active Cells.

592 Each of the Floor Valves weigh in excess of 72,000 kg, with
 593 the shielding provided by a large steel gamma gate, which
 594 is mounted on a pair of rails to allow for the shielding to
 595 be translated sideways to open the aperture. This process
 596 is controlled via the Active Cells high level control system,
 597 with permissions for operation controlled by the radiological
 598 safety systems via interlocks to prevent accidental opening.

599

D. Intrabay Doors

600 The Intrabay Doors are doors that provide safety-critical
 601 shielding within the Active Cells to protect operators in the
 602 Maintenance Cell from radiation originating in the process
 603 cell, whilst still allowing transfer of the crane and loads be-
 604 tween here and the Process Cell. They form part of the barrier
 605 between the Process Cell and Maintenance Cell of the ESS
 606 Active Cells facility. The barrier is achieved with 2 separate
 607 shield doors, an Upper Intrabay Door and a Lower Intrabay

- 559 • Confirming complete cuts, and lifting cut sections, us-
 560 ing only the remote manipulators and cameras
- 561 • Remote wire change

562 Maintenance challenges to the machining station include
 563 remote replacement of motors, sensors and junction boxes,
 564 interface management ensuring compatibility between exist-
 565 ing and replaced components, as well as the high radiation
 566 environment which prevents human access, limits the lifespan
 567 of polymers, and requires bespoke electrical components.

568 Both Shaft Cutting Station and Machining Station are
 569 highly complex systems with significant technical challenges.
 570 These include moving parts with drag chains, electromagnetic
 571 interference challenges, intricate cutting paths, and remote
 572 maintenance. The remote nature of the cutting systems means
 573 that maintenance including routine changing of cutting wires
 574 is required to be conducted remotely using the manipulator
 575 system with feedback via cameras.

608 Door.

609 Both doors open to allow passage of the cranes and sus-
610 pended loads. The Upper door includes a number of small
611 cut outs to allow for passage of the crane rails, crane resolver
612 track and crane drag chains. Both doors are controlled via
613 the Active Cells High-Level Control System by an operator
614 situated within the Active Cells Control Room.

615 In the event of failure, recovery systems located outside
616 of the Active Cells Facility can return both the Lower and
617 Upper Intrabay Doors to the closed position without the need
618 of workers access to the Active Cells.

619 The doors have only a small opening, which provides a dy-
620 namic confinement function due to the air flow through from
621 the Maintenance Cell to the Process Cell. The Intrabay doors
622 also provide a physical barrier to minimise dust and contami-
623 nation entering the Maintenance Cell.

624 The Lower Intrabay Door is constructed from S355 carbon
625 steel, 360mm thick in sheets, clad with 4mm stainless steel. It
626 moves horizontally along a floor rail using a rack and pinion
627 system, with a balance rail midway up the wall. The system
628 incorporates a manual recovery drive system through a gear-
629 box actuated from outside the cell

630 The Upper Intrabay Door is constructed from S355 carbon
631 steel 150mm thick, clad in 4mm stainless steel. It swings ver-
632 tically to open using a wire rope and pulley system. In the
633 open position, the door is held flat against the ceiling sup-
634 ported by two shotbolts actuated external to the Active Cells.
635 The pulley drums are located outside of the cell via penetra-
636 tions.

637 E. Component Transfer Hatch

638 The Component Transfer Hatch [20] provides means for
639 transferring small components of up to 30kg in and out of
640 the Active Cells via a tunnel which extends the steel lining of
641 the cell through the concrete shielding wall, whilst maintain-
642 ing the safety of the facility. It forms part of the ESS Active
643 Cells outer perimeter; the hot side hatch is to be located in
644 the Active Cells Process Cell and the cold side hatch located
645 in the Technical Galleries Penetration Room connected to a
646 glovebox.

647 In all scenarios the Component Transfer Hatch must pro-
648 vide a shielding and confinement barrier to protect workers
649 in the Penetration Room from radiation and contamination
650 hazards in the Active Cells. This means providing the re-
651 quired radiological shielding (equivalent to 1300mm of high
652 density (MagnaDense 8s) concrete) and ensuring the Active
653 Cells confined area remains at a lower pressure than its sur-
654 roundings so that any leakage is avoided.

655 The Component Transfer Hatch is composed of two doors,
656 which individually provide the required shielding, a payload
657 transfer mechanism, and a glovebox that ensures confinement
658 and prevents the spread of contamination into the Penetration
659 Room. The main design drivers are:

- 660 • to provide the required shielding needs
- 661 • operational performance

- 662 • to pursue a standardised and optimized design,

- 663 • to enable ease of installation

- 664 • to ensure a simple and quick maintainability paying
665 special attention to the Remote Handling Compatibil-
666 ity of the Hot Side design and the ergonomics of the
667 Cold Side design solution.

- 668 • Decontamination aspects to minimize the accumulation
669 of radioactive debris.

670 The doors are composed of two monocoque parts based
671 on an optimised stainless steel shell configuration filled of
672 poured lead, where the shell serves both as structure of the
673 door and as mould for the lead casting. With the aim of stan-
674 dardising the design and optimising efforts and costs, a single
675 solution has been developed for both hot and cold doors.

676 Shielding needs have been determinant for the dimensional
677 configuration of the doors so that each door independently
678 provides the required radiation protection. The shielding con-
679 figuration has been defined as a result of an iterative pro-
680 cess starting from very simple ray tracing studies to detailed
681 and exhaustive calculations performed with Particle Transport
682 Codes (MCNP) [21] that have confirmed the shielding capa-
683 bilities of the system.

684 Challenges posed by the installation constraints have also
685 been overcome through a modular design solution. This
686 modular design provides a simple solution to the constrained
687 spaces and apertures for installation at both sides, being the
688 dimensions of the Floor Valves apertures in the Hot Side and
689 the restrictive dimensions of the Penetration Room the main
690 challenges for the installation.

691 The design of both doors has been developed so that, while
692 maintaining the same architecture at both sides, it is adapt-
693 able to the dissimilar arrangement of the building interfaces
694 present in the Process Cell and Penetration Room minimiz-
695 ing to the maximum extent its impact on the aesthetics of the
696 doors design.

697 The transfer mechanism transfers the payload into and out
698 of the Active Cells. The maximum volume that can be trans-
699 ferred between the hot side and cold is 290 x 290 x 160mm.
700 The design of the transfer mechanism:

- 701 • Is characterized by its modularity and encapsulated na-
702 ture.

- 703 • Maximizes the predictability of this system

- 704 • Provides a reliable and fail-safe design

- 705 • Eases the installation and maintenance operations.

706 The glovebox is the component in charge of ensuring
707 the confinement of the system. The design has been con-
708 ceived to be a monobloc configuration that contains the whole
709 system within its confinement barrier having only electrical
710 feedthroughs crossing the confinement boundary, which min-
711 imises the number of leak barriers and associated risks.

712

F. Waste Transfer System

713 After waste is processed and packaged in the Process Cell,
714 the waste packages must be transitioned through the Maintenance
715 Cell, into the Transport Hall via a the Waste Transfer
716 Hatch, where they can be collected by lorry for road transport
717 to off-site storage facilities. The confinement and shielding
718 barriers between the Transfer Area and the Transport Hall
719 are provided by a large confinement door and external shield
720 block.

721 The Waste Transfer System provides a means for trans-
722 porting filled Waste Storage Baskets within shielded stainless
723 steel tanks along this route, with the steel tanks loaded by
724 the grapple crane. The system is centered around a trolley
725 which is capable of supporting loads of 115 tonnes in order
726 to accommodate the mass of the waste plus the mass of the
727 shielded containers in which it is packed. Features are in-
728 cluded to ensure the robustness of the interactions between
729 the Grapple Crane and the Waste Transfer system for transi-
730 tioning waste packages between the two.

731 The Waste Transfer System is connected into the safety
732 system to ensure safety of the facility whilst the hazardous
733 waste packages are being transitioned.

734

G. Storage Pits and Lids

735 The Storage Pits sit beneath the floor of the Maintenance
736 Cell and provide safe storage locations for processed materi-
737 als and for specific high-activation components to cool prior
738 to processing. The storage space within the Active cells was
739 sized to allow for storage of more materials than would be
740 processed in any single operational campaign.

741 The Storage Pit lids provide a shielding barrier between the
742 Storage Pits and the Maintenance cell, and can be remotely
743 opened and closed using the Active Cells handling system.
744 The Storage Pit Lids also provide a shielding barrier on the
745 waste export route from the Active Cells and on a number of
746 opening which are included to allow for future expansion of
747 local post irradiation examination capabilities. The Storage
748 Pit Lids were required to provide an equivalent to 1300mm
749 of high density concrete of shielding, with neutrons analy-
750 sis conducted to validate the design. The Storage Pit Lids
751 are primarily constructed using re-enforced high density con-
752 crete with a stainless steel cladding, with some special cases
753 manufactured from mild steel with a stainless steel liner.

754 The Storage Pit Lids have been designed for full remote
755 handling by the grapple crane (as shown in Figure 8). To
756 allow for larger storage pit openings whilst remaining within
757 the load capacity of the Grapple Crane, the storage pit lids
758 have been segmented - with between 2 and 4 lids per pit (with
759 individual lids weighing up to 22,000 kg). In total there are
760 26 separate Pit Lids, providing approximately 400,000 kg of
761 shielding.

762 Additional safety locks have been provided which prevent
763 the pits being opened by the grapple crane, to safeguard work-
764 ers from accidental exposure during hands-on maintenance.

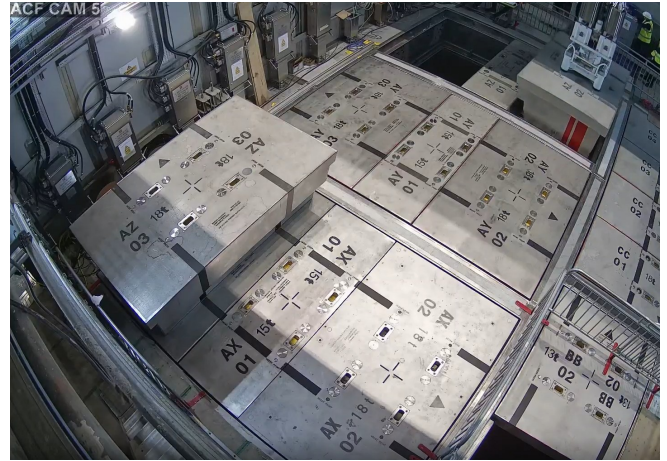


Fig. 8. Storage Pit Lid being handled by the Grapple Crane in the Maintenance Cell

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V. DESIGN OF THE HANDLING SYSTEM

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- 787 1. Storage Pit Lid handling activities (Operational Vol-
788 ume A)
- 789 2. Large Target Station component handling activities (in-
790 cluding layover) using the Grapple Crane
- 791 3. Waste Basket handling activities using the Grapple
792 Crane
- 793 4. Lifting Chain installation and use activities
- 794 5. Target Station component lifting adapter installation
795 activities
- 796 6. Medium sized Target Station component handling ac-
797 tivities (including layover) using the 8t hoist



Fig. 9. Arrangement of the handling system. A telescopic mast interfaces with the crane bridge to provide X-Y-Z positioning within the cells. At the bottom of the mast, the dual-armed Telbot manipulator is mounted to provide dexterous tele-robotic manipulation capabilities.

- 798 7. Waste Basket handling activities II (For handling of
- 799 lighter/empty baskets using the 8t hoist)
- 800 8. Shaft Cutting Station and Machining Station line re-
- 801 placeable unit replacement
- 802 9. Cutting Station wire replacement
- 803 10. Activities involving large bolts and tooling installation
- 804 11. Floor and wall mounted item removal activities
- 805 12. Handling of delicate components
- 806 13. Junction Box replacement activities
- 807 14. Camera replacement activities
- 808 15. Pipe and wire cutting activities
- 809 16. Contamination survey activities
- 810 17. Active Cells cleaning activities
- 811 18. Maintenance control for installation and maintenance
- 812 Use

813 These could then be considered as bounding tasks on the
 814 cell for initial specification of needs and also as a known base-
 815 line for capability of the handling system when considering

816 new additions or modifications to equipment within the Pro-
 817 cess Cell.

818 Challenges faced in designing the handling system in-
 819 cluded accounting for recovery scenarios, ensuring opera-
 820 tional coverage of the full volume, compatibility with the
 821 radiation environment, mast travel constraints (including ca-
 822 ble routing), long travel drag chains, camera and signal cable
 823 runs, and limited headroom for maintenance.

824 To support fully remote operations across a large working
 825 volume, the Active Cells Facility requires a handling system
 826 capable of both precise manipulation and heavy lifting. Op-
 827 erational requirements and infrastructure constraints led to
 828 the definition of two functional payload capacities 50 kg for
 829 dexterous tasks and up to 25 tonnes for large component han-
 830 dling. However, the single set of crane rails limited system
 831 deployment, prompting the definition of operational zones
 832 with specific equipment and task allowances. To extend lift-
 833 ing capacity in the manipulator area without compromising
 834 fine control, an 8-tonne auxiliary hoist was included on the
 835 Mast Crane as a mid-range lifting solution [8] and a 3-tonne
 836 crane hook was added to the base of the mast as a lower-range
 837 lifting solution.

838

A. Mast Manipulator

839 The selected manipulators for dexterous manipulation
 840 tasks are dual-arm Telbot systems from Walischiemler, each
 841 arm rated for a payload capacity of 50 kg and equipped with
 842 integrated force-feedback functionality. The manipulator as-
 843 sembly is mounted on a telescopic vertical mast with a max-
 844 imum extension of 8 metres, which can be retracted to allow
 845 passage through the transfer opening into the Maintenance
 846 Cell. This vertical mast provides a stable platform for dexter-
 847 ous manipulation tasks anywhere within the Process Cell.

848 The mast base is capable of rotating ± 180 deg around the
 849 vertical axis, enabling the manipulators to access a wide range
 850 of positions and orientations within the Process Cell. In addi-
 851 tion to the manipulators, an 8-tonne lifting hook is suspended
 852 from a hoist on the overhead crane gantry. This hook falls
 853 within the reach envelope of the manipulator arms, allowing
 854 the operator to rig and unrig heavy components for lifting and
 855 transfer.

856 Control of the manipulators is achieved through kinemat-
 857 ically equivalent master arms, which the operator interacts
 858 with. The in-cell manipulators replicate these motions in real-
 859 time. Simultaneously, forces exerted on the manipulator arms
 860 are scaled and fed back to the operator via the control inter-
 861 face, enabling tactile awareness of the task environment.
 862 This force-feedback capability significantly enhances preci-
 863 sion and control, making it possible to perform delicate or
 864 complex operations remotely.

865 The dexterous manipulators have been specified to allow
 866 for direct handling of tooling, some line replaceable units, and
 867 lifting equipment, with several options for gripper interfaces
 868 including pre-defined geometries and defined bolting patterns
 869 which allow for use of a standardised gripper block.



Fig. 10. Grapple crane carrying stainless steel waste storage basket.

B. Grapple crane

The Grapple Crane (See Figure 10) is a dual bridge beam overhead gantry crane, which deploys a grapple interface via four hoist ropes for stability. The four twistlocks are actuated by radiation tolerant stepper motors, and the whole interface plate can rotate by ± 180 deg about the vertical axis whilst carrying loads. Each axis of motion has redundant drives to allow recovery back into the Maintenance Cell in case of failure.

The interface for the Grapple Crane was standardised early in the design process. This was essential to allow concurrent development of the equipment within the cell, but also to ensure that the remote handling operations could be conducted as efficiently as possible. The heavy-lift interface was defined as four actuated twistlocks to be deployed by the crane, and their respective pockets in the interfacing component. This allows the crane to attach to compatible loads without requiring operators to perform any rigging.

VI. DESIGN OF THE HIGH-LEVEL CONTROL SYSTEM AND OPERATOR INTERFACES

The High-Level Control System (HLCS) is a vital part of the ESS Active Cells Facility. The ESS ACF contains a vast array of lower-level control systems developed by various 3rd party suppliers. These systems need to be operated from a unified interface with enhanced functionality to reduce the likelihood of operator error. These mechanisms include interlocks, simulators, user authorisation, command sequencing and action monitoring.

The HLCS is separated into vertical slices. Each slice controls an individual system such as the machining station, grapple crane or lighting control. The different sections of the vertical slice are integrated via ROS 2 [22]. For each connected device, a driver is provided that allows ROS2 to communicate with the device via OPCUA [23]. Each driver uses the RTI

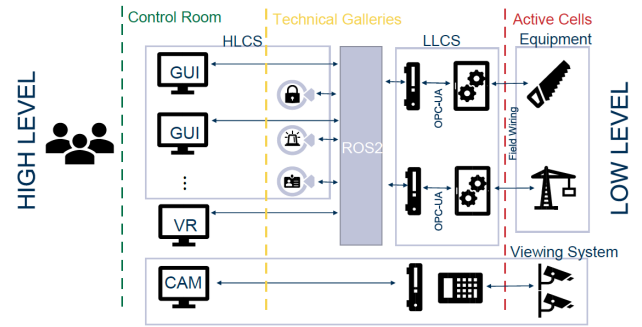


Fig. 11. Architectural design of the High-Level Control System. Operators interface with equipment via Graphical User Interfaces (GUIs) illustrated on the left. Control and communications of data is then transferred via layers including a ROS2 element, and OPC-UA interfaces to the low-level control systems of individual equipment controllers (right).

OPCUA-DDS Gateway along with some custom software.

ROS2 Manager Nodes add configurable interlocks, command authorisation, enhanced command interfaces (Actions), and other high-level functionality to support operations. Graphical User Interfaces have been developed using QML integrated with ROS2 to communicate with the manager nodes.

A. System Architecture

The HLCS has been developed in a layered structure (see Figure 11) where clients such as GUIs interact with the system through ROS2 Actions and Services. These invoke specific commands across the various low-level control systems and devices. In addition to commands, a Condition Engine Node continuously monitors the current states of the subsystems and generates Conditions, used by Manager Nodes to prevent or allow the execution of commands.

The HLCS can connect to either the physical system or a simulation. When connected to the physical system, the Driver Node interacts with the individual system Low Level Control Systems (LLCSs), whereas in simulation-mode, it interacts with an emulation of the system instead.

B. High Level Functionalities

In order to accommodate multi-user interactions with the system, a role-specific authorisation system ensures that users can only interact with permitted subsystems and only approved personnel can override inhibit conditions within the system.

Concurrent interaction is prevented through the use of Conditions whilst the Graphical User Interfaces (GUIs) continuously update the Human Machine Interfaces (HMIs) based on the availability of operational commands. This increases the usability of the GUI for multi-user interactions.

936 An alert system continually monitors the Conditions and
 937 can alert operators to concerning situations clearly and
 938 quickly.

939 A comprehensive logging system allows for the record-
 940 ing of all interactions across the HLCS components. These
 941 records can be kept for future reference and retracing of
 942 events. In simulation mode these can serve as a task devel-
 943 opment tool.

944 C. Viewing and Lighting Systems

945 Due to the operations being conducted remotely without
 946 the use of windows, a comprehensive viewing and lighting
 947 system was required to allow for remote monitoring and oper-
 948 ation of the equipment within the Active Cells. The View-
 949 ing System provides visual feeds for operators in the control
 950 room. Due to the number of interconnected elements, it is one
 951 of the most complex electrical packages across the facility.

952 Cameras include 12 Radiation Tolerant Cameras in the Ac-
 953 tive Cells, 6 in the maintenance cell and 6 in the process cell,
 954 as well as 8 cameras on the cranes and 1 mobile camera in the
 955 Process Cell. The system provides views to 5 workstations
 956 (desk positions in the control room), including 1 workstation
 957 for the manipulator operator.

958 A bespoke Lighting System has also been installed with
 959 considerations made to the radiation environment. Features
 960 of the lighting system include radiation tolerant lights rated
 961 up to 1MGy total lifetime dose, dimming controls, and indi-
 962 vidualy switchable lights. The lighting system is designed to
 963 be fully maintainable by the remote handling system, as well
 964 as featuring mobile lights that can be positioned by operators
 965 remotely to provide lighting for specific tasks as required.

966 In order to eliminate stroboscopic effects on Viewing Sys-
 967 tem, a 230V direct current power supply is used to power the
 968 lighting system.

969 D. Graphical User Interfaces

970 Graphical User Interfaces have been provided for all of
 971 the given systems using the UKAEA Commander tool, com-
 972 bined with QML, allowing operators to control and monitor
 973 the equipment. Figure 12 shows an example of the user inter-
 974 face provided for the Grapple Crane.

975 Multi-user interaction is enabled by ROS 2/DDS and gov-
 976 erned by a Preconditions and Claims system. Execution re-
 977 quires an active Claim on the subsystem and satisfied Pre-
 978 conditions. This supervision and governance, along with en-
 979 hanced feedback and context awareness, is what makes con-
 980 current GUIs operationally viable. This functionality allows
 981 for a user interface or status display to be duplicated on mul-
 982 tiple screens, however access to send commands or operate
 983 equipment can only be "checked out" by one operator at a
 984 time. This effectively is a set of inhibits and interlocks func-
 985 tionality for protection within the HLCS.

986 The modular and agile design allows for any of the desks
 987 to be used by any of the operators depending on operational

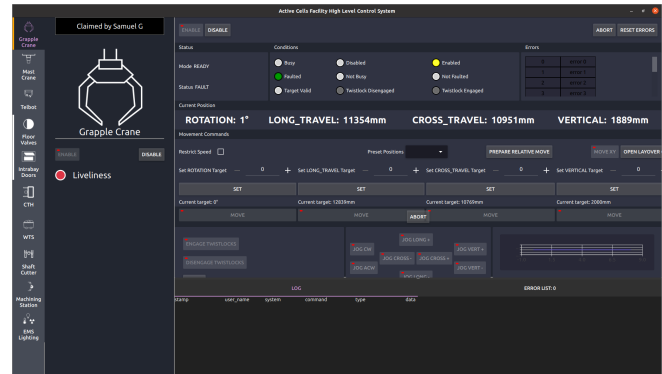


Fig. 12. Example Graphical User interface for control of the Grapple Crane. The interface shows different control modes for each axis, including jog and drive to set point. These include a visual indicator showing the position of the axis within its range of motion and limits (which are visualised using an accompanying VR system).

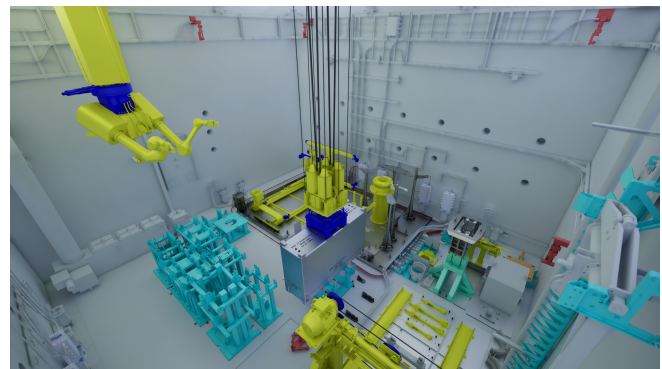


Fig. 13. Virtual Reality visualisation showing views from the process cell during a simulated remote handling operation.

988 needs with a high degree of interchangeability. User login
 989 functionality is also provided to ensure only operators who
 990 are suitably qualified and experienced can control items of
 991 equipment on a granular basis.

992 E. Virtual Reality Visualisation

993 A Digital Twin or Virtual Reality (VR) model is updated
 994 in real-time with the status and positional information of all
 995 instrumented systems within the facility as shown in Figure
 996 13. The spatial information provided by the VR system is
 997 displayed on computer monitors, and can be used by the oper-
 998 ators for monitoring, and planning consecutive actions for
 999 the task at hand.

1000 The VR Visualisation is provided by RHOVR, a software
 1001 system to provide support for remote handling engineers.
 1002 It provides advanced 3D visualisation for remote handling
 1003 equipment in challenging environments.

1004 The primary goal of RHOVR is to deliver a real-time in-
 1005 teractive 3D model powered by the 3D visualisation software
 1006 (Unreal Engine [24]). 3D models of the equipment are ani-

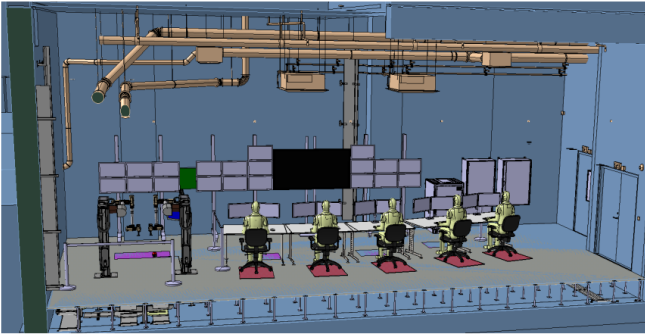


Fig. 14. Layout of the Active Cells Control Room showing operator stations and display screens.

1007 mated in real-time to match the state of equipment as reported
1008 by the control systems.

1009 The system also allows for offline task development and
1010 training in a safe and controlled, yet realistic environment,
1011 reducing cost and risk associated with developing new or
1012 challenging tasks, and training new individual operators and
1013 teams to conduct operations within the Active Cells Facility.

1014 F. HLCS Integrated Subsystems

1015 In order to the perform various tasks including size-
1016 reduction and waste-handling, there are 13 subsystems such
1017 as overhead cranes, manipulators, diamond-wire saw and cut-
1018 ting stations, etc. Every system is interfaced with the HLCS
1019 through the industrial OPC UA communication protocol.

1020 OPC UA is a connection-oriented protocol and is not di-
1021 rectly compatible with ROS2. In order to communicate with
1022 the LLCS systems, OPC UA Gateways are used to read val-
1023 ues, which are then published as Topics. Conversely Driver
1024 Nodes are used to write commands directly to the subsystems.
1025 To ensure operational integrity, a bidirectional heartbeat sys-
1026 tem consisting of assertors and monitors are implemented.

1027 G. Control Room

1028 The design for the Control Room was deeply informed by
1029 the overall concept and operational method from the Remote
1030 Handling Control Room at JET. The ESS Active Cells Facil-
1031 ity hosts significantly more equipment than the JET remote
1032 maintenance systems, and so the design could not be directly
1033 translated, but was adapted to meet the needs of the new con-
1034 text. Additionally, it was desirable to leverage advantages
1035 of new technological developments and some of the known
1036 shortcomings of the JET design in delivery of the Active Cells
1037 Control Room.

1038 The overall design includes a set of connected desks for the
1039 operations team in front of a wall of display screens for moni-
1040 toring camera views and software displays as shown in Figure
1041 14. Thin client computing is available and provides access to
1042 displays and user interfaces for equipment at the desks. A

1043 set of control arms, kinematically similar to the remote Tel-
1044 bot manipulator are provided as the primary operator inter-
1045 face for performing remote handling and manipulation tasks.
1046 Feedback is provided via camera views relayed via the dis-
1047 play screens, as well as some haptic information rendered to
1048 the operator through motors actuating the control arms.

1049 Considerations have been made for adaptability and versa-
1050 tility of the control room for example by providing the ability
1051 to interchangeably switch any display to any viewing monitor.

1052 VII. DESIGN OF THE SAFETY AND MONITORING 1053 SYSTEMS

1054 The Active Cells Facility includes a range of subsystems
1055 for safety and monitoring of the status of the facility, rang-
1056 ing from conventional machine safety systems, radiologi-
1057 cal safety systems, and environmental monitoring systems.
1058 These are described in the following sections.

1059 A. Radiological Safety system

1060 The Radiological Safety System provides thirty different
1061 Safety Instrumented Functions which together protect work-
1062 ers from exposure to radiological hazards when inside or out-
1063 side the active cells. These Safety Functions can be grouped
1064 into:

- 1065 • Detecting the radiation levels inside and outside the ac-
1066 tive cells.
- 1067 • Detecting that movable radiation shielding blocks and
1068 doors are in the correct positions to protect workers
1069 from radiation shine paths and prevent these shielding
1070 elements from being moved while operators are in the
1071 potential shine path.
- 1072 • Managing access to the cells (for the limited scenar-
1073 ios that human access is required) by only releasing the
1074 airlock key for entry when all shielding is in place and
1075 radiation levels are within acceptable safe limits.
- 1076 • Pressure monitoring to ensure that dynamic confine-
1077 ment is maintained (by ensuring the air pressure in the
1078 cells lower that air pressure outside the cells by a de-
1079 fined margin). This ensures any air and leakage across
1080 the seals to the cell will be inwards rather than poten-
1081 tially contaminated air escaping.
- 1082 • Initiating alarms to alert operators and evacuate person-
1083 nel in the case of any unexpected radiological event.

1084 The risk reduction required is achieved by two independent
1085 safety systems with diverse approaches to ensure the likeli-
1086 hood of significant exposure occurring is extremely low, and
1087 within the limits set by the European Spallation Source Or-
1088 ganisation. The two independent safety systems are called the
1089 Radiological Protection System and the Radiological Alarm
1090 System.

1091 The Radiological Protection System is a SIL-2 rated system implemented via a Safety PLC. It primarily acts by removing power from cranes, doors, trays, hatches, trolleys and manipulators when an unsafe configuration of automated systems is detected. The Radiological Protection System also prevents unsafe access to the cells via a key interchange. The Radiological Alarm System is a SIL-1 rated relaylogic based safety system which causes alarms to activate if interlocks or confinement fails. This provides a backup to the Radiological Protection System, allowing operators to evacuate if all other systems fail.

B. Differential Pressure Monitoring System

1103 The pressure within the Active Cells is maintained below the pressure of the surrounding areas to contribute to the confinement boundary. This pressure difference is monitored by the Differential Pressure Monitoring System (DPMS). The DPMS delivers a Safety Instrumented Function to monitor the difference in pressure between the inside and outside of the ACF. It raises an alarm if the difference falls below a threshold value.

1111 The system takes two independent measurements of the pressure difference per cell and a 2 out of 2 to alarm architecture is used to reduce the risk of spurious alarm trips due to transient pressure fluctuations.

1115 Remotely handleable dust filters are located on the hot side to prevent contamination ingress into the pipes, and three-way valves allow a compressed air line to be fitted to the system in order to purge the pipelines of contamination.

1119 Exposure to the Active Cells atmosphere for the DPMS is provided via the Media Couplings, which are through wall penetrations with a labyrinth shape to prevent shine paths. As these are cast into the building structure the number and locations of these needed to be considered early in the facility development.

C. Master Emergency Stop System

1126 It is a legislative requirement under the Machinery Directive to provide Emergency Stop functionality for industrial machines and this function is provided by safety systems local to each machine. All of the machinery described is designed to be operated from the Active Cells Control Room and there are a wide variety of possible hazardous scenarios in which the operators may need to quickly stop the operation of machinery to keep personnel safe and for asset protection.

1134 The Master Emergency Stop System provides the functionality for the operator to press a single button, bringing everything in the Active Cells to a stop, removing the need for operators to spend time identifying specific stops for individual equipment.

1139 The Master Emergency Stop interfaces with nine other systems and machines including:

- Remote Handling System

- Intrabay Doors
- Component Transfer Hatch
- Transfer Cask System
- Intelligent Extraction Tool Cask System
- Machining Station
- Floor Valves
- Shaft Cutting Station
- Waste Transfer System

1150 The Master Emergency Stop system also monitors faults which may occur in any of these interfacing systems. It provides logic to allow central reset of the interfacing systems with appropriate monitoring to prevent unsafe reset in the case of faults or local safety demands.

1155 The local safety systems for individual pieces of equipment are implemented using a diverse range of physical hardware, which interface with the Master Emergency Stop System, ensuring the same functionality is delivered across the Active Cells.

1160 The installed Master Emergency Stop System is software/-PLC based and meets Performance Level d in compliance with key Machinery Safety Standards EN ISO 12100, EN ISO 13849-1 and EN ISO 13850.

D. Fire Suppression System

1165 The overall approach towards fire safety within the facility began with minimising the risk of fires occurring, and then minimising the risk of fires spreading if they were to occur.

1168 Approaches to minimising risk of fire include use of Low-Smoke Zero Halogen cables throughout the facility, compounding technology constraints imposed by radiation hardness requirements, as well as minimising the use of oils, greases and other combustible materials.

1173 A fire detection system is installed, which includes detection systems to monitor the rate of temperature change, as well as monitoring for smoke.

1176 If a fire were to be detected, airflow in the facility will be restricted and controlled, minimising spread. A fire suppression system including a water mist spray is also in place, balancing the need to suppress potential fires, whilst minimising the impact of water interactions with active dust such as spread of contamination. The water mist system is not immediately triggered on a fire detection, but instead is assessed by a central ESS fire control unit which allows for manual activation of the system. The actuation and control systems related to the fire suppression system are installed outside the Active Cells in order to minimise complexity related to the challenges of the environment inside the Active Cells.

E. Environmental Monitoring System

The Environmental Monitoring System (EMS) is a non-safety system for monitoring operational data of the Active Cells and the surrounding Ex-Cell Technical Gallery areas.

The primary functions of the EMS include monitor the ambient temperature in the Process Cell and Maintenance Cell, as well as monitoring the ambient temperature, relative humidity, cubicle temperatures, and presence of flooding in the Technical Galleries. Miscellaneous signals from around the facility, such as non-safety gamma monitors in the Waste Transfer Area are also monitored.

Overall this subsystem includes:

- 40 Temperature sensors
- 8 Humidity sensors
- 15 position switches to detect doors for confinement
- 8 Leak sensors
- An operational gamma monitor

Analogue sensors were preferred throughout the EMS design due to increased radiation tolerance, simplicity of integration, and ease of replacement in future compared with digital equivalents.

All data collected by the Environmental Monitoring System is to be provided to the Active Cells Control System to be displayed via a human interface. Operators in the Control Room will have the collated data at their disposal via logs and via visual representations. The EMS will also send alerts to operators via the Control System, should the environmental monitored values become of a concern. For example, in the case a cubicle reaches 50 °C, the operators in the control room will be alerted.

VIII. CONSIDERATIONS FOR MAINTENANCE OVER THE FACILITY LIFETIME

Due to the restrictions on human access into the facility, especially the process cell, specific considerations had to be made for maintenance and modifications of the facility over its multi-decade lifetime. Approaches to this included features to enable remote replacement of components expected to fail, alongside high reliability and robustness for elements that were expected to last the lifetime of the facility.

Any equipment being designed for use in the Active Cells has been designated as either line replaceable, or non-maintainable. The challenges of operating completely remotely steered the overall maintenance approach away from in-situ repair activities and towards simpler operations involving only replacement of modules in-situ. Overall this approach required simpler operations to be conducted in the cells, however made system designs more complex and non-standard compared with typical industrial systems.

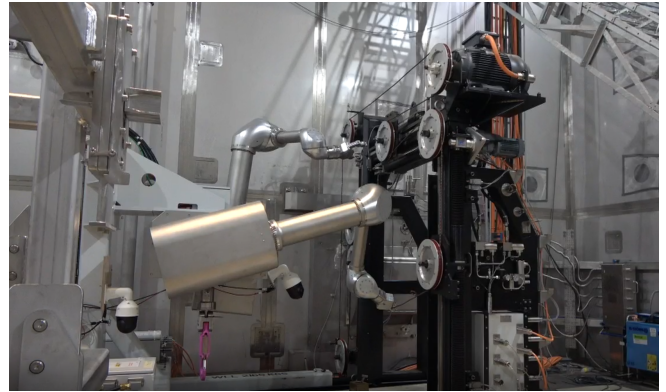


Fig. 15. Remote changing of a diamond saw wire using the Telbot manipulator within the Process Cell.

Items designated as non-maintainable are mostly simple structural steel elements. Whilst they are considered non-maintainable, considerations have been made for their permanent removal from the facility, allowing for some flexibility with future needs as well as eventual decommissioning.

Maintainable items including sensors, actuators, and many other items were typically mounted on plates with features for remote connection and disconnection of services as well as remote handling including installation and removal using the facility Remote Handling system.

A. Remote Diamond Wire Replacement

One of the key items requiring frequent replacement due to routine operations is the diamond wire blade of both the Shaft Cutting Station and Machining Station. The wire is twisted to evenly wear the diamonds, and the wires coiling makes direct handling with the manipulator challenging. This is however achieved with the Handling System as shown in Figure 15.

Trials were carried out to identify methods to retain the wires, with multiple integrated and external handling aids investigated. The key learnings being to lock the pulley as well as the wire, working with gravity, and that the key wire retention points are at the opposite diagonal pulleys in the set-up (top left and bottom right pulleys).

B. Electrical Junction Box Replacement

Experience from remote maintenance at JET revealed that electrical connection points can be a relatively common source of faults and failures. With the Active Cells Facility housing numerous pieces of equipment, sensors, and actuators, combined with the expectation of remote replacement of many of these elements, there are risks associated with electrical connectivity issues.

In order to mitigate these risks, electrical and signal connectivity to the machines in the facility has been provided via cables with connectors which interface with the junction

1270 boxes mounted on the walls of the cell. These wall mounted
 1271 junction boxes provide feed-throughs to relay signals and
 1272 power to areas outside the cells where human access is per-
 1273 missible.
 1274 The junction boxes feature remote handling compatible
 1275 features and interfaces to allow for remote connection and
 1276 disconnection of services to the equipment within the facility.
 1277 In some cases, dual, redundant junction box positions have
 1278 been allocated to allow for potential failures, as well as po-
 1279 tential future expansion to the systems.

IX. FUTURE NEEDS AND PLANNED UPGRADES

1281 Whilst the Active Cells Facility was designed to perform a
 1282 specific set of known tasks on known components, it is antici-
 1283 pated that there will be some differences in future needs. Dur-
 1284 ing design and delivery, some accommodations were made
 1285 for flexibility and agility in the capabilities and equipment
 1286 provided by the facilities.

1287 The most strongly anticipated change to the needs of the
 1288 facility would result from variations in the components to be
 1289 processed. The facility was designed to process waste com-
 1290 ponents in an initial design, however it is likely that these
 1291 designs will evolve as the facility transitions into operations.

1292 Some accommodations (including modularity of equip-
 1293 ment and interfaces) have been included as discussed in previ-
 1294 ous sections, allowing for future changes to equipment. Ad-
 1295 ditionally, the removal of non-maintainable items has been
 1296 considered, allowing for the potential of a future overhaul and
 1297 refit of the facilities from scratch in the case of a significant
 1298 change to the required processes.

1299 Digital aspects of the system (including the High Level
 1300 Control System) have been created in a manner that allows
 1301 for future upgrades with relatively low impact. It is expected
 1302 that the digital twin system might be enhanced to provide ad-
 1303 ditional functionality such as automated updating and object
 1304 tracking, using data from the cameras.

1305 Finally, one area of possible automation to boost efficiency
 1306 might lie in automation of some of the longer but relatively
 1307 simple tasks. For example, the process of opening a Pit in-
 1308 volves the serial removal of up to 4 Storage Pit Lids, resulting
 1309 in a 2-hour overall process. It is conceivable that this type of
 1310 well-understood task could be automated.

A. Identifications for future improvements

1312 Throughout the design and delivery of the Active Cells,
 1313 potential enhancements have been considered that would im-
 1314 prove the efficiency of operations, or provide other benefits.
 1315 A selection of these are described in brief below:

- 1316 1. Automated motion sequences for cranes, provid-
 1317 ing functionality for pre-programming movement se-
 1318 quences for common locations and tasks.
- 1319 2. General resolved motion for cranes, allowing more
 1320 than one joint moving at a time, defining motions di-

rectly at the lifting point. This is currently in place
 for for specific tasks (layover operations) to enable the
 tracing of arcs, however it is believed there is potential
 for further benefits through use of this type of resolved
 motion.

3. Improved viewing on the manipulator, including cam-
 era enhancements such as roll function (digital or phys-
 ical).
4. Automated tracking of components and equipment
 with cameras. This could include pulley positions on
 the Shaft Cutting Station.
5. The addition of boundaries and anti-collision zones for
 cranes and manipulators, which could be manually de-
 fined by operators, or dynamically defined from tracked
 objects.
6. A physical mock-up facility for training, task develop-
 ment, and trials.
7. Digital Twin based training and operation planning
 packages.
8. Joystick control of cranes with fully variable speed.
9. Additional Telbot end effectors to replace the gripper,
 with a remote exchange at a gripper change station, fa-
 cilitating alternative interfaces to equipment and the en-
 vironment.
10. Wire saw cooling system to improve the cut times and
 life of the wire.
11. Additional tooling suites for optimised material pro-
 cessing and handling.
12. Enhanced sensing capabilities within the cell, for ex-
 ample mobile gamma monitors or 3D geometric mea-
 surement systems for object tracking, mapping current
 status of the cell, and localisation of gripper interfaces.
13. Leveraging Artificial Intelligence to improve processes
 in the cell through utilisation of gathered process data
 for condition monitoring or process optimisation.

These thoughts are provided as potential considerations for
 future facilities, as well as to stimulate research in the topic
 areas.

X. FURTHER IMPLICATIONS AND LESSONS LEARNED FOR OTHER FACILITIES

The ESS Active Cells Facility is a first-of-a-kind large scale
 hot cell facility designed to perform highly challenging waste
 size reduction and waste storage tasks entirely remotely over
 decades of operation. This includes remote handling and ma-
 nipulation of equipment and components using a robotic ma-
 nipulator system within a high radiation environment. As

such, it has paved the way in terms of establishing technological solutions and processes that will likely be relevant to other waste processing facilities and high-energy physics experiments.

Windowless hot cells are possible - Despite the facility still being in the process of delivery at the time of writing, we are confident that it is possible to design, deliver, and operate a fully remote hot cell with operations spanning a wide spatial volume. The Active Cells Facility was designed for fully remote operations with robotic manipulation and feedback via radiation tolerant camera systems. Preliminary testing of fully remote use of the manipulators, cranes and cutting systems using the viewing system has demonstrated this capability. It was designed for decades of operations, accounting for future maintenance, modifications, and upgrades.

Cost evaluations - Cost estimates were calculated at the beginning of the delivery process, however until engaging directly with the market it was highly difficult to accurately estimate costs associated with supply of some of the bespoke equipment needed. Benchmarking against existing products and equipment delivered into similar facilities, taking into account differences in requirements, proved an invaluable tool for improving the accuracy of cost estimates as well as identifying delivery risks.

Design for remote - Many aspects of design and delivery of the Active Cells would have been significantly simpler and cheaper if components were designed for remote operations from the start. Engagement with remote handling and operations expertise during initial design of the facility and components to be processed would have been highly beneficial.

Allowing suppliers to innovate - The approach to engagement with industrial supply chain through delivery of the facility was largely seen as a success. In particular, specifying requirements whilst allowing for divergence from conceptual designs allowed suppliers to find innovative ways to solve the real problems, in some cases using existing solutions in novel ways, driving down cost.

Robustness to supply chain and technology changes - The functional approach, applying systems engineering

frameworks, has allowed UKAEA to adapt rapidly to supply chain issues (such as supplier insolvencies) and technical challenges to maintain project progress without necessitating significant rework.

XI. SUMMARY

This paper has explored the overall approach to delivery of the ESS Active Cells Facility, a hot cell designed for size reduction and packing of large highly radioactive waste components from the ESS experiment.

Operational analysis was conducted in order to analyse the required tasks and aid in specifying requirements on equipment that would be needed in the facility. During this process, operations engineers with experience from operating the remote maintenance systems at the Joint European Torus fusion experiment were engaged in order to translate know-how from the similar operations conducted over several decades.

The overall design and approach to design of the Active Cells was presented, including highlighting some of the key cross-cutting infrastructure. Some of the key challenges were analysed and used to help assess maturity of available solutions as well as outstanding technical risk.

An approach to delivery of the individual subsystems in a manner that encouraged innovative solutions from the supply chain was presented, as well as some descriptions of the key equipment resulting.

Considerations for maintenance and upgrades is an important topic when designing a facility intended to operate for decades, and this is particularly challenging when doing so in extreme high radiation environments such as in the Active Cells. The overall approach to accommodating maintenance and modifications was discussed in some detail.

Finally, in the hope of informing the future design of similar facilities, some of the more salient lessons learned and highlights were presented. This included aspects related to design, procurement, and cost estimation, but with the key lesson being that the undertaking is an achievable one.

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